

Statische berekening

Onderdeel : staalconstructie

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Project naam : Nieuwbouw schuur

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dd : 08-07-15

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Taal : Nederlands

Toelichting berekening :

Globaal is de berekening opgebouwd uit 3 delen.

-Deel één met hierin aangegeven de algemene zaken zoals normen, opbouw van de belastingen en detailberekeningen.

-Deel twee (**10.1**) met de grafische in- en uitvoer waarin de belastinginvoer in beeld is gebracht en momentenlijnen, dwarskrachtenlijnen en verplaatsingen terug te vinden zijn.

-Deel drie (**10.2**) met hierin numerieke in- en uitvoer waarin het voornamelijk van belang is te zien waaruit de belastingcombinaties samengesteld zijn en wat de resultaten van de staafcontroles zijn.

Hierin is dus tevens terug te vinden hoe de belastingen van de maatgevende reacties opgebouwd zijn.

De reactiekrachten zelf zijn helemaal achterin de berekening terug te vinden.

blz 37 t/m 38

Onder de reactiekracht staat vermeld wat het maatgevende belastinggeval is en de opbouw van dit belastinggeval is dus in deel **10.2** bij de belastingcombinaties terug te vinden

blz 8 t/m 12

1.1 Inleiding

Het betreft hier een agrarisch (stal, loods) gebouw , categorie E , CC1

In de gevels en het dak windverband om de constructie in langsrichting te schoren.

In de andere richting wordt de stabiliteit verzorgd door een ongeschoord portaal.

Tijdens de montage zogdragen voor voldoende stabiliteit van de gemonteerde onderdelen dmv het aanbrengen van (tijdelijke) schoren.

1.2 Algemene kwaliteiten, factoren en eisen

Staalkwaliteit : S235

(breuktaaiheid zie blz 5)

Boutkwaliteit : 8.8 t.a.v.

Ankerkwaliteit : 4.6 t.a.v.

Potentiële factoren :

		ψ_0	ψ_1	ψ_2
(QK,sn)	sneeuwbelasting :	0,00	0,20	0,00
(QK,w)	windbelasting :	0,00	0,20	0,00

Partiële veiligheids factoren UGT :

	ogu	gu
(verg. 6.10a)	$\gamma_G = 1,35$	0,90
(verg. 6.10b)	$\gamma_G = 1,20$	0,90
	$\gamma_Q = 1,50$	
	$\xi = 0,89$	

Partiële veiligheids factoren BGT :

$\gamma_G = 1,00$
$\gamma_Q = 1,00$

Partiële factoren γ_M EN-1993-1-1:

$\gamma_{M0} = 1,00$
$\gamma_{M1} = 1,00$
$\gamma_{M2} = 1,25$

Betrouwbaarheidsdifferentiatie KFI-factor : 0,90

Ontwerplevensduur : 15 jr

		δ_{bij}	δ_{totaal}
Verplaatsingen :	verticaal :	dak $\leq 0,004 L_{rep}$	$\leq 0,004 L_{rep}$

Verplaatsingen :	horizontaal :	gevel- $H/100$	($\delta_{max.} = 38,00 \text{ mm}$) (indicatief)
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1.3 Belastingcombinaties

Zie ook deel **10.2** numerieke computerinvoer blz 8 t/m 12
Veranderlijke belastingen : sneeuw + wind

UGT

fundamentele combinatie :

6.10a

$$KFI \cdot (\gamma G \cdot G_{k,eg} + \gamma G \cdot G_{k,d,w} + \gamma Q \cdot \psi_0 \cdot q_{k,sn} + \gamma Q \cdot \psi_0 \cdot q_{k,wi}) \\ 0,9 \cdot (1,35 \cdot G_{k,eg} + 1,35 \cdot G_{k,d,w} + 1,5 \cdot 0 \cdot q_{k,sn} + 1,5 \cdot 0 \cdot q_{k,wi})$$

6.10b

$$KFI \cdot (\gamma G \cdot G_{k,eg} + \gamma G \cdot G_{k,d,w} + \gamma Q \cdot q_{k,sn} + \gamma Q \cdot \psi_0 \cdot q_{k,wi}) \\ 0,9 \cdot (1,2 \cdot G_{k,eg} + 1,2 \cdot G_{k,d,w} + 1,5 \cdot q_{k,sn} + 1,5 \cdot 0 \cdot q_{k,wi})$$

6.10b

$$KFI \cdot (\gamma G \cdot G_{k,eg} + \gamma G \cdot G_{k,d,w} + \gamma Q \cdot \psi_0 \cdot q_{k,sn} + \gamma Q \cdot q_{k,wi}) \\ 0,9 \cdot (1,2 \cdot G_{k,eg} + 1,2 \cdot G_{k,d,w} + 1,5 \cdot 0 \cdot q_{k,sn} + 1,5 \cdot q_{k,wi})$$

6.10b

$$\gamma G \cdot G_{k,eg} + \gamma G \cdot G_{k,d,w} + KFI \cdot (\gamma Q \cdot \psi_0 \cdot q_{k,sn} + \gamma Q \cdot q_{k,wi}) \\ 0,9 \cdot G_{k,eg} + 0,9 \cdot G_{k,d,w} + 0,9 \cdot (1,5 \cdot 0 \cdot q_{k,sn} + 1,5 \cdot q_{k,wi})$$

BGT

karacteristieke combinatie :

$$\begin{aligned} & * \gamma G \cdot G_{k,eg} + \gamma G \cdot G_{k,d,w} + \gamma Q \cdot q_{k,sn} + \gamma Q \cdot \psi_0 \cdot q_{k,wi} \\ & (1 \cdot G_{k,eg} + 1 \cdot G_{k,d,w} + 1 \cdot q_{k,sn} + 1 \cdot 0 \cdot q_{k,wi}) \\ & * \gamma G \cdot G_{k,eg} + \gamma G \cdot G_{k,d,w} + \gamma Q \cdot \psi_0 \cdot q_{k,sn} + \gamma Q \cdot q_{k,wi} \\ & (1 \cdot G_{k,eg} + 1 \cdot G_{k,d,w} + 1 \cdot 0 \cdot q_{k,sn} + 1 \cdot q_{k,wi}) \end{aligned}$$

quasi-blijvende combinatie :

1.4 Normen

Gehanteerde normen voor de constructie :

NEN-EN 1090 (nl)

Eurocode - Vervaardigen van staalconstructies

augustus 2011

NEN-EN 1990 (nl) + NB

Eurocode - Grondslagen van het constructief ontwerp

december 2011

NEN-EN 1991 (nl) + NB

Eurocode 1 - Belastingen op constructies , algemene belastingen

1-1 Volumieke gewichten, eigengewicht en opgelegde belastingen voor gebouwen

december 2011

1-3 Sneeuwbelasting

december 2011

1-4 Windbelasting

december 2011

NEN-EN 1993-1-1 (nl) + NB

Eurocode 3 - Ontwerp en berekening van staalconstructies

1-1 Algemene regels en regels voor gebouwen

december 2011

NEN-EN 1993-1-8 (nl) + NB

Eurocode 3 - Ontwerp en berekening van staalconstructies

1-8 Ontwerp en berekening van verbindingen

december 2011

NEN-EN 1995-1-1 + C1 + A1/NB

Eurocode 5 - Ontwerp en berekening van houtconstructies

deel 1-1 Algemeen- Gemeenschappelijke regels en regels voor gebouwen

juli 2013

<i>Programmatuur :</i>	Belastingen+factoren	Excel, Kloeze spreadsheet
	Hoofdberekening	3-D eindige elementen programma STAAD Pro. De doorsnede- en stabiliteitscontrole van de staven wordt binnen het programma uitgevoerd volgens EUROCODE NEN-EN 1993-1-1 Eerste-orde elastische berekening
	Detailberekening	COP csJoint Excel, Kloeze spreadsheets

1.5 Algemene gebouw informatie

Gebouw lokatie :

geografische ligging

Land :	Nederland
Plaats :	Peest
Aardbevings gebied :	nee ▼

Gebouw kenmerken :

bouw situatie : nieuwbouw ▼

soort bouwwerk : agrarisch (stal, loods) gebouw ▼

schoorsysteem : langshevels geschoord ▼

classificatie bouwwerk : non-sway ▼ ($\alpha_{cr} = 46,11 \geq 10$) non-sway

omstandigheden staalconstructie : binnen, onverwarmt ▼

ontwerplevensduur : 15 jr
categorie : E
gevolgklasse : CC1
gebruiks-categorie : SC1 (statisch)
productie-categorie : PC1 (staalkwaliteit $\leq S275$)
uitvoeringsklasse : EXC1

afmetingen van het gebouw : $l = 10,00$ m (lengte)
 $b = 7,50$ m (breedte)
 $h_{(n)} = 5,21$ m (hoogste punt)

langshevels : ongelijke hoogten
 $h_A = 3,80$ m (hoogte hoge zijgevel)
 $h_B = 3,00$ m (hoogte lage gevel)

vorm van het dak : zadeldak ▼

$\alpha_1 = 45,00^\circ$ (hoge gevel)
 $\alpha_2 = 20,00^\circ$ (lage gevel)

oppervlak gevel : zeer ruw ▼ (rimpels, ribben, kronkelingen)

oppervlak dak : zeer ruw ▼ (rimpels, ribben, kronkelingen)

vloer : nee ▼

kraan : nee ▼

brand : nee ▼

hemelwater afvoer : buitengoot ▼

dakplaat als kipsteun : nee ▼

houten delen : ja ▼ (dak + wand)

1.6 Prestatiekenmerken

Constructief :

Methode van verklaren : 2a (MPCS)

Ontwerpkeuze : Eurocode 3: ontwerp en berekening van staalconstructies NEN-EN 1993

Materiaal :

Materiaal keuze : Warmgewalst staal incl koudgewalste kokers conform EN-10025-x en EN 10219-1

Duurzaamheid :

Vorbewerking : niet gespecificeerd

Finishing : verzinken

Finishniveau : C1

Graad van verbewerking : P1

Kenmerken :

Algemeen :

toleranties op geometrische gegevens : NEN-EN 1090-2

Lasbaarheid : Constructiekoolstofstaal conform EN-10025-x en EN 10219-1
(zie onderdeelpecificaties voor details)

Breuktaaiheid balkstaal : JR (27J bij 20 °C) maximale elementdikte t= 32,5 mm

Breuktaaiheid stripstaal : JR (27J bij 20 °C) maximale elementdikte t= 37,5 mm

Breuktaaiheid kokers : JR (27J bij 20 °C) maximale elementdikte t= 37,2 mm

Reactie op brand : klasse A1

Vrijkomen van cadmium : NPD

Radioactieve starling : NPD

Duurzaamheid : Oppervlaktebehandeling verzinken (ISO 1461)

Constructieve kenmerken :

Draagvermogen : Constructief ontwerp conform Eurocode 3: ontwerp en berekening van
staalconstructies NEN-EN 1993 vlgs. de NB van Nederland

Vervorming in bruikbaarheidsgrenstoestand : NPD

Vermoeiingssterkte : NPD

Brandweerstand : NPD

Fabrikage :

producten geleverd : vlgs. onderdelenspecificatie, EN 1090-2, conform EXC1

De belastingen zijn handmatig ingevoerd in Staad, ter verduidelijking een voorbeeld van iedere belasting.

Voorbeeld veldbreedte dak : $b = 5,00 \text{ m}$

2.1	Gk, eg	-eigengewicht staal
2.1	Gk, d+w	-blijvende belasting dak + wand
2.3	qk, sn	-sneeuwbelasting
2.4	qk, wi	-windbelasting

2.1 Blijvende belastingen

staalconstructie : behandeling- verzinken, factor EG staal Y-1,08

dakopbouw : sandwichpaneel dak ▼

sandwichpaneel				gewichten :
isolatie	PUR	d= 60,00	0,125 kN/m ²	
gording	hout		0,078 kN/m ²	
aditioneel	leidingen + licht		0,050 kN/m ² +	
		Gk, d	totaal : 0,253 kN/m²	
		(voorbeeld)	qk, d= 1,27 kN/m	

gevelopbouw : stalen profielplaat ▼

staalplaat	type : 35.207.1035x0,63		gewichten :
isolatie	nee		0,060 kN/m ²
wandregel	hout		0,000 kN/m ²
aditioneel			0,078 kN/m ²
			0,000 kN/m ² +
		Gk, w	totaal : 0,138 kN/m²
		(voorbeeld)	qk, w= 0,69 kN/m

eventuele vorstrand : afdracht rechtstreeks naar fundering ▼

2.2 Opgelegde belastingen

(n.v.t.)

3 Ontwerpsituaties

klimaatgebied : Nederland ▼

zone : 0 ▼

omstandigheden : normale omstandigheden 3.2 (1) ▼

ontwerpsituatie : blijvende/tijdelijke otwerpsituatie (1) verdeeld +(2) herverdeeld ▼

sneeuwbelasting aanpassen aan ontwerplevensduur : ja ▼

ontwerplevensduur 15 jr. V= 0,8

volumiek gewicht van sneeuw (γ) : compact ▼2,00 kN/m³

4 Sneeuwbelasting op de grond

4.1 karakteristiek waarden

karakteristieke waarde sneeuwbelasting op de grond $S_{k50} = 0,70 \text{ kN/m}^2$
 $S_n = 0,53 \text{ kN/m}^2$

 $S_{k15} = 0,76 S_{k50}$

4.3 uitzonderlijke sneeuwbelasting op de grond n.v.t.

5 Sneeuwbelasting op daken

5.1 aard van de belasting

a) de vorm van het dak : zadeldak

5.2 belastingschikkingen

 $S = \mu_i C_e C_t S_k$ b) warmtecoëfficiënt : $\leq 1 \text{ W/m}^2\text{K}$ ▼ $C_t = 1,0$ d) blootstellingscoëfficiënt : normaal ▼ $C_e = 1,0$

5.3 sneeuwbelastingcoëfficiënten

 $\alpha_1 = 45^\circ$ $\mu_1 = 0,40$ $\alpha_2 = 20^\circ$ $\mu_1 = 0,80$

e) aangrenzende daken : nee ▼

6 Lokale effecten

6.2 sneeuwophoping

obstakel : geen uitstekende delen ▼

Sneeuwbelastingen : $S = \mu_i C_e C_t S_k$

(grondvlak)

zadeldak

 $(\alpha_1) \quad S_1 = 0,21 \text{ kN/m}^2 \quad (\text{verdeeld geval (i)})$ $(\alpha_2) \quad S_2 = 0,42 \text{ kN/m}^2 \quad (\text{verdeeld geval (i)})$ $S_1 = 0,11 \text{ kN/m}^2 \quad (\text{herverdeeld geval (ii+iii)})$ $S_2 = 0,21 \text{ kN/m}^2 \quad (\text{herverdeeld geval (ii+iii)})$

(voorbeeld) $S_2 = 0,42 \text{ kN/m}^2 \quad (0,399 \text{ kN/m}^2)$
 $S_1 = 0,21 \text{ kN/m}^2 \quad (0,150 \text{ kN/m}^2)$

 $q_{sn} = 2,00 \text{ kN/m} \quad (\text{dakvlak})$ $q_{sn} = 0,75 \text{ kN/m} \quad (\text{dakvlak})$

2.4 Wind belastingen

Wind belasting NEN-EN 1991-1-4 (nl) december 2011

ψ -factoren : ψ_0 ψ_1 ψ_2
0,00 0,20 0,00

luifel :

algemeen: ☒ default waarden

ontwerplevensduur : 15 jr.

windgebied :

terreincategorie : onbebouwd

$K = 0,281$
 $n = 0,5$
 $Z_0 = 0,200$ m
 $Z_{min} = 4$ m

windbelasting aanpassen aan ontwerplevensduur :

afstand tot grens overgangsgebied $\geq 5,00$ km



4 Windsnelheid en stuwdruk

4.2 *basiswaarden* $V_b = C_{dir} \cdot C_{season} \cdot C_{prob} \cdot V_{b,0}$
 $V_b = 22,5$ m/s

$C_{dir} = 1,0$ (standaard)
 $C_{season} = 1,0$ (standaard)
 $C_{prob} = 0,917$
 $V_{b,0} = 24,5$ m/s

4.3 gemiddelde wind

4.3.1 variatie met hoogte $V_m(Z) = C_r(Z) \cdot C_o(Z) \cdot V_b$

ruwheidslengten
 $Z_{0,II} = 0,05$ m
 $Z_{max} = 200$ m
 $Z = 5,2$ m ($Z_{min} > 4$ m)

4.3.2 terreinruwheid $K_r = 0,209$

$C_r(Z_s) = 0,68$

4.3.3 terreinorografie

$\Phi = 0,000$

orografie parameters

parameters niet van toepassing

orografieeffecten hoeven niet meegenomen te worden (4.3.3)
 $C_o(Z) = 1,000$

gemiddelde windsnelheid $V_m(Z_s) = 15,3$ m/s

4.3.4 grote en beduidend hogere naburige gebouwen

naburig gebouw minstens twee keer zo hoog als gemiddelde bebouwing

bebouwings parameters

parameters niet van toepassing

4.3.5 bebouwingsdichtheid

$h_{dis} = 0$ m

4.4 *windturbulentie*
 opm. 1 standaard afwijking van de turbulentie σ_v

$$\sigma_v = 4,70$$

opm. 2 bepaling $L_v(Z)$ $Z = 5,2 \text{ m}$
 $L_v(z_s) = 0,3067$

4.5 *extreme stuwdruk*
 opm. 1

basisstuwdruk $q_b = 0,32 \text{ kN/m}^2$
 blootstellingsfactor $C_e(Z) = 1,47$

5 Windbelastingen

5.2 *winddruk op de buitenzijde en binnenwanden*

buitenzijde $W_e = q_p(Z_e) \cdot C_{pe}$ (drukcoëfficiënten zie blz 10)
 binnenwanden $W_i = q_p(Z_i) \cdot C_{pi}$ (drukcoëfficiënten zie blz 11)

5.3 *windkrachten*

$$A_{ref} = \boxed{10,0 \text{ m}^2}$$

$$F_w = C_s C_d \cdot q_p(Z_e) \cdot C_f \cdot A$$

$$Q_w = C_s C_d \cdot q_p \cdot C_f \cdot b$$

6 **Bouwwerkfactor $C_s C_d$** $H \leq 15 \text{ m}$ gedetailleerde procedure :
 aangepaste C_d : ($h < 50 \text{ m}$ en $h/b < 5$)

6.3 *gedetailleerde procedure*

6.3.1 Bouwwerkfactor $C_s C_d > 0,85$

constructietype : verticale constructies zoals gebouwen

constructietype :

$\delta_s = \text{n.v.t.}$

$C_{s,l} = 1,000$ $C_{s,b} = 1,000$
 $C_{d,l,A} = 1,000$ $C_{d,b,C} = 1,000$
 $C_{d,l,B} = 1,000$ $C_{d,b,D} = 1,000$

$C_s C_{d,l,A} = 1,000$ ($1,000 \times 1,000 = 1,00 \geq 0,85$)
 $C_s C_{d,l,B} = 1,000$ ($1,000 \times 1,000 = 1,00 \geq 0,85$)
 $C_s C_{d,b,C} = 1,000$ ($1,000 \times 1,000 = 1,00 \geq 0,85$)
 $C_s C_{d,b,D} = 1,000$ ($1,000 \times 1,000 = 1,00 \geq 0,85$)

Extreme stuwdruk : referentieperiode 15 jr , $h = 5,21 \text{ m}$, windgebied III, terreincategorie II

$$q_p(5,21) = 0,462 \text{ kN/m}^2 \quad (q_p(Z) = 0,550 \text{ kN/m}^2 ; C_{prob} = 0,917)$$

Winddruk :

wind op $\beta 0^\circ$ (gevel A+B) $Z_e; h; l = 5,2 \text{ m}$ $Q_{W,l,A} = 0,462 \cdot C_f \cdot b$
 $Q_{W,l,B} = 0,462 \cdot C_f \cdot b$
 wind op $\beta 90^\circ$ (gevel C+D) $Z_e; h; l = 5,2 \text{ m}$ $Q_{W,b,C} = 0,462 \cdot C_f \cdot b$
 $Q_{W,b,D} = 0,462 \cdot C_f \cdot b$

7 **Druk- en krachtcoëfficiënten** (belastingen bepalen vlgs 7.2.9 NEN-EN 1991-1-4)

7.2 *Drukcoëfficiënten voor gebouwen* (zadeldak, lengte 10m, breedte 7,5m, hoogte 5,21m)

Gevels

7.2.2 verticale gevels van gebouwen met rechthoekige plattegrond

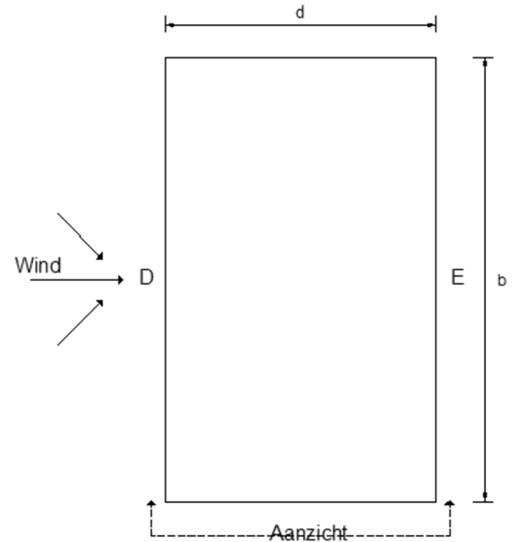
Opmerking gebrek aan correlatie tussen vlakken D en E in rekening brengen:

$h/l = 0,52$ correlatiefactor= 0,850

$h/b = 0,69$ correlatiefactor= 0,850

$Ze(h) = 5,2 \text{ m}$

-windwrijving $C_{fr} = 0,04$ (gevels)



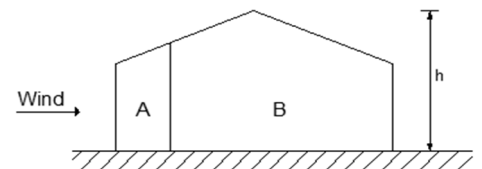
-winddruk, windzuiging (gevels)

wind ($\theta=0^\circ$) $Q_{W,l} = 0,462 \cdot C_f \cdot b$

$e = 10,00 \text{ m}$

$d = 7,50 \text{ m}$

Zone	C_{pe}
A = 2,00 m	-1,20
B = 5,50 m	-0,80



(+ correlatiefactor) $D = 10,00 \text{ m}$ $+0,80$ ($+0,80 \times 0,850 = +0,680$)
 (+ correlatiefactor) $E = 10,00 \text{ m}$ $-0,50$ ($-0,50 \times 0,850 = -0,425$)

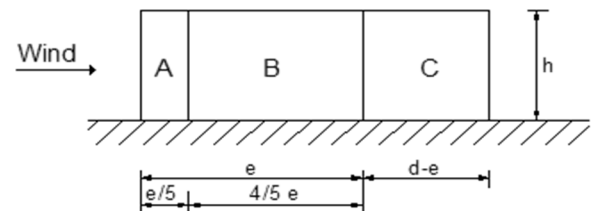
(voorbeeld) $q_{W,l;D} = 1,57 \text{ kN/m}$
 (voorbeeld) $q_{W,l;E} = -0,98 \text{ kN/m}$

wind ($\theta=90^\circ$) $Q_{W,b} = 0,462 \cdot C_f \cdot b$

$e = 7,50 \text{ m}$

$d = 10,00 \text{ m}$

Zone	C_{pe}
A = 1,50 m	-1,20
B = 6,00 m	-0,80
C = 2,50 m	-0,50
(+ correlatiefactor) $D = 7,50 \text{ m}$	$+0,80$ ($+0,80 \times 0,850 = +0,680$)
(+ correlatiefactor) $E = 7,50 \text{ m}$	$-0,50$ ($-0,50 \times 0,850 = -0,425$)



Daken

7.2.5 zadeldak

$$\alpha_1 = 45,0^\circ$$

$$\alpha_2 = 20,00^\circ$$

-windwrijving

$$C_{fr} = 0,04$$

-winddruk, windzuiging (- =zuiging, + =druk)

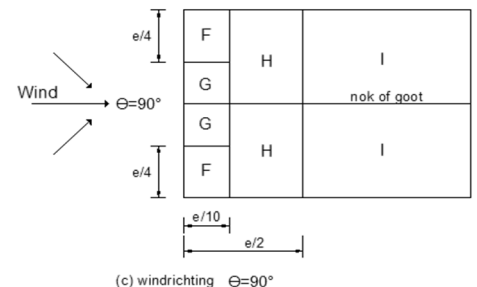
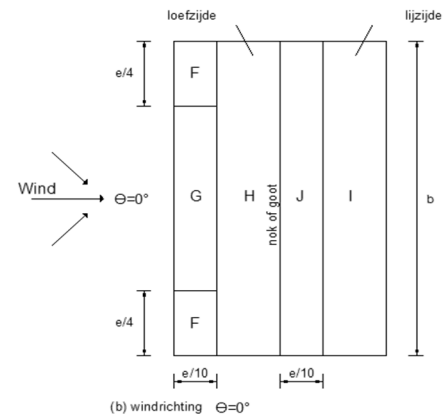
wind ($\theta=0^\circ$) ($45,0^\circ$)	l (e/4)	b (e/10)	Cpe-	Cpe+
QW,l= 0,462 . Cf . b	F= 2,50	1,41	-0,00	+0,70
	G= 5,00	1,41	-0,00	+0,70
	H= 10,00	0,59	-0,00	+0,60
	I= 10,00	5,41	-0,40	+0,00
	J= 10,00	1,06	-0,83	+0,00

wind ($\theta=180^\circ$) ($20,00^\circ$)	l (e/4)	b (e/10)	Cpe-	Cpe+
QW,l= 0,462 . Cf . b	F= 2,50	1,06	-0,77	+0,37
	G= 5,00	1,06	-0,70	+0,37
	H= 10,00	5,41	-0,27	+0,27
	I= 10,00	0,59	-0,20	+0,00
	J= 10,00	1,41	-0,30	+0,00

wind ($\theta=90^\circ$)	l (e/4)	b (e/10)	Cpe- (45°)	Cpe- (20°)
QW,b= 0,462 . Cf . b	F= 2,65	0,75	-1,10	-1,23
	G= 0,00	0,75	-1,40	-1,33
	H= 2,00	3,00	-0,90	-0,67
	I= 2,00	6,25	-0,50	-0,50

(voorbeeld) Cpe= **-0,00**

$$QW,l= 0,00 \text{ kN/m}$$



7.2.9 inwendige druk (7.1 + 7.2)

(+ = overdruk, - = onderdruk)

rekening houden met dominante zijde :

gevels af te sluiten :

gehele gevel geopend : ja ; langsgevel

wind op +X druk Cpi= +0,72

wind op -X zuiging Cpi= -0,45

wind op +/-Z zuiging Cpi= -0,79

3.1 Windverband+aansluiting NEN-EN 1993-1-1 + NEN-EN 1993-1-8

windverband	<u>strip</u> :	50 x 6	S235	$f_y = 235 \text{ N/mm}^2$ $f_u = 360 \text{ N/mm}^2$	$\gamma_{M_0} = 1,00$ $\gamma_{M_2} = 1,25$		
trekkracht $N_{Ed} = 21,9 \text{ kN}$ excentrische belasting							
				$N_{u,Rd} = [0,9 A_{net} f_u] / \gamma_{M_2} = 51,3 \text{ kN}$	$\geq N_{Ed} = 21,9 \text{ kN}$	(0,43)	(uitscheuren niet maatgevend)
	bout : M16 8.8		gerolde draad	aantal : 2 st	h.o.h. $p_1 = 60 \text{ mm}$	$e_{1;1} = 30 \text{ mm}$	
	afschuifvlak : door de draad		aantal bouten boven elkaar : 1 st				
	gaten : normale gaten						
	$d_0 = 17 \text{ mm}$						
	$k_s = 1,00$	$\alpha_b = 0,59$	$F_{v,Rd} = 60,3 \text{ kN}$	$\geq F_{v,Ed} = 11,0 \text{ kN}$	(0,18)		
		$k_1 = 2,42$	$F_{b,Rd} = 39,3 \text{ kN}$	$\geq F_{b,Ed} = 11,0 \text{ kN}$	(0,28)		
windverband	<u>plaat</u> :	$d = 10 \text{ mm}$	S235	$f_y = 235 \text{ N/mm}^2$ $f_u = 360 \text{ N/mm}^2$			
				$V_{eff,2,Rd} = 0,5 f_u A_{nt} / \gamma_{M_2} + (1 / \sqrt{3}) f_y A_{nv} / \gamma_{M_0} = 104,5 \text{ kN}$	$\geq N_{Ed} = 21,9 \text{ kN}$	(0,21)	
	$e_{1;1;min.} = 25 \text{ mm}$	$\alpha_d = 0,49$	$F_{v,Rd} = 60,3 \text{ kN}$	$\geq F_{v,Ed} = 11,0 \text{ kN}$	(0,18)		
	$e_{2;1;min.} = 25 \text{ mm}$	$k_1 = 2,42$	$F_{b,Rd} = 54,6 \text{ kN}$	$\geq F_{b,Ed} = 11,0 \text{ kN}$	(0,20)		
windverband	<u>hoek</u> :	50 x 50 x 5	S235	$f_y = 235 \text{ N/mm}^2$ $f_u = 360 \text{ N/mm}^2$	$\gamma_{M_0} = 1,00$ $\gamma_{M_2} = 1,25$		
trekkracht $N_{Ed} = 22,1 \text{ kN}$ centrische belasting							
				$N_{u,Rd} = [\beta_2 A_{net} f_u] / \gamma_{M_2} = 59,6 \text{ kN}$	$\geq N_{Ed} = 22,1 \text{ kN}$	(0,37)	(uitscheuren maatgevend)
	bout : M16 8.8		gerolde draad	aantal : 2 st	h.o.h. $p_1 = 60 \text{ mm}$	$e_{1;1} = 30 \text{ mm}$	
	afschuifvlak : door de draad		aantal bouten boven elkaar : 1 st				
	gaten : normale gaten						
	$d_0 = 17 \text{ mm}$						
	$k_s = 1,00$	$\alpha_b = 0,59$	$F_{v,Rd} = 60,3 \text{ kN}$	$\geq F_{v,Ed} = 11,1 \text{ kN}$	(0,18)		
		$k_1 = 2,42$	$F_{b,Rd} = 32,8 \text{ kN}$	$\geq F_{b,Ed} = 11,1 \text{ kN}$	(0,34)		
windverband	<u>plaat</u> :	$d = 10 \text{ mm}$	S235	$f_y = 235 \text{ N/mm}^2$ $f_u = 360 \text{ N/mm}^2$			
				$V_{eff,1,Rd} = f_u A_{nt} / \gamma_{M_2} + (1 / \sqrt{3}) f_y A_{nv} / \gamma_{M_0} = 128,2 \text{ kN}$	$\geq N_{Ed} = 22,1 \text{ kN}$	(0,17)	
	$e_{1;1;min.} = 25 \text{ mm}$	$\alpha_d = 0,49$	$F_{v,Rd} = 60,3 \text{ kN}$	$\geq F_{v,Ed} = 11,1 \text{ kN}$	(0,18)		
	$e_{2;1;min.} = 25 \text{ mm}$	$k_1 = 2,42$	$F_{b,Rd} = 54,6 \text{ kN}$	$\geq F_{b,Ed} = 11,1 \text{ kN}$	(0,20)		

(krachten zie blz 36 ,10.2 numerieke computeruitvoer)

doorsnede klasse: 1	$\alpha y; z = 0,49$				
knikkromme : c	$\lambda_1 = 93,91$				
	$\bar{\lambda} = 1,89$	$\alpha h = 0,00$	$\alpha h = 0,00$		
		$C_{my} = 0,95$	$C_{mz} = 0,95$		
	$\Phi = 2,69$	$C_{mLT} = 0,95$	$C_{mLT} = 0,95$		
	$\chi = 0,22 \leq 1$	$K_{yy} = 1,359$	$K_{zz} = 1,359$	druk + buiging 6.61 : 0,84	≤ 1
	$\chi_{LT} = 1$	$K_{yz} = 0,816$	$K_{zy} = 0,816$	druk + buiging 6.62 : 0,84	≤ 1

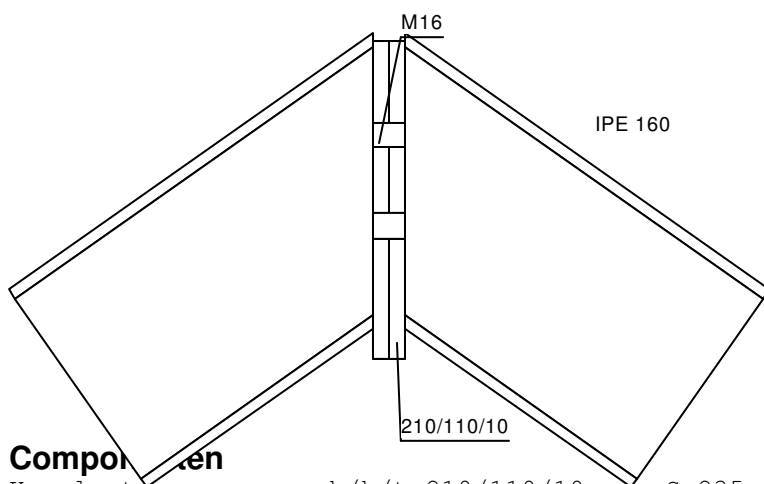
3.3 verbindingen NEN-EN 1993-1-8

Algemeen : Tenzij anders aangegeven in de voetplaatberekening geldt voor verankeringen voetplaten / beton
2x M16 4.6, inboordiepte 130mm met een randafstand >65mm
Voetplaatdikte $\geq 10\text{mm}$

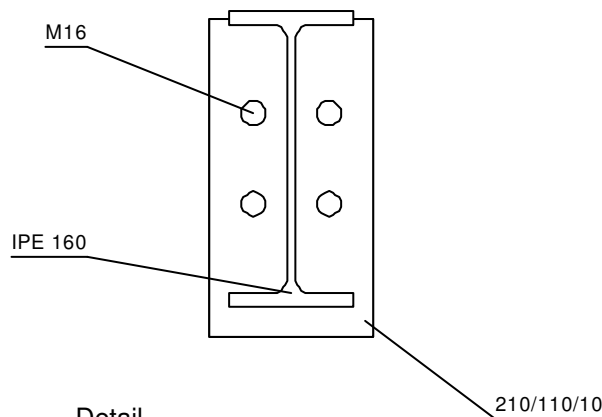
Algemene gegevens

Type constructie: Ongeschoord
Corrosieve omgeving: Nee
Knoopconfiguratie: Ligger stuikverbinding
Ligger: IPE 160, S 235, $\alpha = -35^\circ$, $L_b = 6500$ mm
Verbindingstype: Kopplaat-verbinding
Rekenprocedure: Eurocode 3
Berekeningsprocedure: EP - Elastische frame analyse / Plastische knooppberekening

Zij-aanzicht



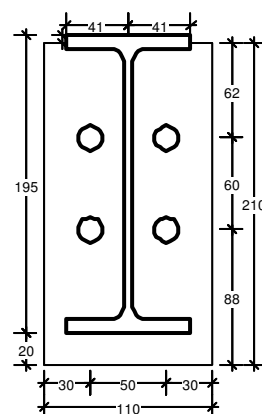
Doorsnede



Componenten

Kopplaat: b/h/t=210/110/10 mm, S 235
Bouten: 4 M16 8.8
Lassen
Ligger: $a_f = 4$ mm, $a_w = 4$ mm

Detail



Resultaten

positief moment

Weerstand

$M_{j,Rd} = 17.6$ kNm

$V_{j,Rd} = 68.9$ kN

Stijfheid

$S_{j,ini} = 14128$ kNm/rad

Classificatie

Sterkte : Niet-volledig sterk

Stijfheid : Stijf

Bezwijkvorm

Liggerflens op druk

negatief moment

Weerstand

$M_{j,Rd} = 17.6$ kNm

$V_{j,Rd} = 68.9$ kN

Stijfheid

$S_{j,ini} = 14039$ kNm/rad

Classificatie

Sterkte : Niet-volledig sterk

Stijfheid : Stijf

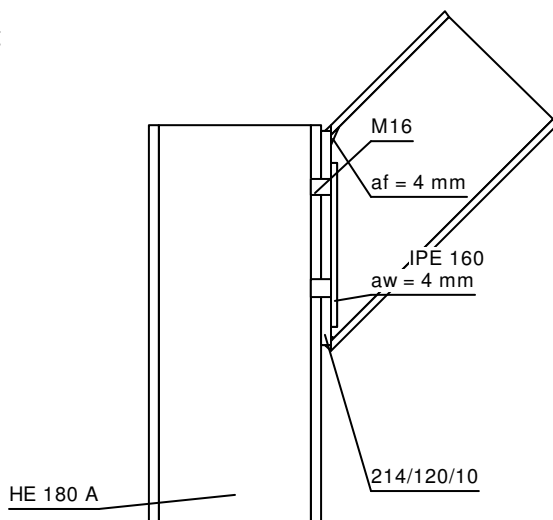
Bezwijkvorm

Liggerflens op druk

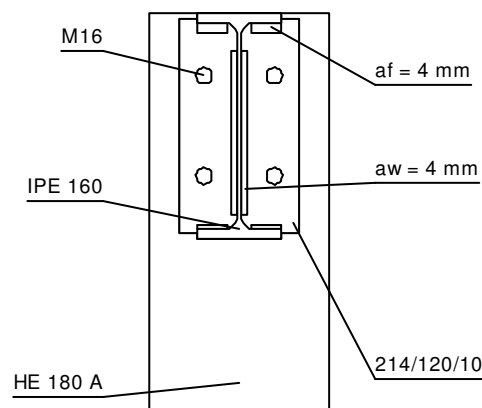
Algemene gegevens

Type constructie: Geschoord
 Corrosieve omgeving: Nee
 Knoopconfiguratie: Enkelzijdige ligger-kolom verbinding, bovenaan kolom
 Ligger: IPE 160, S 235, $\alpha = 45^\circ$, $L_b = 2000$ mm
 Kolom: HEA 180, S 235
 Verbindingstype: Kopplaat-verbinding
 Rekenprocedure: Eurocode 3
 Berekeningsprocedure: EP - Elastische frame analyse / Plastische knooppberekening

Zij-aanzicht



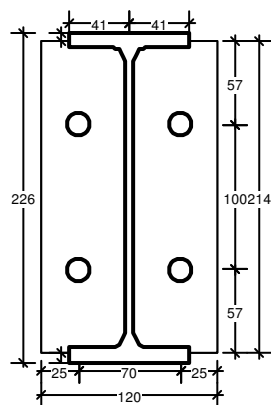
Doorsnede



Detail

Componenten

Kopplaat: b/h/t=214/120/10 mm, S 235
 Bouten: 4 M16 8.8
 Lassen
 Ligger: $a_f = 4$ mm, $a_w = 4$ mm



Resultaten

positief moment

Weerstand

$M_{j,Rd} = 19.6$ kNm

$V_{j,Rd} = 68.9$ kN

Stijfheid

$S_{j,ini} = 4210$ kNm/rad

Classificatie

Sterkte : Niet-volledig sterk

Stijfheid : Flexibel

Bezwijkvorm

Liggerflens op druk

negatief moment

Weerstand

$M_{j,Rd} = 18.0$ kNm

$V_{j,Rd} = 155.0$ kN

Stijfheid

$S_{j,ini} = 3728$ kNm/rad

Classificatie

Sterkte : Niet-volledig sterk

Stijfheid : Flexibel

Bezwijkvorm

Kolomlijf op druk

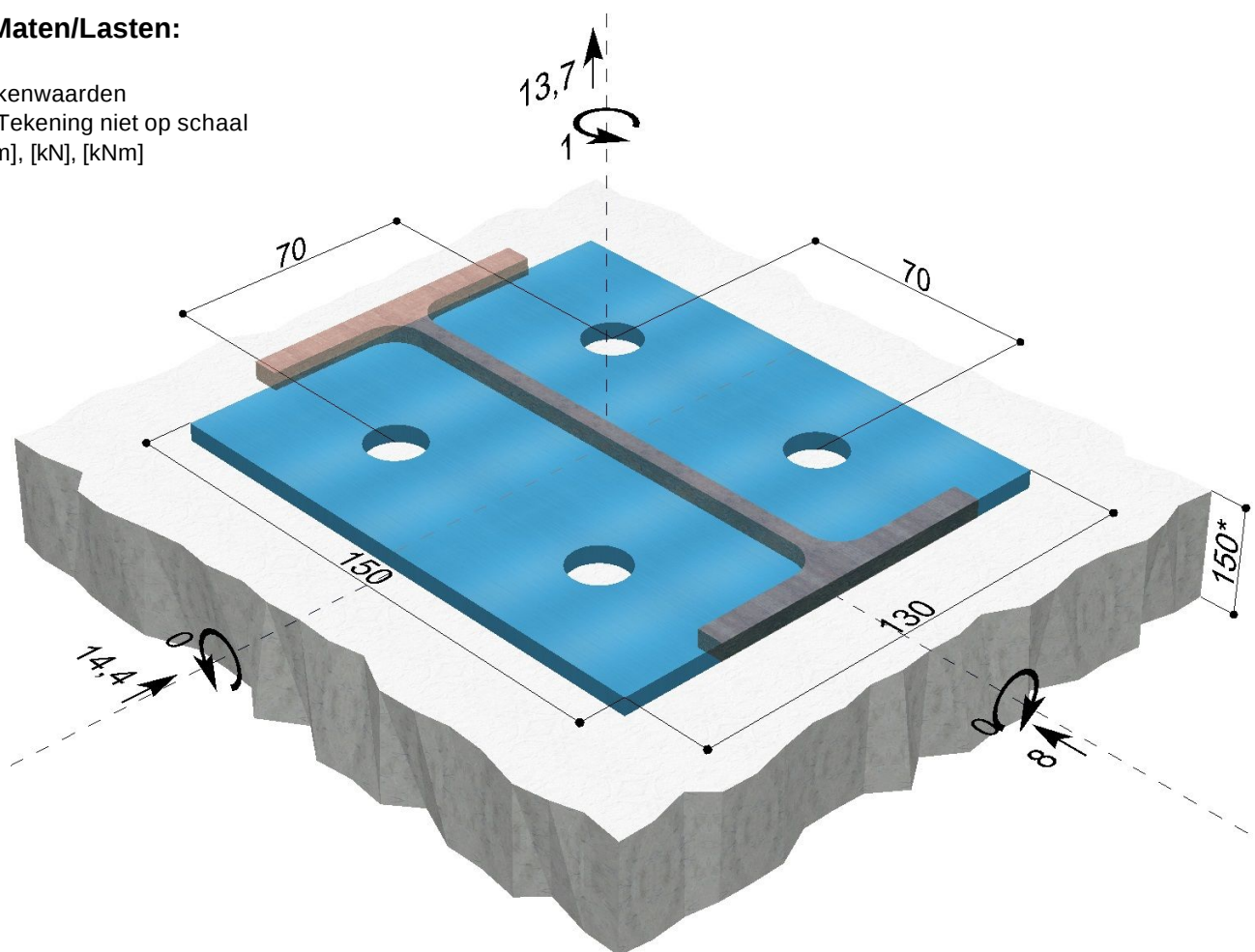
Bedrijf/Opsteller		fischer  BEVESTIGINGSSYSTEMEN
Straat		
Postcode / Plaats		COMPUFIX 8.4
Tel. / Fax		8.4.4282.27076/22/2746
Project	Schuur Venekamp / van Lingen	Pagina 1 van afdruk nr. 34
Bouwdeel	Voetplaat	Datum: 8-7-2015
Opmerkingen		

fischer COMPUFIX: Berekend volgens ETAG, Technical Report TR 029

Belastingtype:	Statische belasting
Anker:	fischer Injektionssystem: FIS A M16x130 (5.8) (Art. Nr. 44972) uit elektrolytisch verzinkt staal met een verankeringsdiepte van $h_{ef} = 80 \text{ mm}$ + Injectiemortel FIS EM in verschillende diameters
Ondergrond:	Gescheurd beton, normaal gewapend Betonsterkteklasse: C 20/25
Randwapening:	Zonder invloed
Ankerbuiging:	Niet aanwezig
Temperatuur:	Langeduur temperatuur: 35°C, Korteduur temperatuur: 60°C
Ankerplaat::	Geen berekening beschikbaar

1 Maten/Lasten:

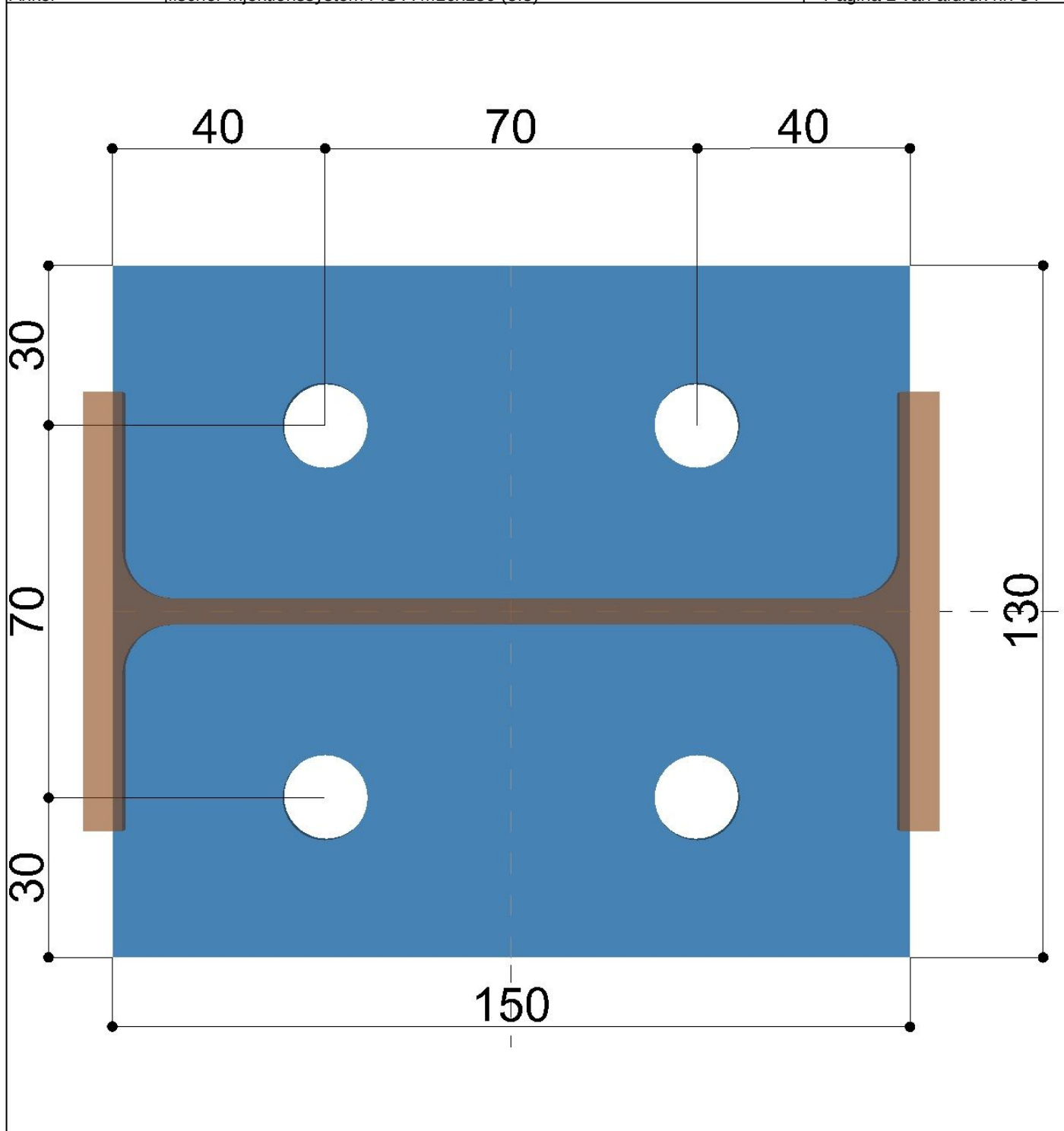
Rekenwaarden
 (*) Tekening niet op schaal
 [mm], [kN], [kNm]



Trekbelasting	Uitnuttingsgraad	Afschuifbelasting	Uitnuttingsgraad	gecombineerde belasting	Uitnuttingsgraad
Staalbreuk:	6,5 %	Staalbreuk:	29,1 %		93,9 %
Betonkegelbreuk:	57,4 %	Betonachteruitbreken:	63,4 %		
Combinatie van uittrekken en betonkegelbreuk:	52,5 %				

Resultaat: Rekentechnische toetsing anker is succesvol
 LET OP: Volledige print van de berekening is noodzakelijk.

Bedrijf/Opsteller		fischer 
Project	Schuur Venekamp / van Lingen	BEVESTIGINGSSYSTEMEN
Bouwdeel	Voetplaat	
Anker	fischer Injektionssystem FIS A M16x130 (5.8)	Pagina 2 van afdruk nr. 34



INVOER : wandregel :

gebruiksfunctie : wandregel

plaatsing : 1-velds

balkmaat : geschaafd 71 x 171

steunpunt : discreet

controle : enkele buiging

$A = 12141,0 \text{ mm}^2$

$W_y = 346,0 \cdot 10^3 \text{ mm}^3$

$W_z = 143,7 \cdot 10^3 \text{ mm}^3$

$I_y = 2958,5 \cdot 10^4 \text{ mm}^4$

$I_z = 510,0 \cdot 10^4 \text{ mm}^4$

$i_y = 49,4 \text{ mm}$

$i_z = 20,5 \text{ mm}$

hout : gezaagd

sterkteklasse : C24

klimaatklasse : 1

belastingduurklasse BB : blijvend

belastingduurklasse OB : kort

h.o.h afstand wandregel : 1,850 m

overspanning wandregel : 5,00 m

$W_{\max} = 33,3 \text{ mm} \quad (L/150)$

opleglengte : 100 mm

dikte beschot : 8 mm

sterkteklasse beschot : C18

$S = 0,12$

uitkapping : ja

uitkapping h= 30 mm boven

$\gamma_M = 1,30$

$\kappa_{\text{mod}}; \text{BB} = 0,60$

$\kappa_{\text{mod}}; \text{BB}; t; 90 = 0,50$

$\kappa_{\text{mod}}; \text{OB} = 0,90$

$\kappa_{\text{mod}}; \text{OB}; t; 90 = 0,80$

$k_{\text{def}} = 0,60$

$K_h; h = 1,00$

$K_h; b = 1,16$

$K_{\ell} = 0,97$

$K_r = 1,00$

$K_m = 0,70$

$K_{\text{cr}} = 0,67$

$f_{m;0;k} = 24,00 \text{ N/mm}^2$

$f_{t;0;k} = 14,00 \text{ N/mm}^2$

$f_{t;90;k} = 0,40 \text{ N/mm}^2$

$f_{c;0;k} = 21,00 \text{ N/mm}^2$

$f_{c;90;k} = 2,50 \text{ N/mm}^2$

$f_{v;0;k} = 4,00 \text{ N/mm}^2$

$E_{0;\text{mean};k} = 11000 \text{ N/mm}^2$

$E_{90;\text{mean};k} = 370 \text{ N/mm}^2$

$E_{0,05;k} = 7400 \text{ N/mm}^2$

$G_k = 690 \text{ N/mm}^2$

$\rho_k = 350 \text{ kg/m}^3$

$f_{m;y;d} = 16,62 \text{ N/mm}^2$

$f_{m;z;d} = 19,30 \text{ N/mm}^2$

$f_{t;0;d} = 10,92 \text{ N/mm}^2$

$f_{t;90;d} = 0,25 \text{ N/mm}^2$

$f_{c;0;d} = 14,54 \text{ N/mm}^2$

$f_{c;90;d} = 1,73 \text{ N/mm}^2$

$f_{v;d} = 2,77 \text{ N/mm}^2$

$E_{0;\text{mean};d} = 11000 \text{ N/mm}^2$

$E_{90;\text{mean};d} = 370 \text{ N/mm}^2$

$E_{0,05;d} = 7400 \text{ N/mm}^2$

$G_d = 690 \text{ N/mm}^2$

$E_{0;u;d} = 7615 \text{ N/mm}^2$

$K_{c,90} = 1$

belastingen :(0,70 kN/m²) wind gevel; trek : 1,299 kN/m¹(0,68 kN/m²) wind gevel; druk : 1,252 kN/m¹UGT druk : 1,690 kN/m¹UGT trek : 1,754 kN/m¹BGT druk : 1,252 kN/m¹BGT trek : 1,299 kN/m¹

ogu

$\gamma_G = 1,35$

$\gamma_G = 1,20$

$\gamma_Q = 1,50$

CC klasse aanpassen : nee

$K_{FI} = 0,90 \quad (CC1)$

UITVOER :maatgevend :

$N_t; E_d = 0,00 \text{ kN}$

$N_c; E_d = 0,00 \text{ kN}$

$V_y; E_d = 4,38 \text{ kN}$

$M_y; E_d = 5,48 \text{ kNm}$

$W; \text{initial} = 32,5 \text{ mm}$

$W; \text{bij} = 0,0 \text{ mm}$

$W; \text{fin} = 32,5 \text{ mm}$

wind gevel; trek

wind gevel; trek

TOETSING : NEN EN 1995-1-1

$(6.1.2) \quad \sigma_{t,0,d} = 0,00 \text{ N/mm}^2 \leq 10,92 \text{ N/mm}^2$

$(6.1.4) \quad \sigma_{c,0,d} = 0,00 \text{ N/mm}^2 \leq 14,54 \text{ N/mm}^2$

$(6.1.5) \quad \sigma_{c,90,d} = 0,62 \text{ N/mm}^2 \leq 2,60 \text{ N/mm}^2$

$\sigma_{m,y;d} = 15,84 \text{ N/mm}^2$

$\sigma_{m,z;d} = 0,00 \text{ N/mm}^2$

$(6.1.6 (6.11)) \quad u_c = 0,953 \leq 1$

$(6.1.6 (6.12)) \quad u_c = 0,667 \leq 1$

$(6.1.7 (6.13)) \quad \tau_{y;d} = 0,65 \text{ N/mm}^2 \leq 2,77 \text{ N/mm}^2 \quad (K_v = 1,00)$

$(7.2) \quad u_c; \text{bij} = 0,00 \leq 1$

$(7.2) \quad u_c; \text{net, fin} = 0,97 \leq 1$

INVOER : *gording :*

gebruiksfunctie : gording

plaatsing : 1-velds

balkmaat : geschaafd 71 x 221

steunpunt : discreet

controle : enkele buiging

(nokgordingen aan elkaar doorverbinden)

hout : gezaagd

$$A = 15691,0 \text{ mm}^2$$

$$W_y = 578,0 \cdot 10^3 \text{ mm}^3$$

$$W_z = 185,7 \cdot 10^3 \text{ mm}^3$$

$$I_y = 6386,4 \cdot 10^4 \text{ mm}^4$$

$$I_z = 659,2 \cdot 10^4 \text{ mm}^4$$

$$i_y = 63,8 \text{ mm}$$

$$i_z = 20,5 \text{ mm}$$

sterkteklasse : C24

klimaatklasse : 1

belastingduurklasse BB : blijvend

belastingduurklasse OB : kort

h.o.h afstand gording : 2,00 m

overspanning gording : 5,00 m

opleglengte : 100 mm

dikte beschot : 8 mm

S= 0,12

uitkapping : ja

uitkapping h= 30 mm boven

$$W_{\max} = 20,0 \text{ mm}$$

sterkteklasse beschot : C18

$$\gamma_M = 1,30$$

$$\kappa_{\text{mod}}; \text{BB} = 0,60$$

$$\kappa_{\text{mod}}; \text{BB}; t; 90 = 0,50$$

$$\kappa_{\text{mod}}; \text{OB} = 0,90$$

$$\kappa_{\text{mod}}; \text{OB}; t; 90 = 0,80$$

$$\kappa_{\text{def}} = 0,60$$

$$K_h; h = 1,00$$

$$K_h; b = 1,16$$

$$K_{\ell} = 0,97$$

$$K_r = 1,00$$

$$K_m = 0,70$$

$$K_{\text{cr}} = 0,67$$

$$f_{m;0;k} = 24,00 \text{ N/mm}^2$$

$$f_{t;0;k} = 14,00 \text{ N/mm}^2$$

$$f_{t;90;k} = 0,40 \text{ N/mm}^2$$

$$f_{c;0;k} = 21,00 \text{ N/mm}^2$$

$$f_{c;90;k} = 2,50 \text{ N/mm}^2$$

$$f_{v;0;k} = 4,00 \text{ N/mm}^2$$

$$E_{0;\text{mean};k} = 11000 \text{ N/mm}^2$$

$$E_{90;\text{mean};k} = 370 \text{ N/mm}^2$$

$$E_{0,05;k} = 7400 \text{ N/mm}^2$$

$$G_k = 690 \text{ N/mm}^2$$

$$\rho_k = 350 \text{ kg/m}^3$$

$$f_{m;y;d} = 16,62 \text{ N/mm}^2$$

$$f_{m;z;d} = 19,30 \text{ N/mm}^2$$

$$f_{t;0;d} = 10,92 \text{ N/mm}^2$$

$$f_{t;90;d} = 0,25 \text{ N/mm}^2$$

$$f_{c;0;d} = 14,54 \text{ N/mm}^2$$

$$f_{c;90;d} = 1,73 \text{ N/mm}^2$$

$$f_{v;d} = 2,77 \text{ N/mm}^2$$

$$E_{0;\text{mean};d} = 11000 \text{ N/mm}^2$$

$$E_{90;\text{mean};d} = 370 \text{ N/mm}^2$$

$$E_{0,05;d} = 7400 \text{ N/mm}^2$$

$$G_d = 690 \text{ N/mm}^2$$

$$E_{0;u;d} = 7615 \text{ N/mm}^2$$

$$K_{c,90} = 1$$

belastingen :

$$Q_k = 2,00 \text{ kN}$$

$$(0,25 \text{ kN/m}^2)$$

$$(0,15 \text{ kN/m}^2)$$

$$(0,56 \text{ kN/m}^2)$$

$$(0,65 \text{ kN/m}^2)$$

$$\text{BB dak} : 0,506 \text{ kN/m}^1$$

$$\text{sneeuw} : 0,300 \text{ kN/m}^1$$

$$\text{wind dak; trek} : 1,127 \text{ kN/m}^1$$

$$\text{wind dak; druk} : 1,299 \text{ kN/m}^1$$

$$\text{UGT druk} : 2,300 \text{ kN/m}^1$$

$$\text{UGT trek} : -1,066 \text{ kN/m}^1$$

$$\text{BGT druk} : 1,805 \text{ kN/m}^1$$

$$\text{BGT trek} : -0,621 \text{ kN/m}^1$$

ogu

$$\gamma_G = 1,35$$

$$\gamma_G = 1,20$$

$$\gamma_Q = 1,50$$

CC klasse aanpassen : nee

$$K_{FI} = 0,90 \quad ()$$

UITVOER :**maatgevend :**

$$N_{t;Ed} = 0,00 \text{ kN}$$

$$N_{c;Ed} = 0,00 \text{ kN}$$

$$V_{y;Ed} = 5,35 \text{ kN}$$

$$M_{y;Ed} = 5,96 \text{ kNm}$$

$$W_{\text{initial}} = 5,9 \text{ mm}$$

$$W_{\text{bij}} = 7,0 \text{ mm}$$

$$W_{\text{fin}} = 12,9 \text{ mm}$$

BB+wind dak;druk :

BB+wind dak;druk :

TOETSING : NEN EN 1995-1-1

$$(6.1.2) \quad \sigma_{t,0,d} = 0,00 \text{ N/mm}^2 \leq 10,92 \text{ N/mm}^2$$

$$(6.1.4) \quad \sigma_{c,0,d} = 0,00 \text{ N/mm}^2 \leq 14,54 \text{ N/mm}^2$$

$$(6.1.5) \quad \sigma_{c,90,d} = 0,75 \text{ N/mm}^2 \leq 2,60 \text{ N/mm}^2$$

$$\sigma_{m,y;d} = 10,32 \text{ N/mm}^2$$

$$\sigma_{m,z;d} = 0,00 \text{ N/mm}^2$$

$$(6.1.6 (6.11)) \quad u_c = 0,621 \leq 1$$

$$(6.1.6 (6.12)) \quad u_c = 0,435 \leq 1$$

$$(6.1.7 (6.13)) \quad \tau_{y;d} = 0,59 \text{ N/mm}^2 \leq 2,77 \text{ N/mm}^2 \quad (K_v = 1,00)$$

$$(7.2) \quad u_{c;\text{bij}} = 0,47 \leq 1$$

$$(7.2) \quad u_{c;\text{net,fin}} = 0,64 \leq 1$$

10.1 - grafische computer in- en uitvoer



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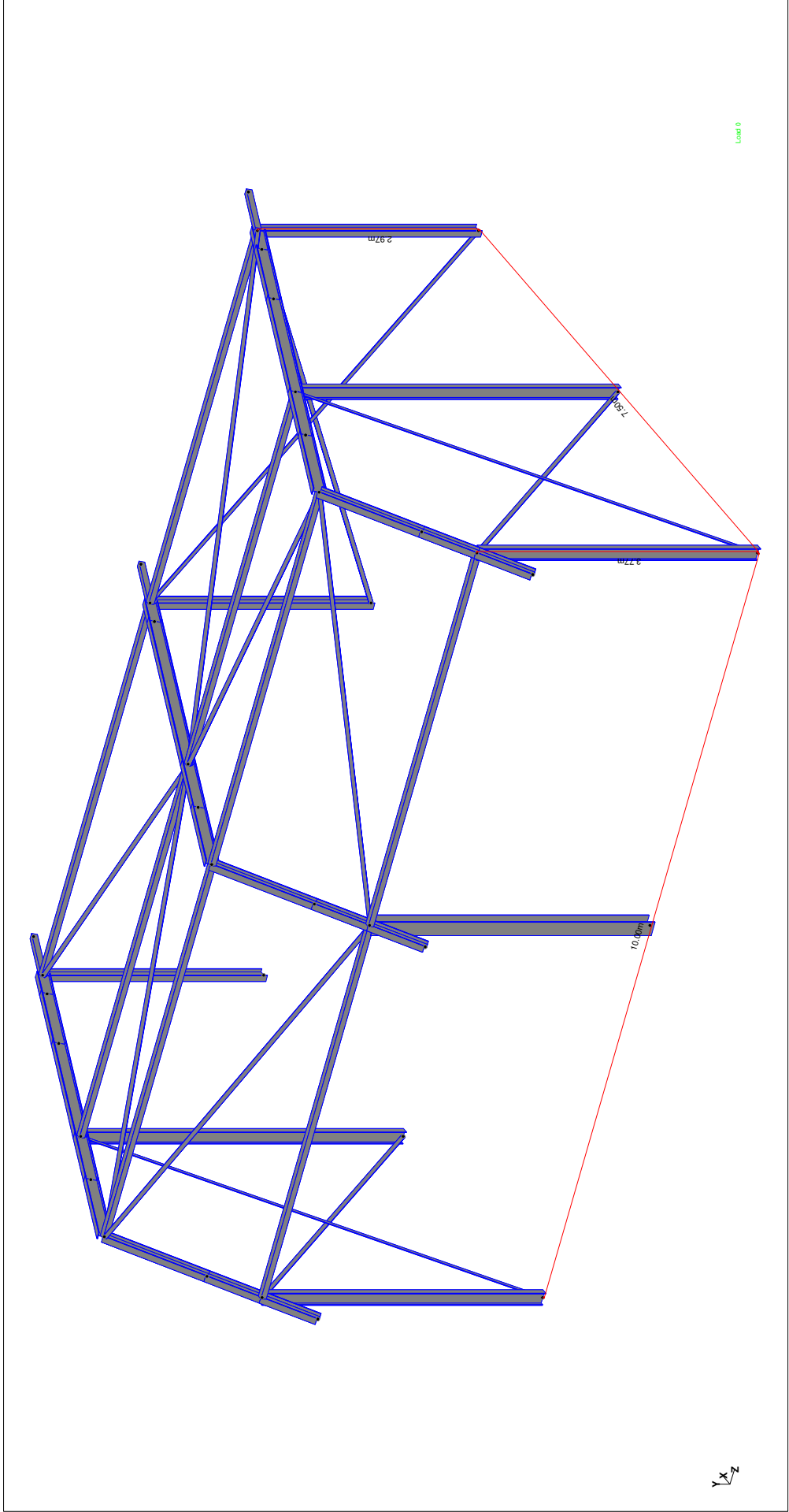
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3D staalconstructie



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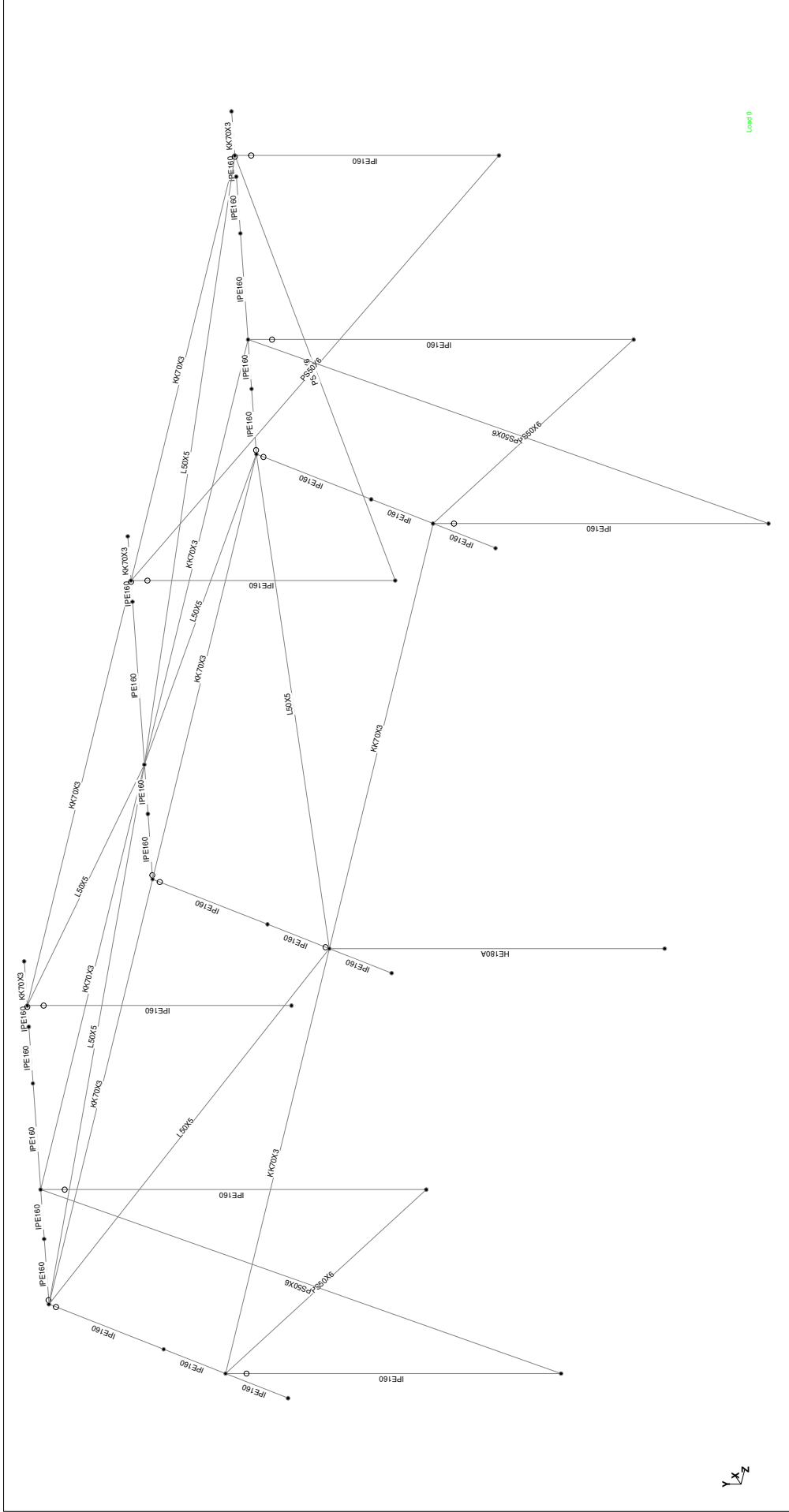
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Job No 9111-011

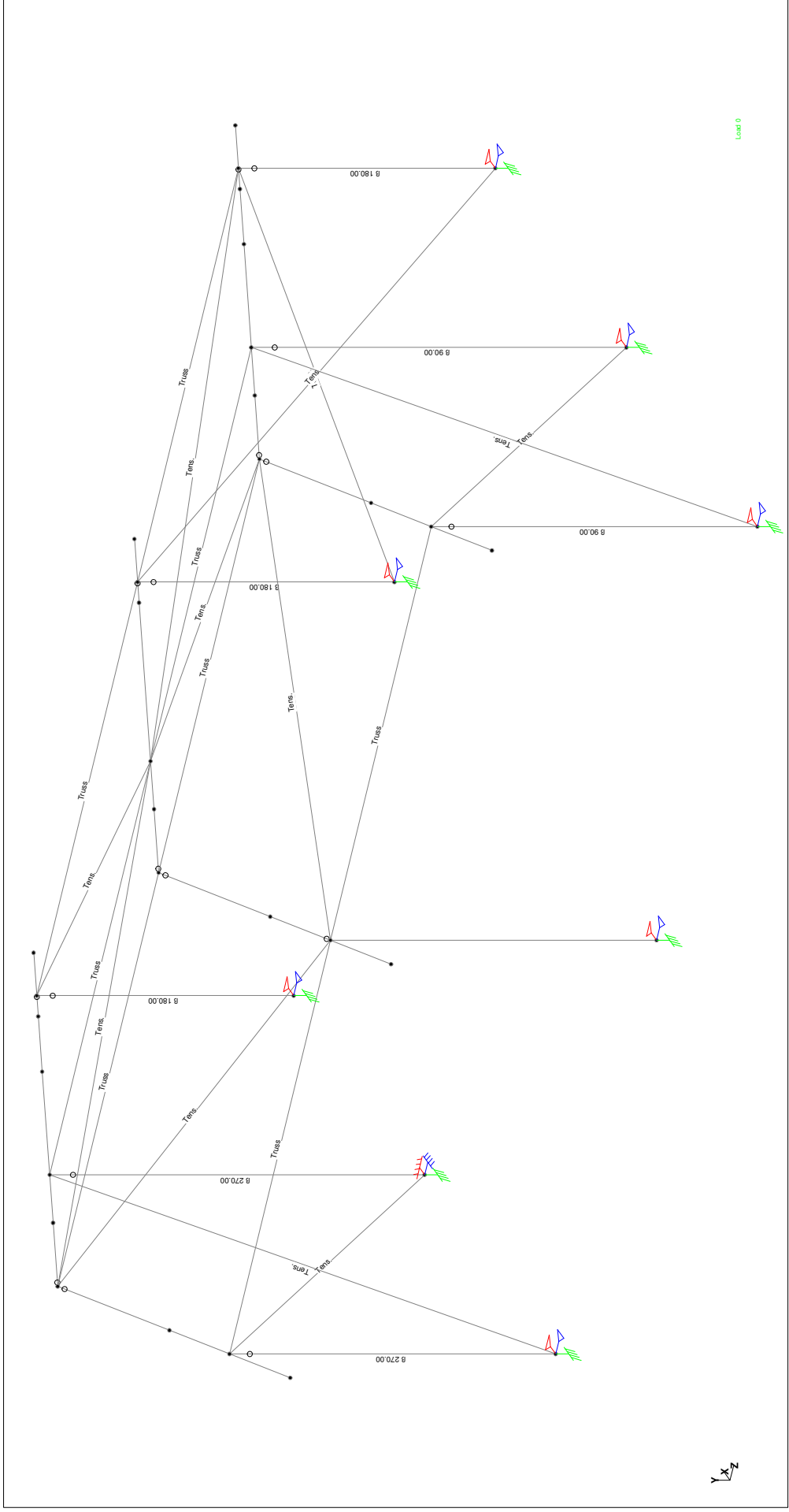
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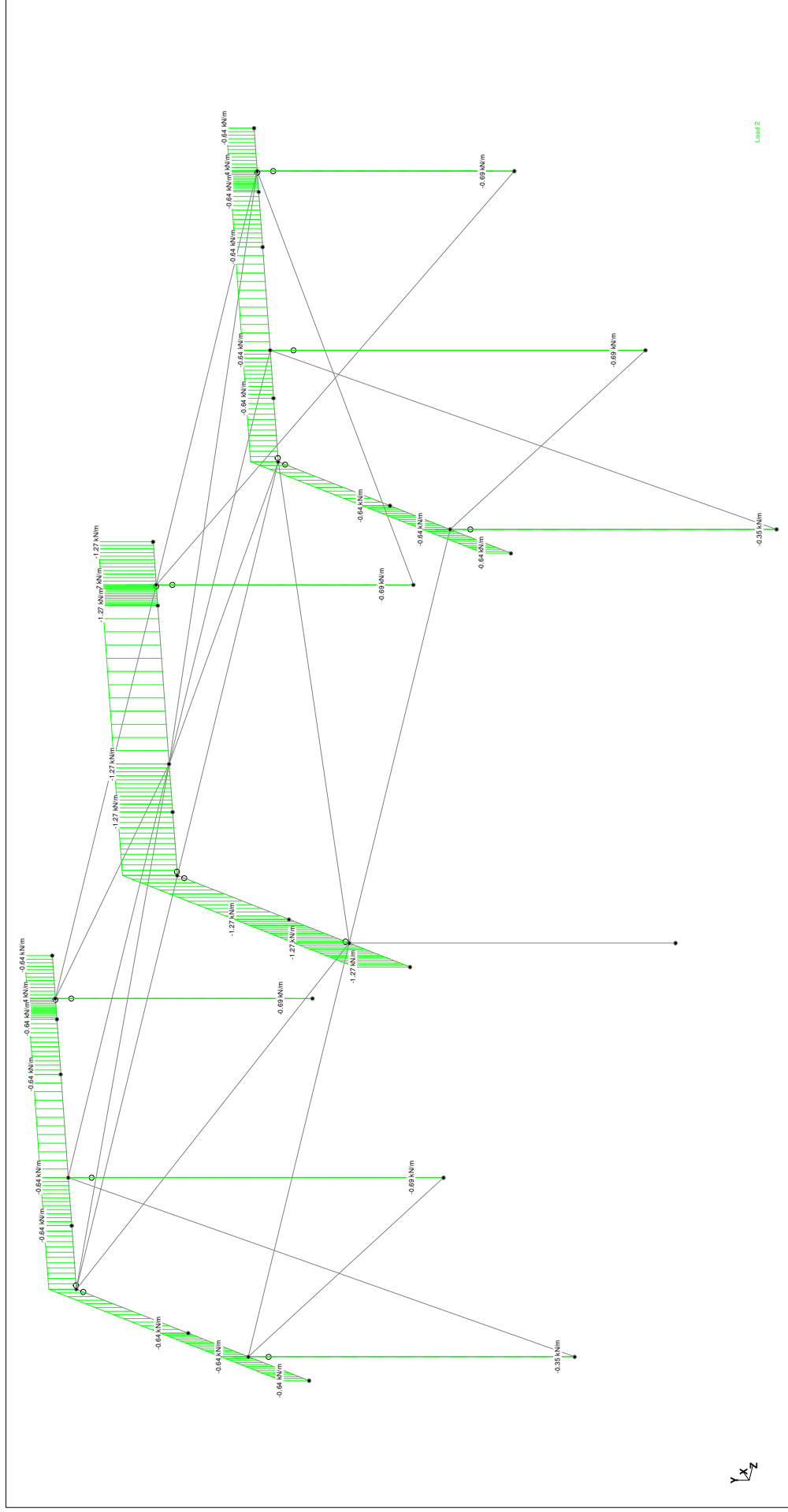
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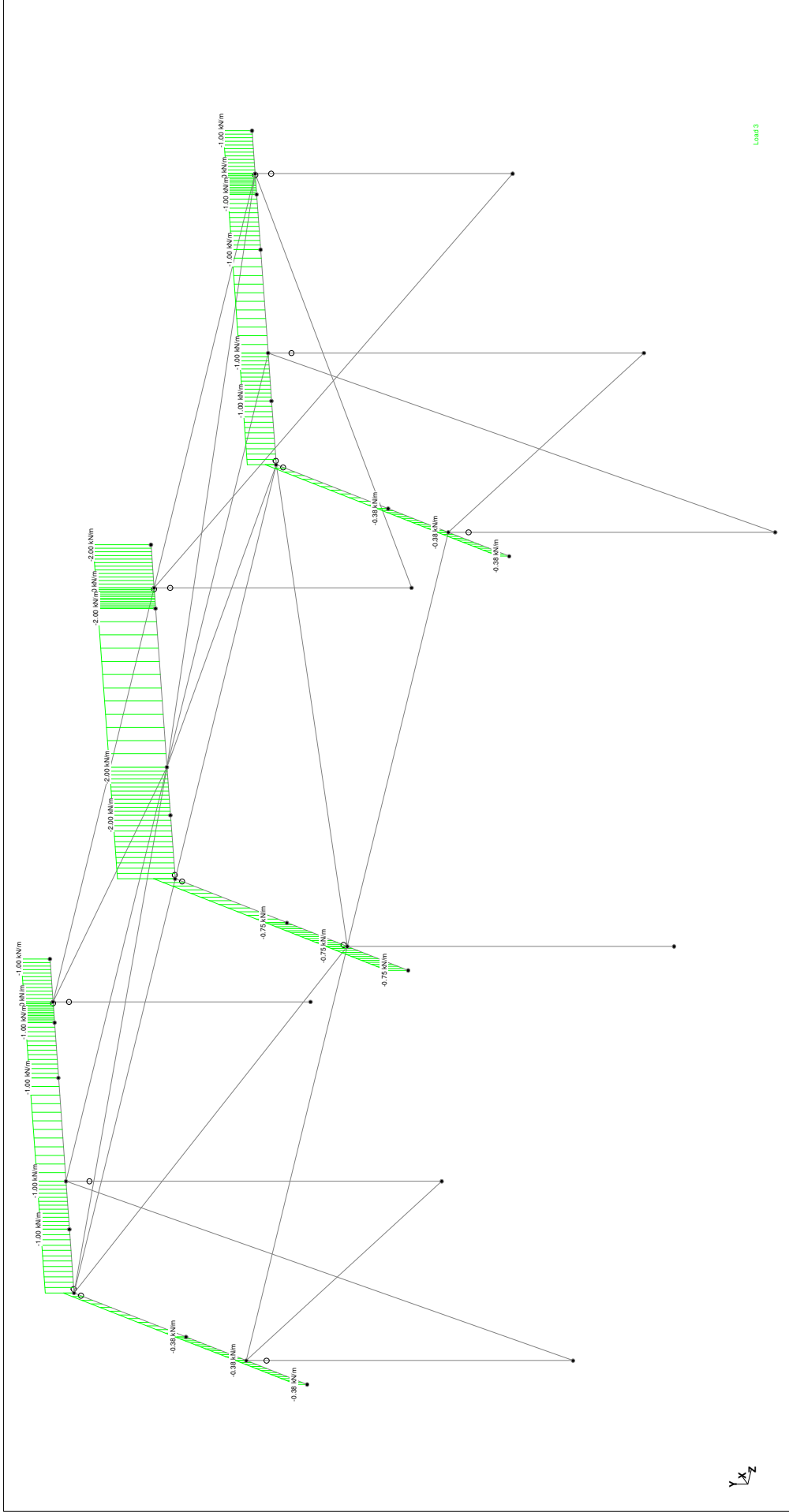
Rev



profiling









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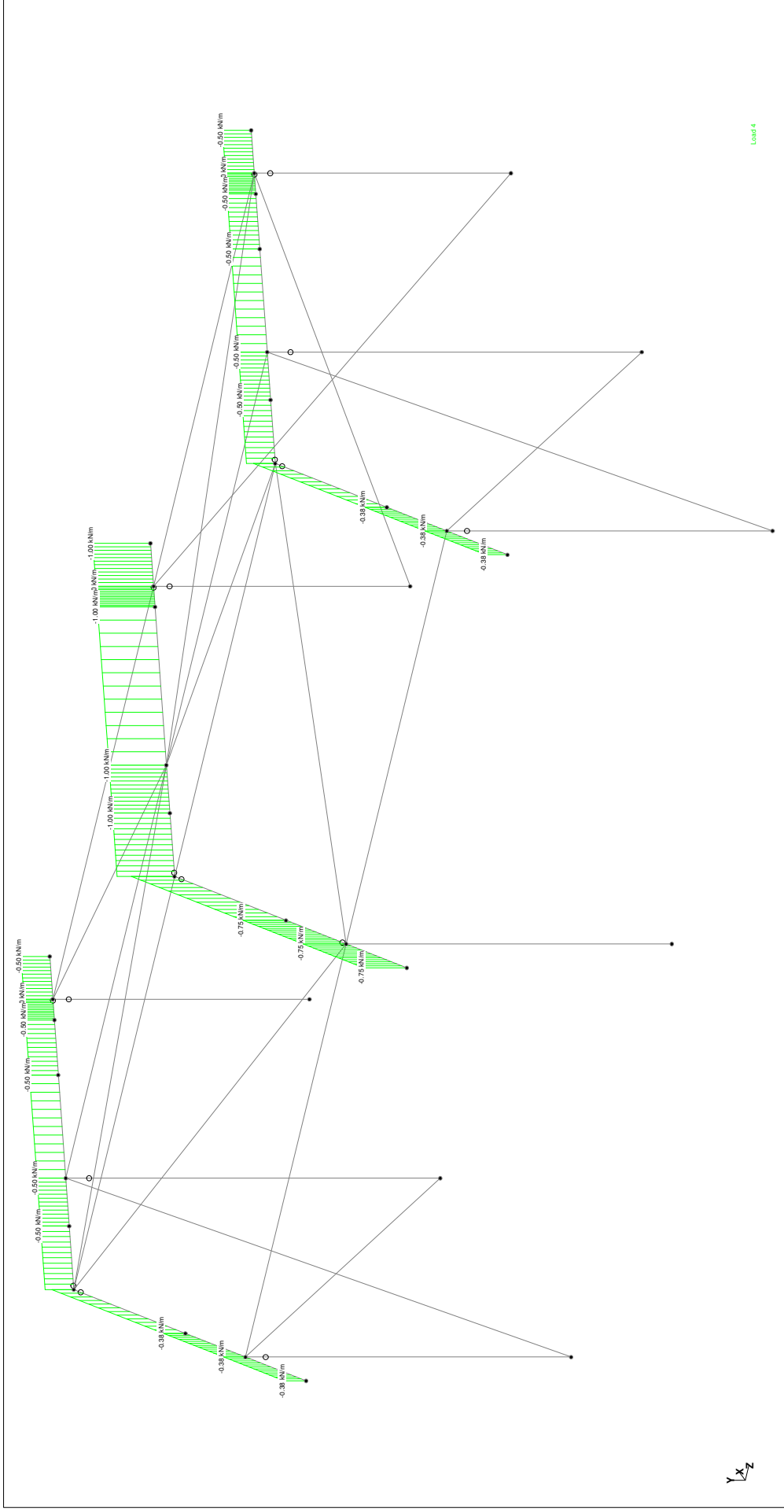
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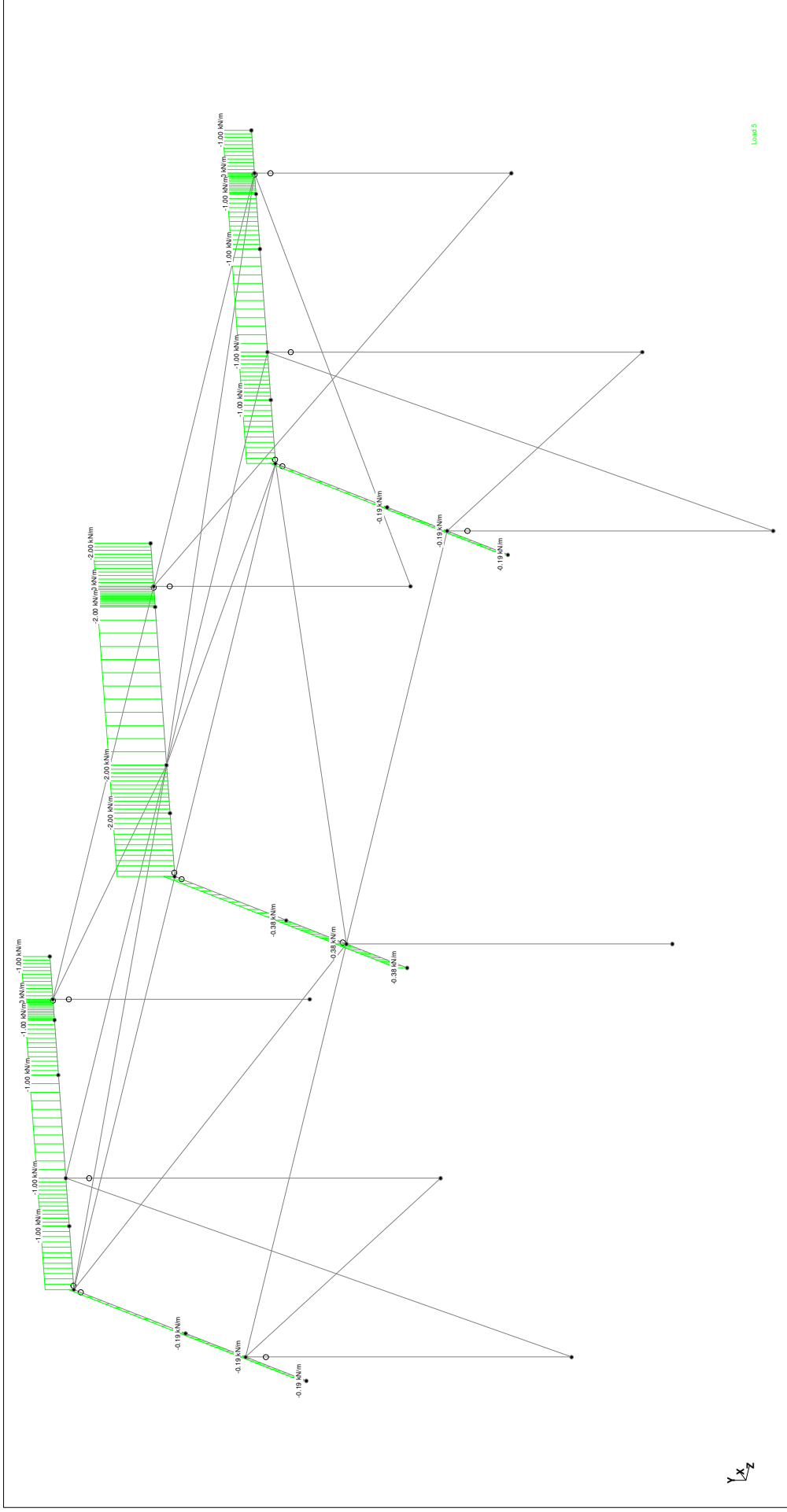
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BG4: sneeuw 2





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Ref

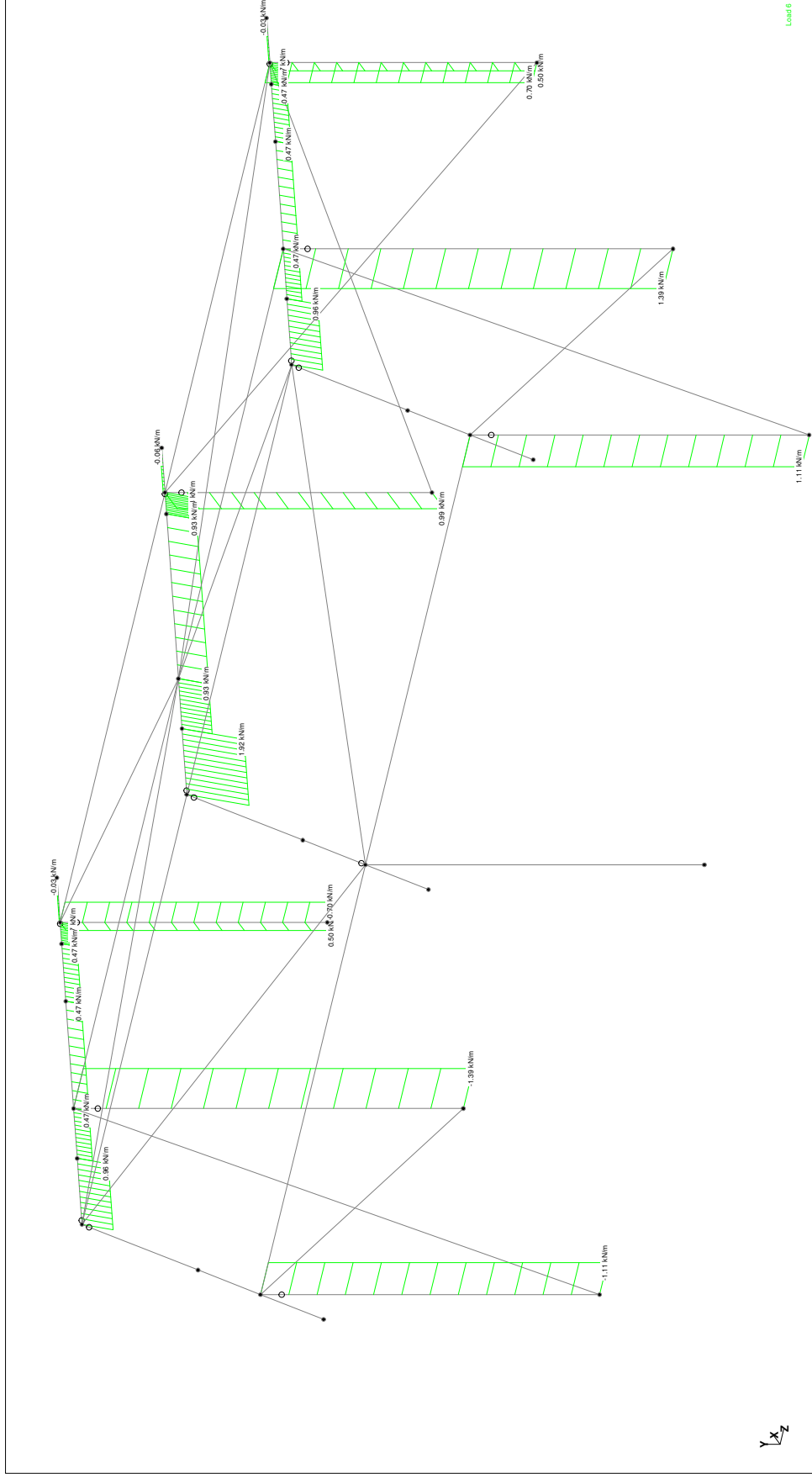
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07-Jul-15		

Date/Time	08-Jul-2015 14:01
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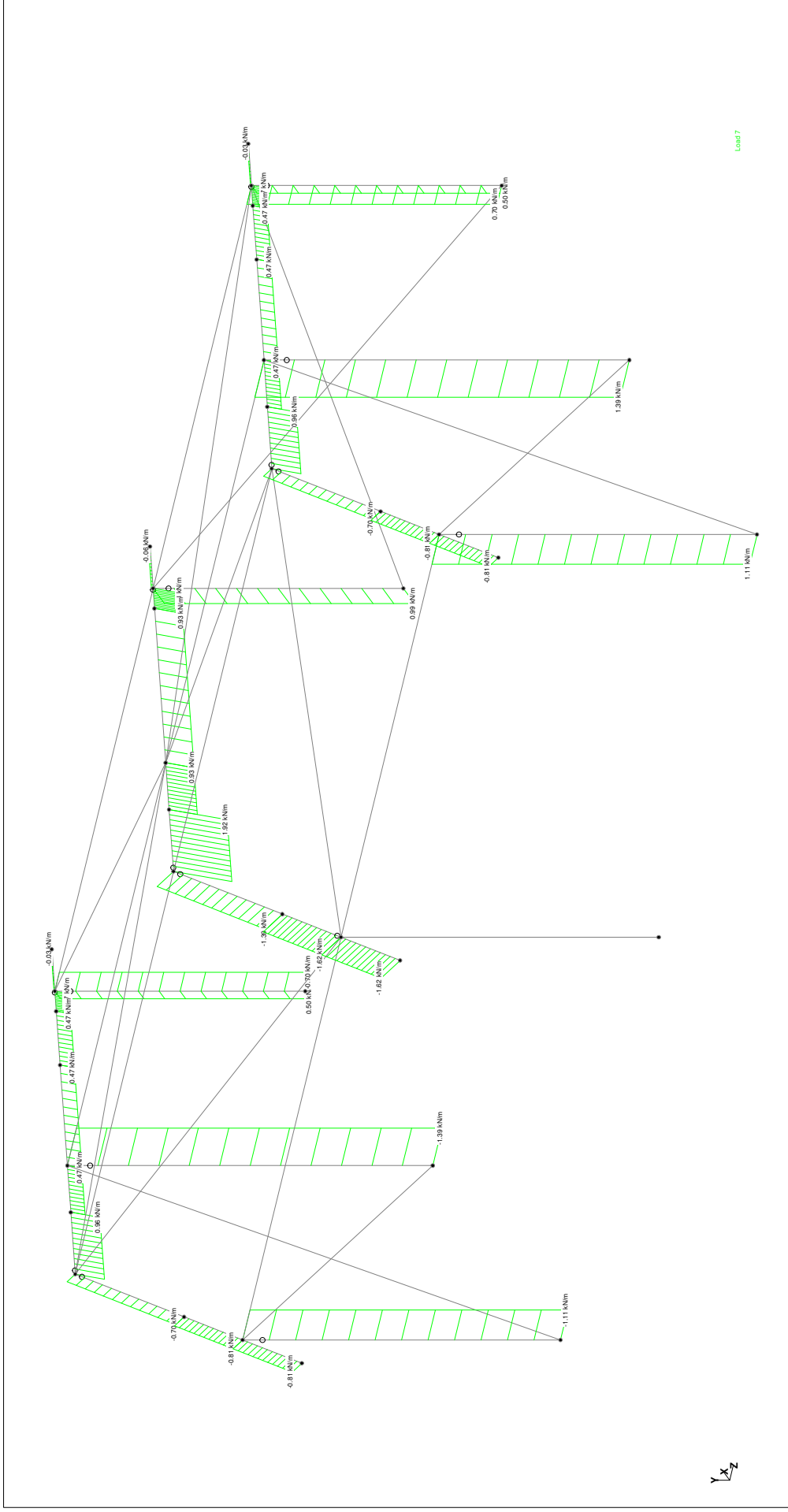
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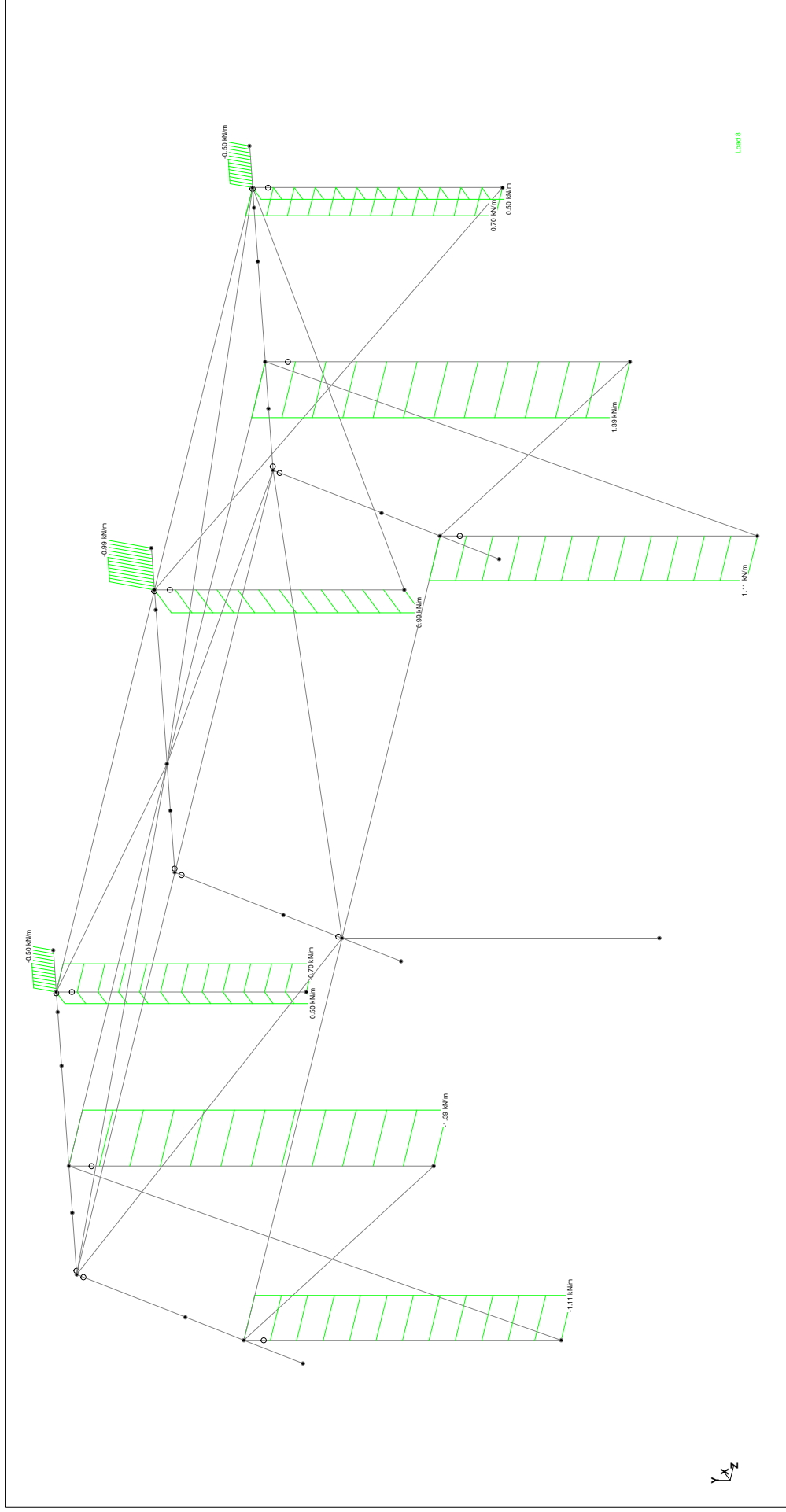
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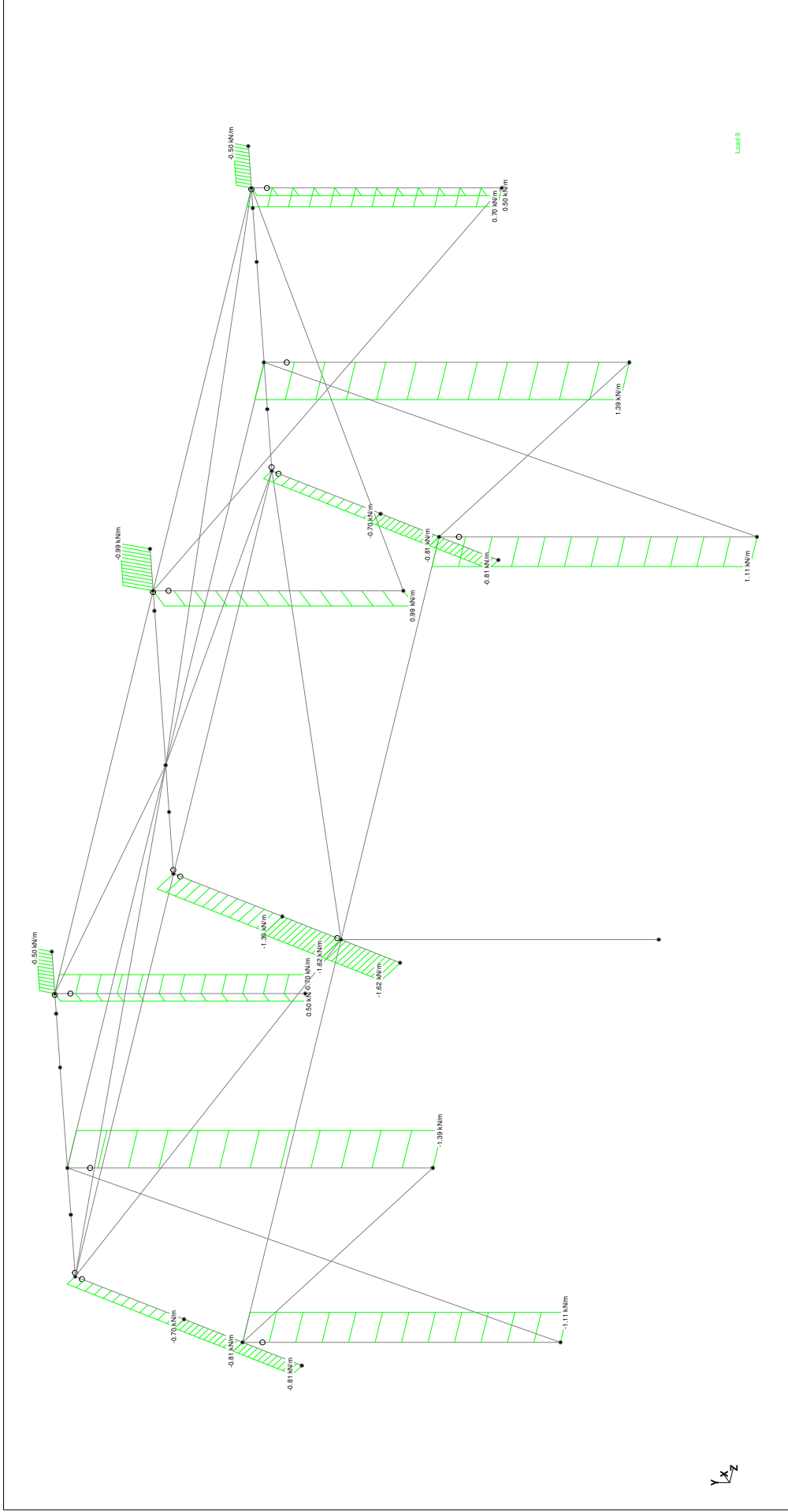
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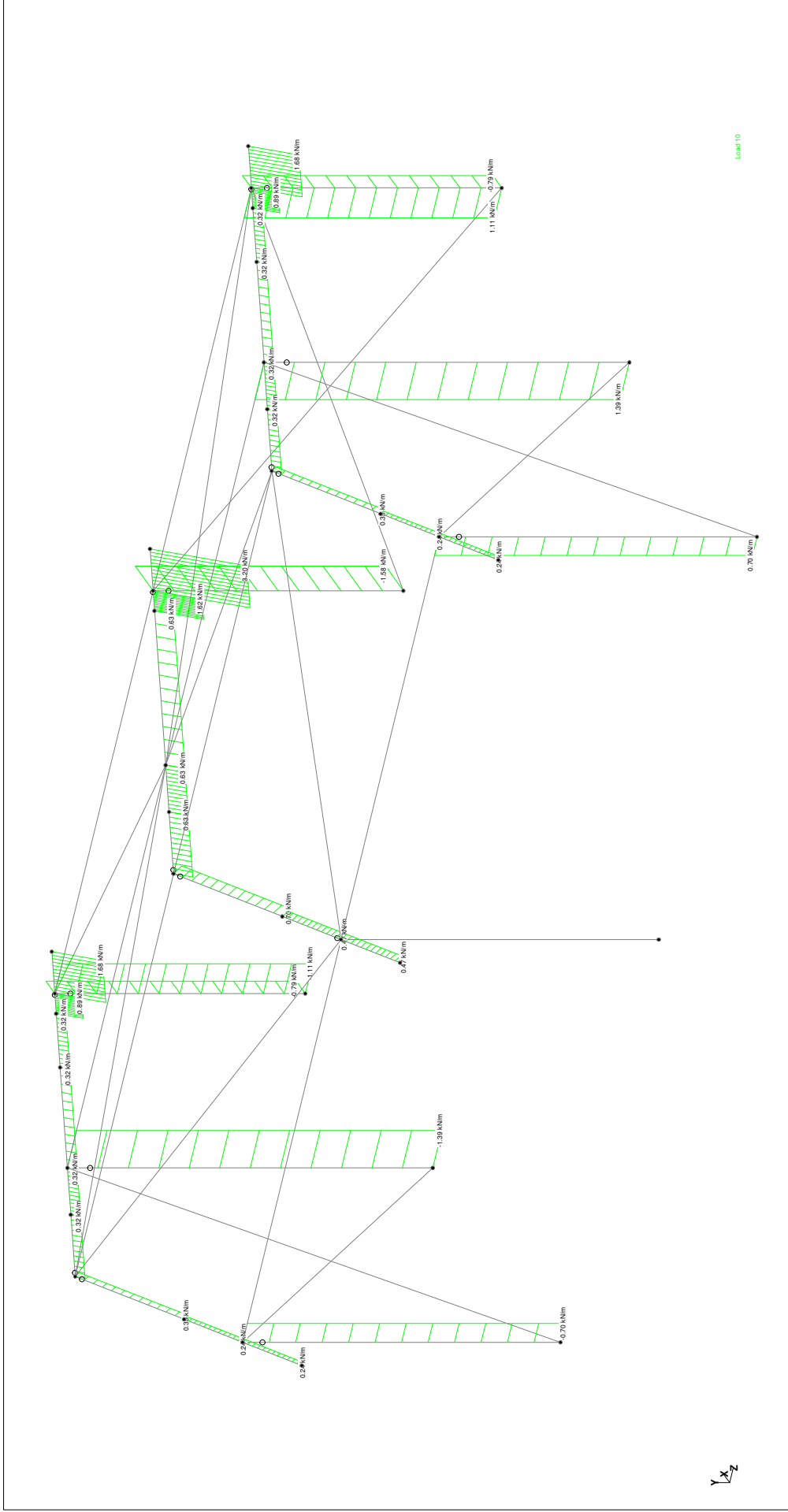
BG6: wind X1





Load 8







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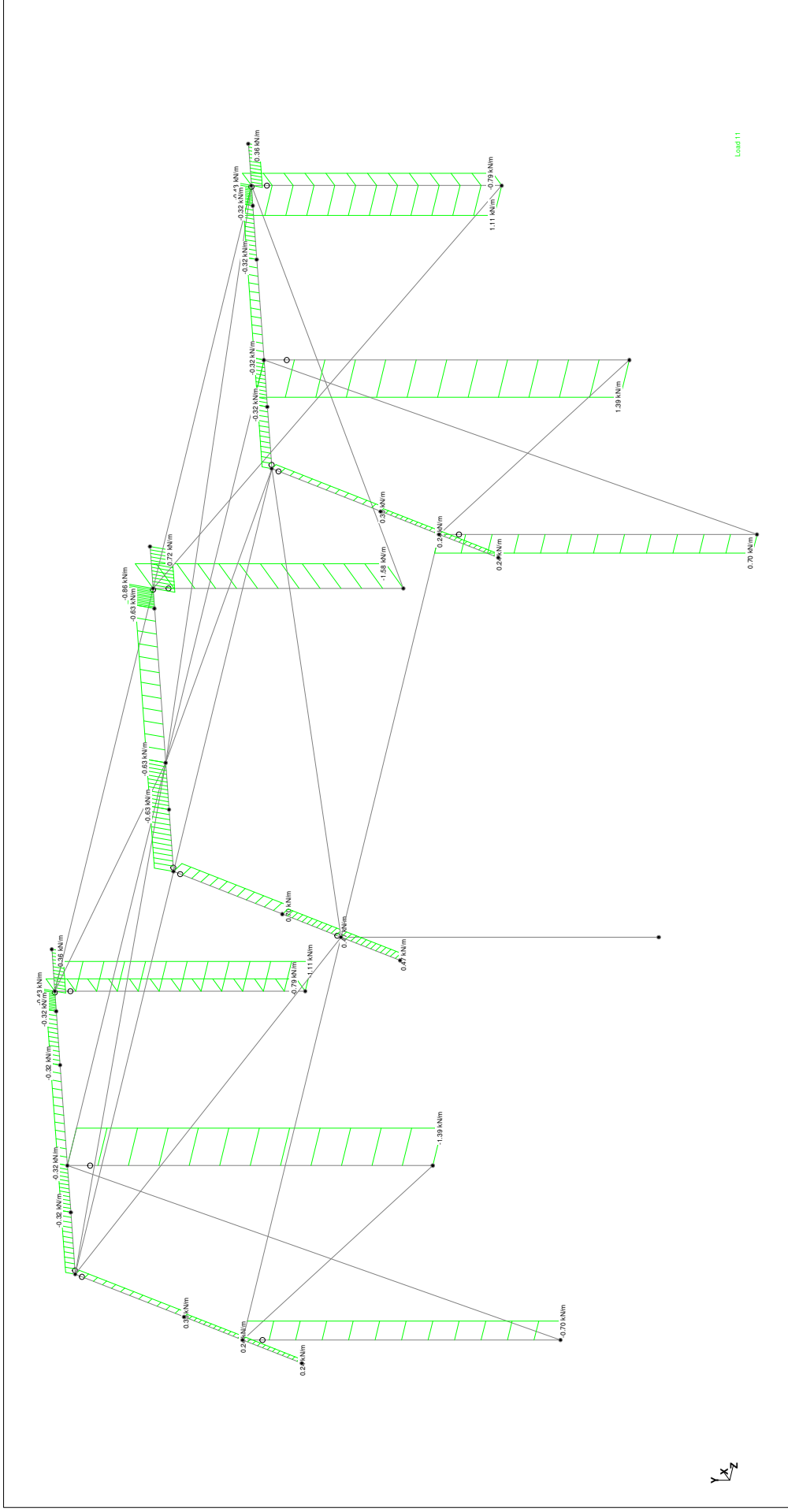
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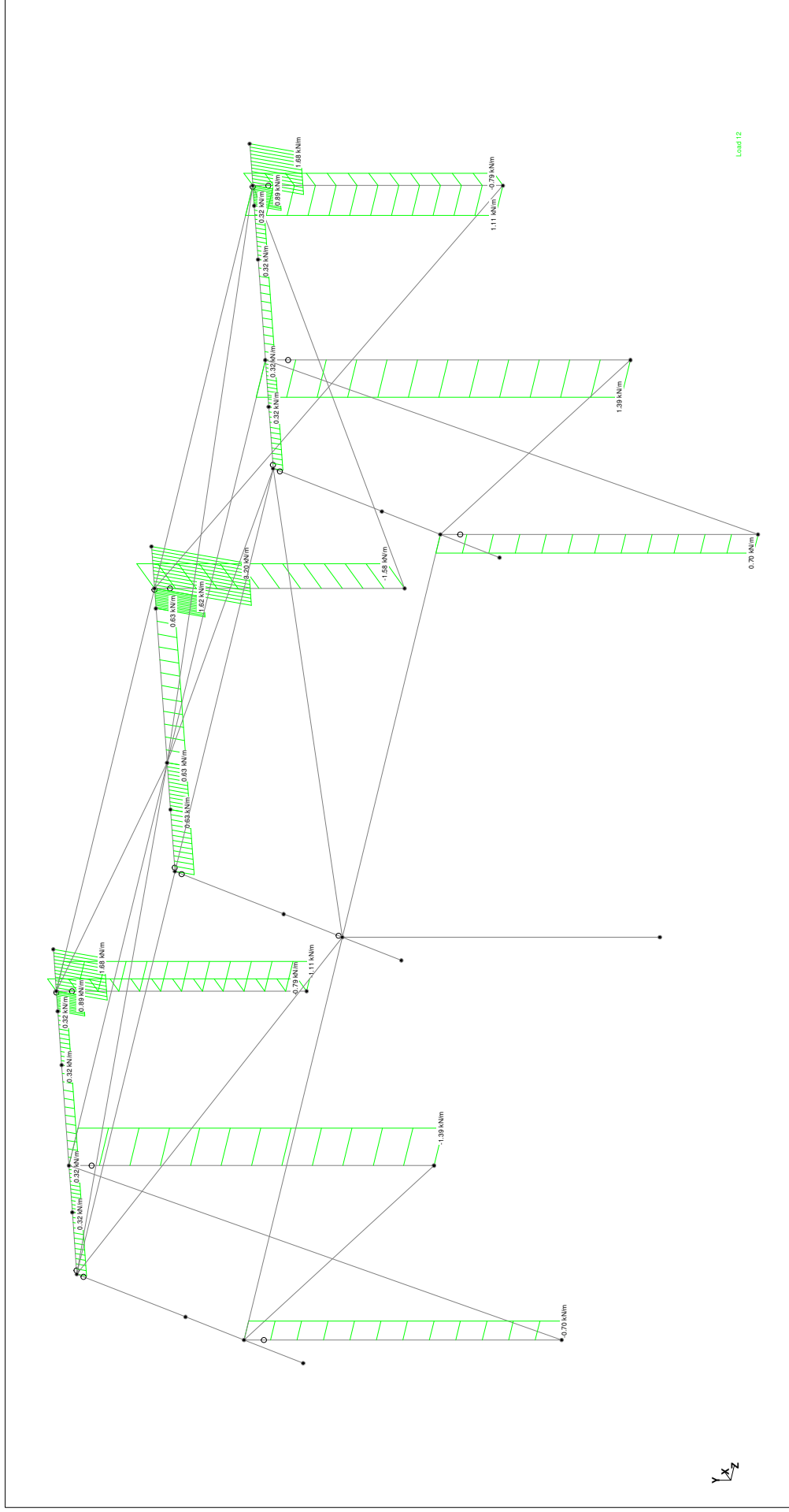
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BG11: wind -X2





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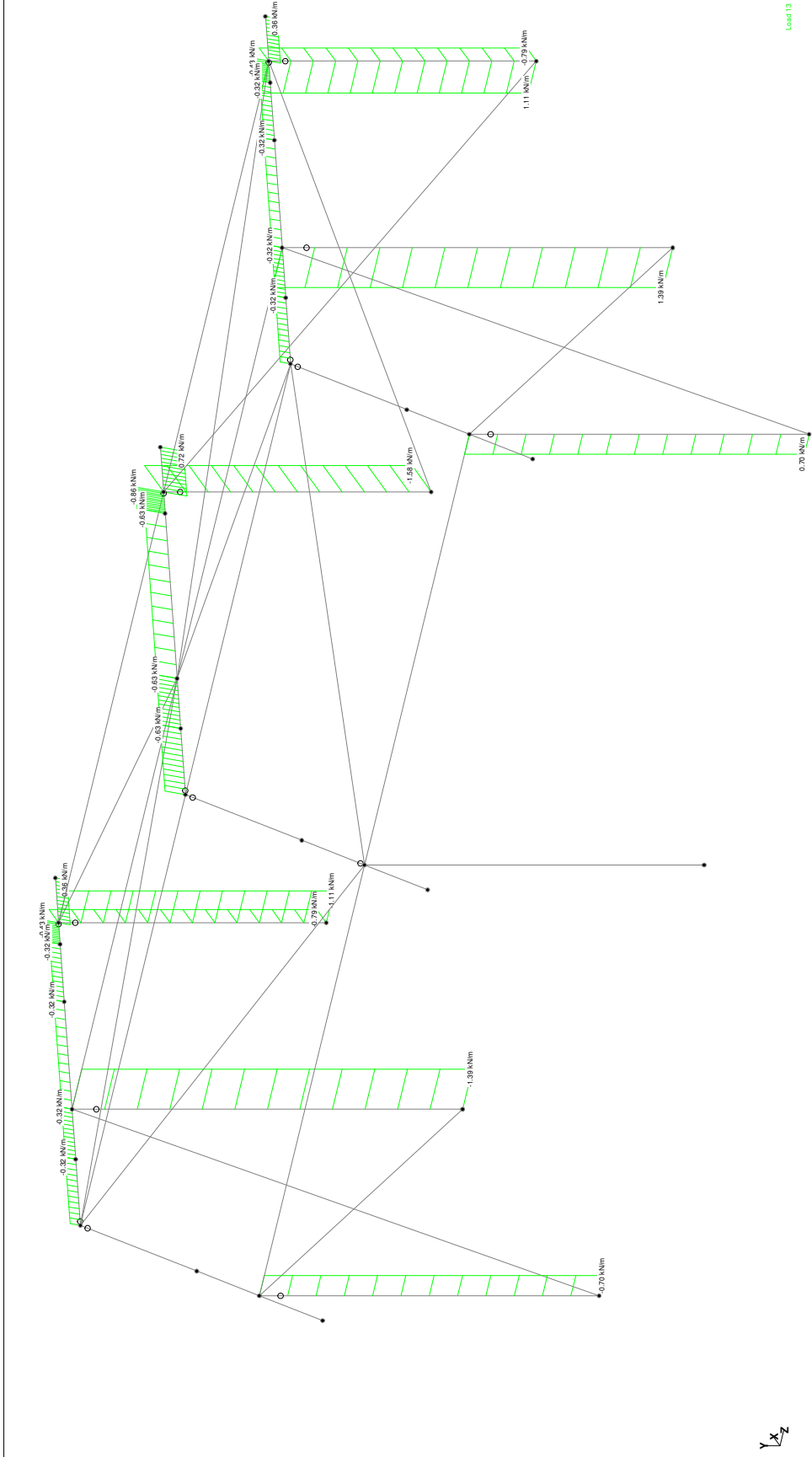
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Load 13

BG13: wind -X4



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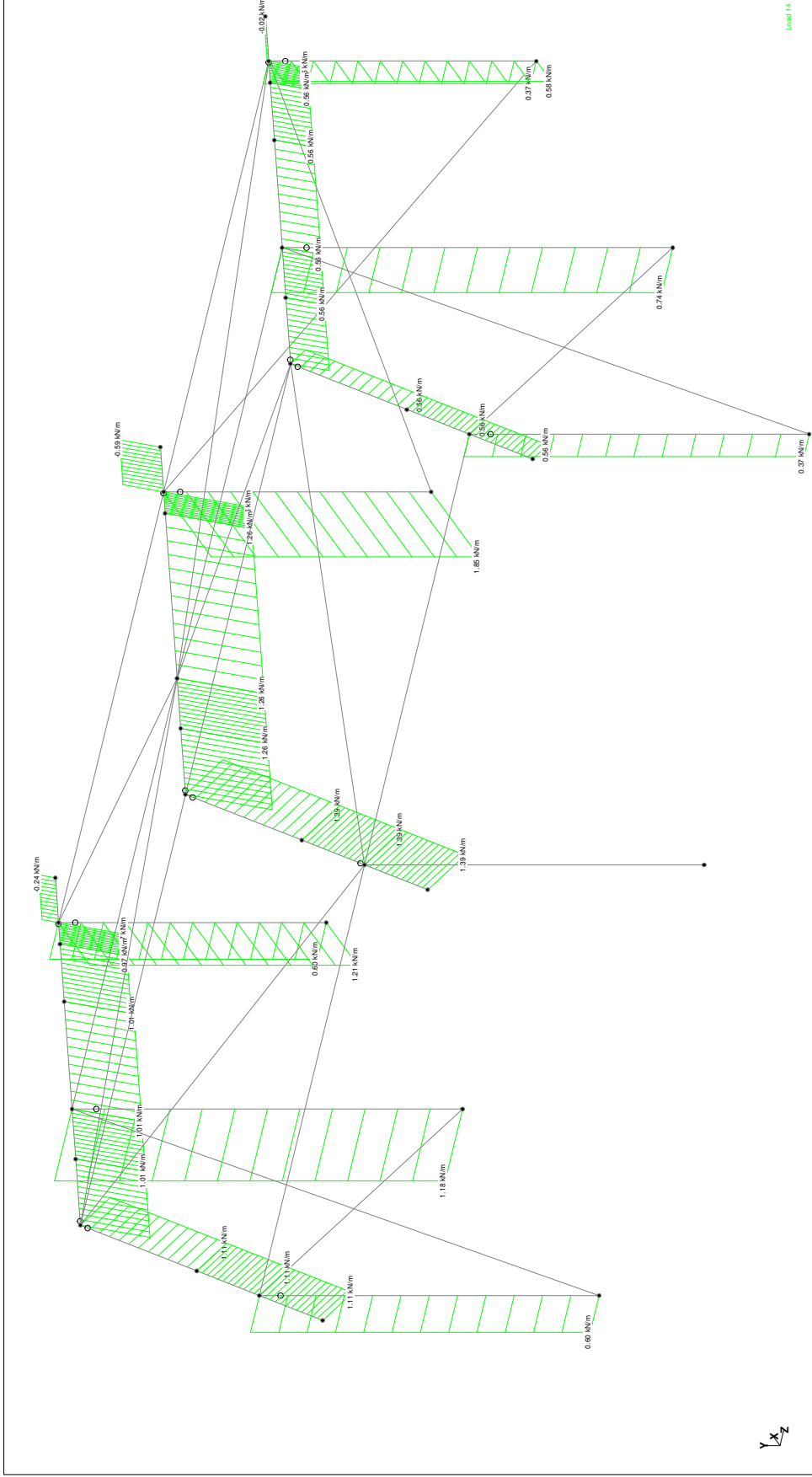
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16

16



Load 14

$$Y \times Z$$

BG14: wind Z



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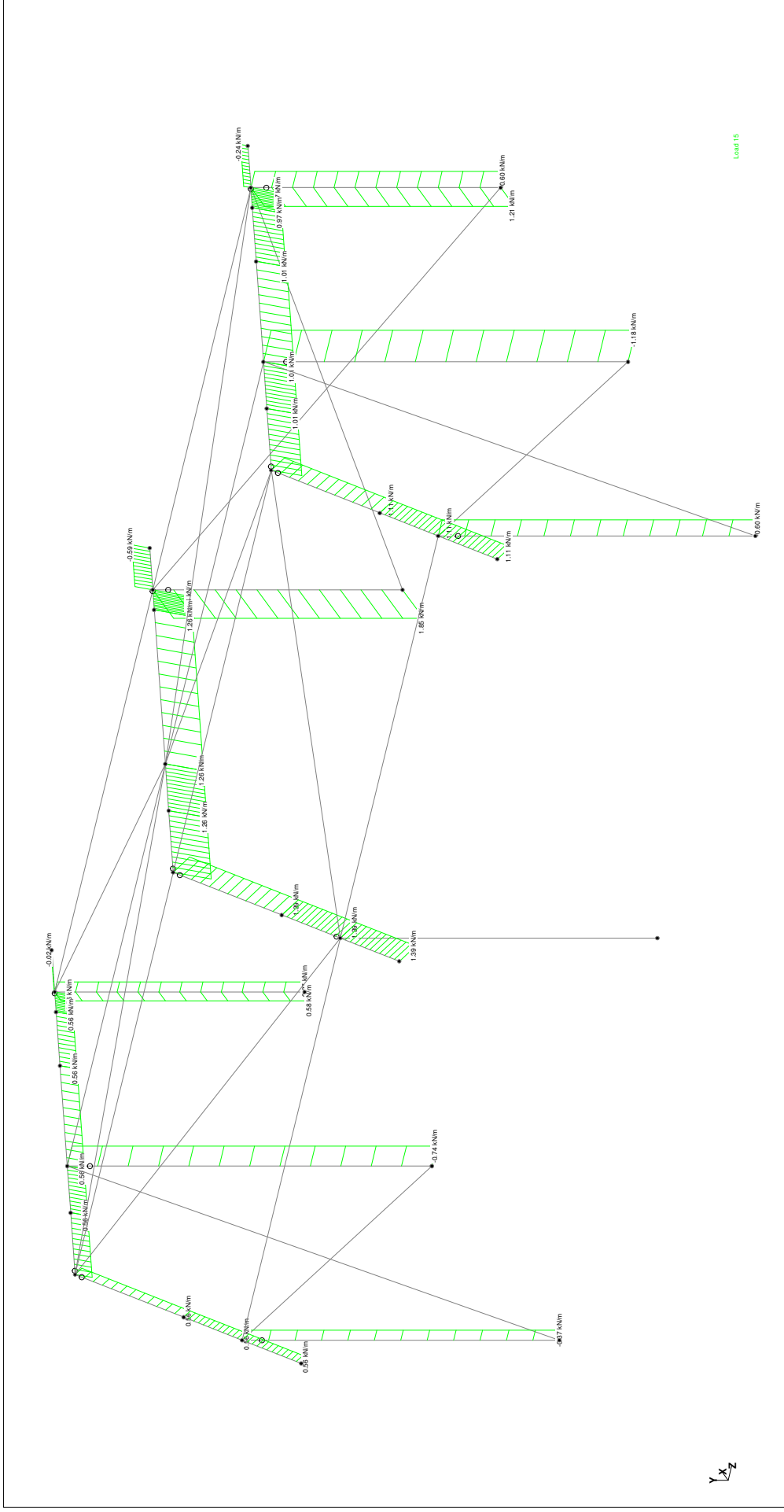
Date	07-Jul-15	Chd	PC
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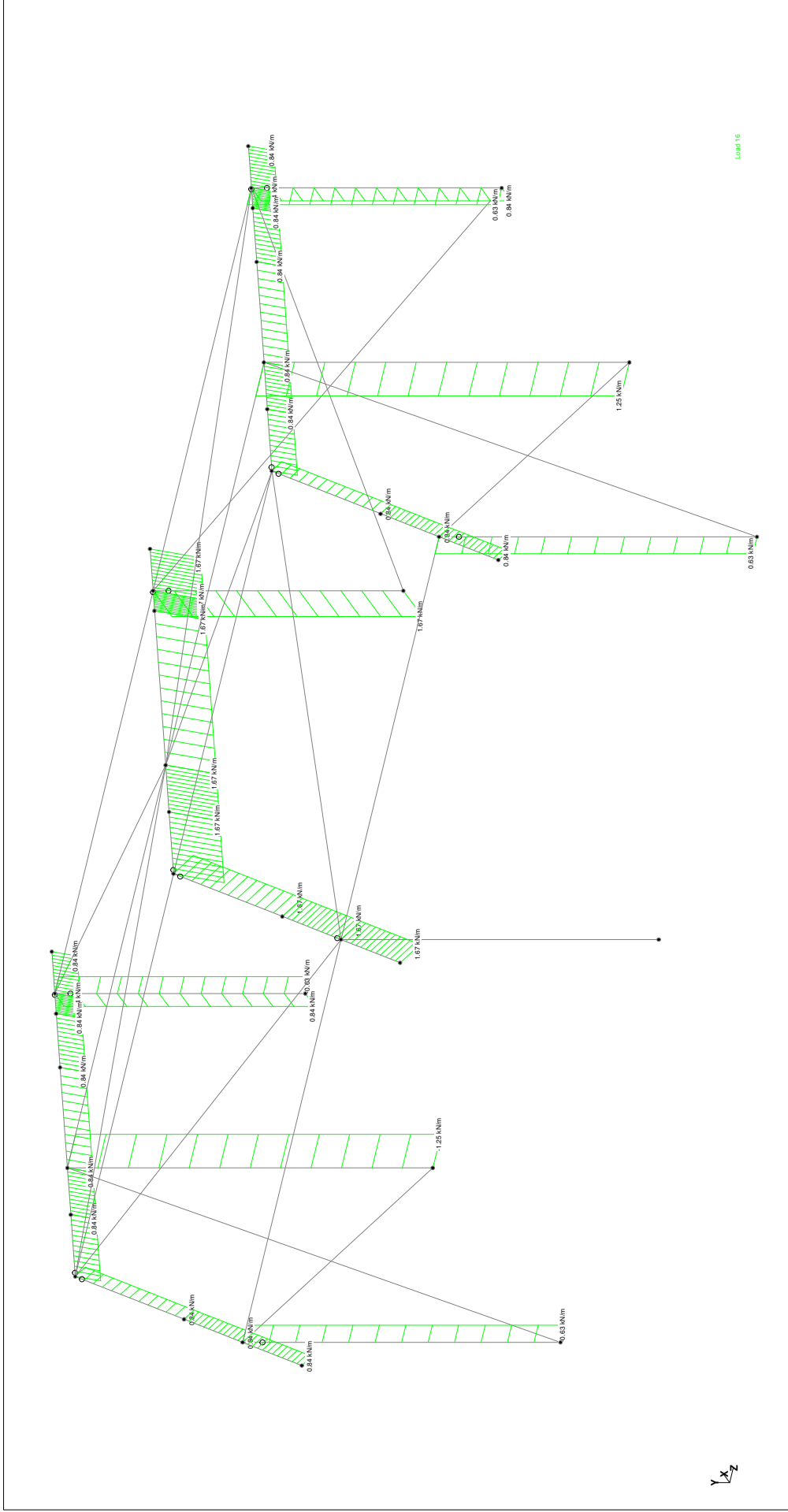
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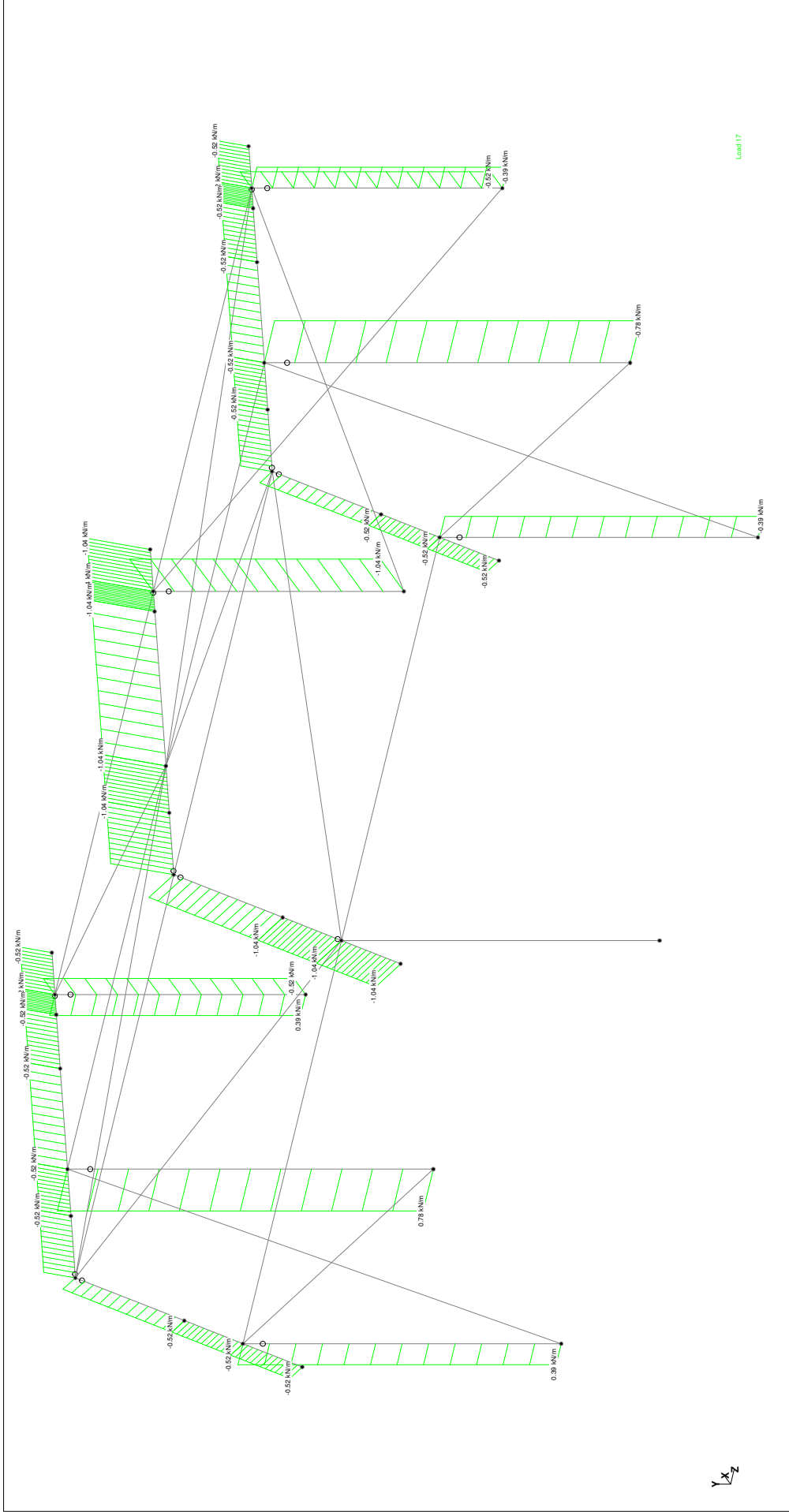
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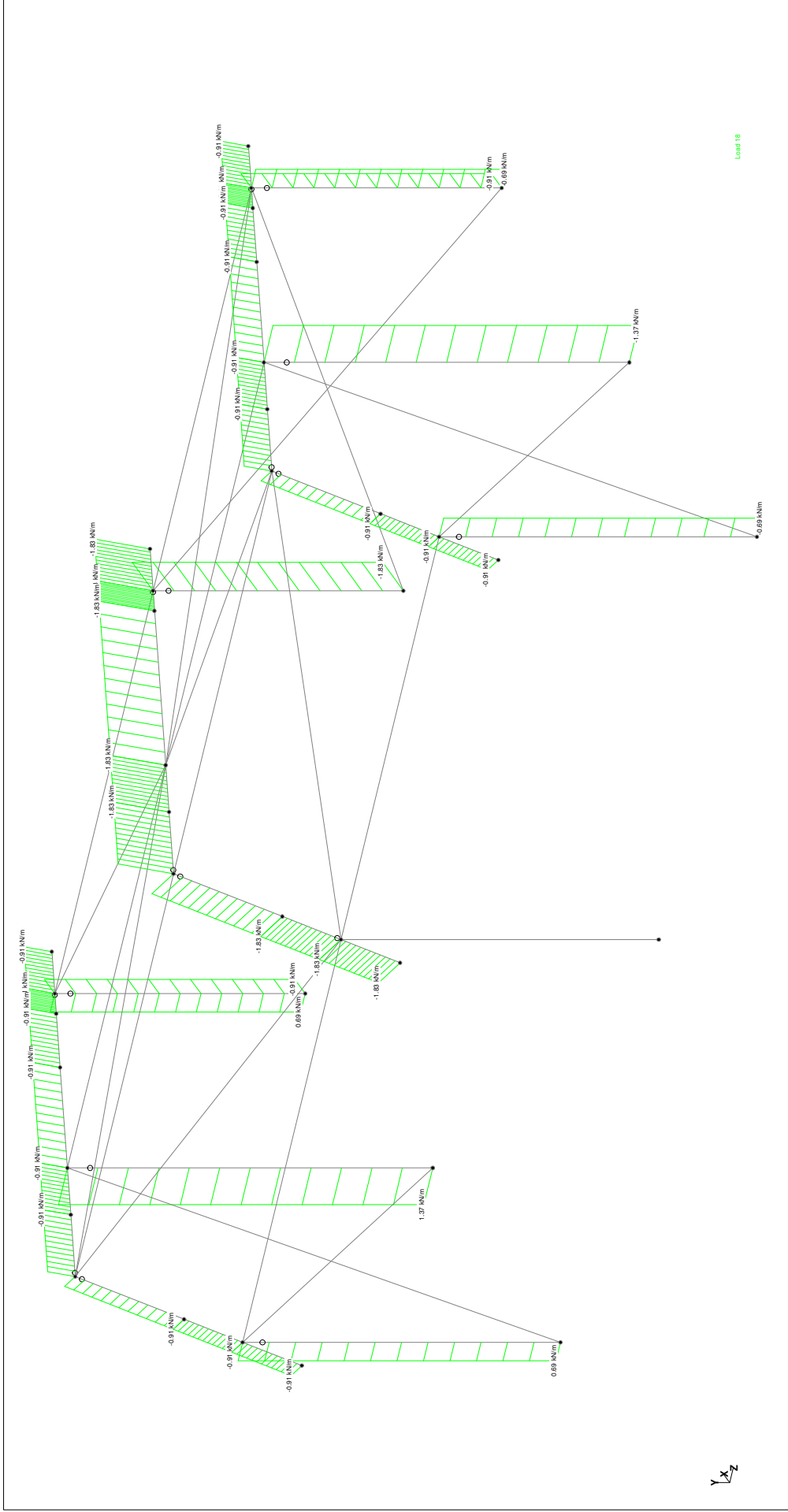
BG15: wind -Z



BG 16: overdruk wind X



BG17: onderdruk wind -X



BG18: onderdruk wind Z en -Z



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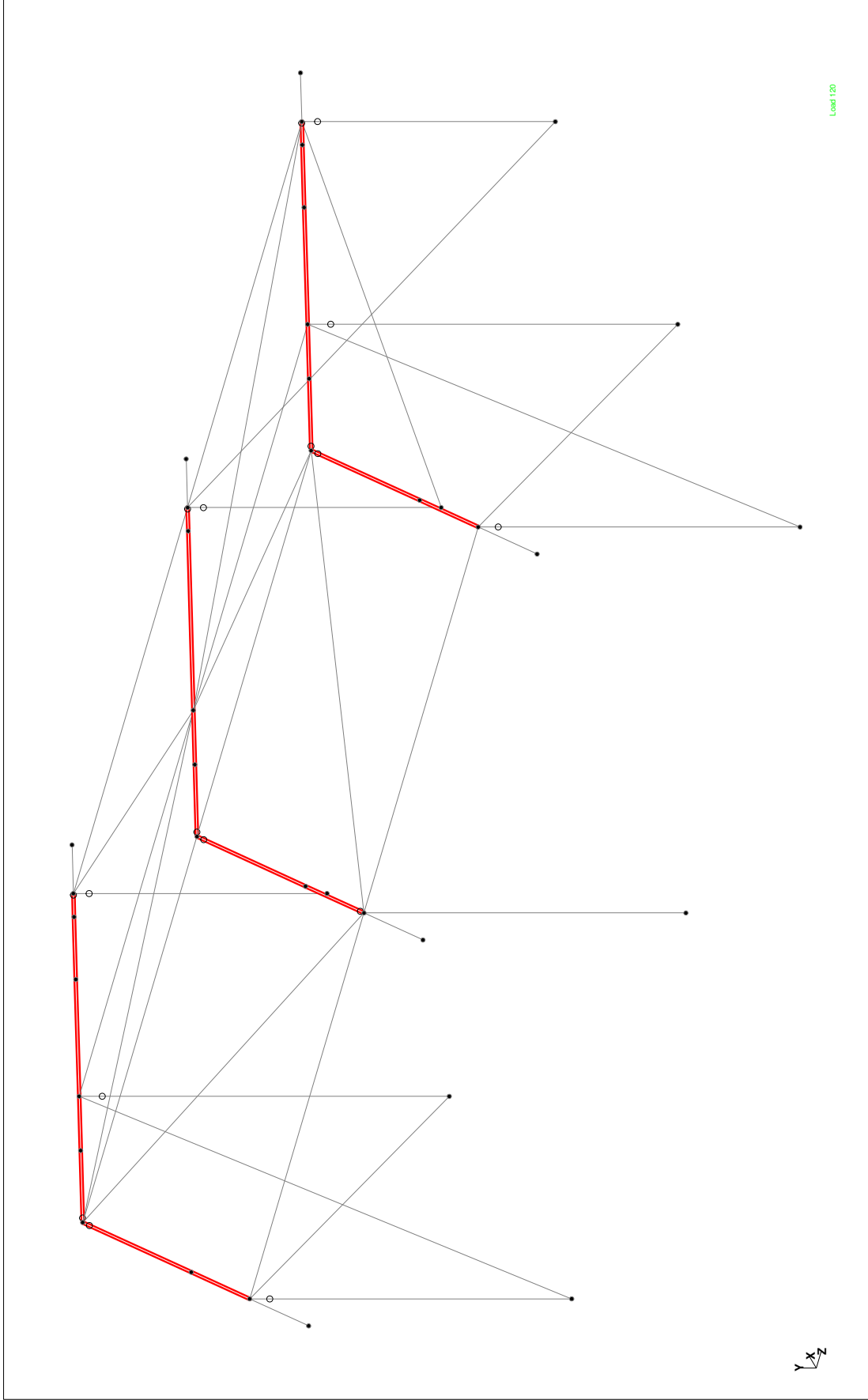
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kniklengte zwakke as L=2.0m



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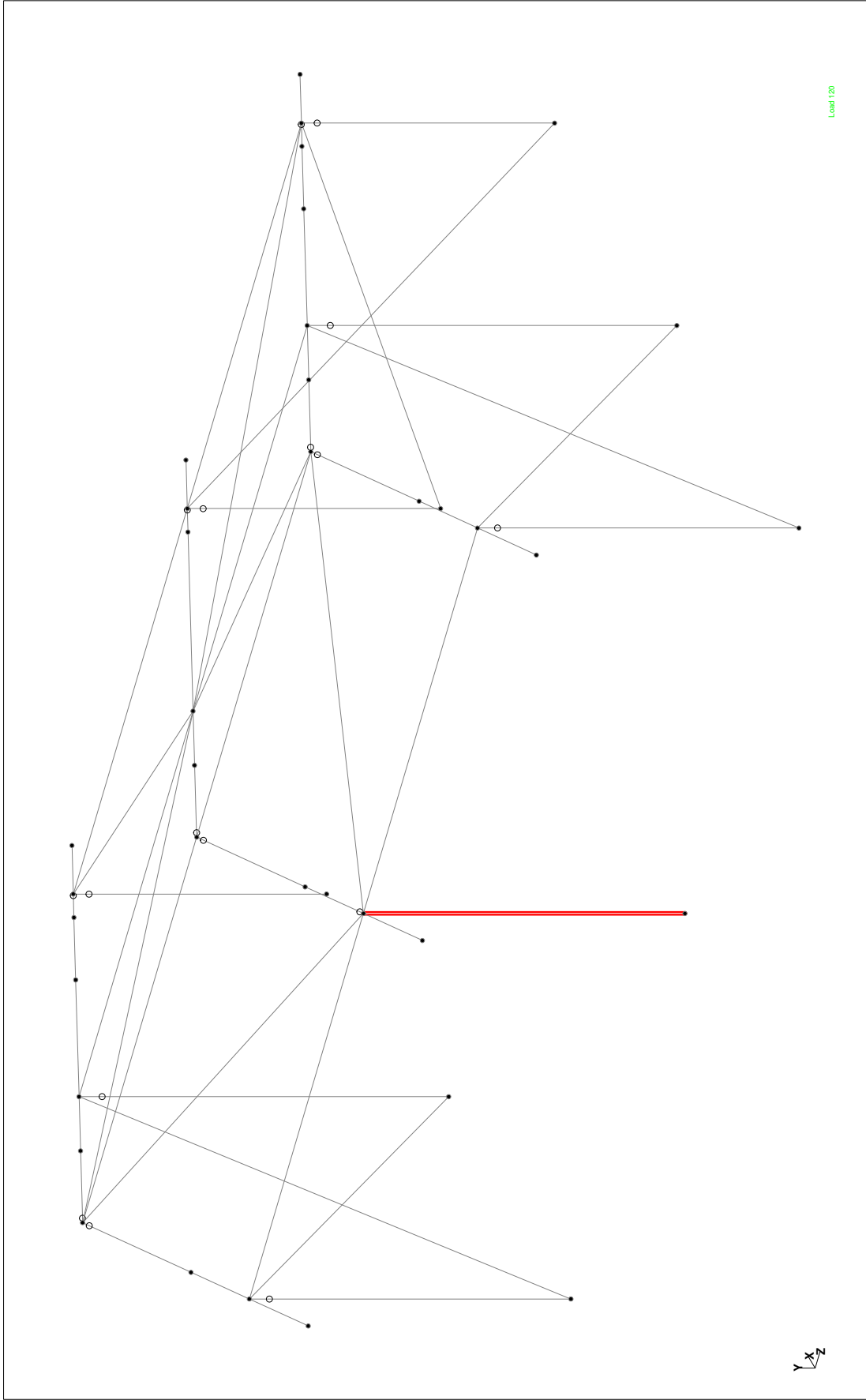
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kniklengte zwakke as L=3.68m



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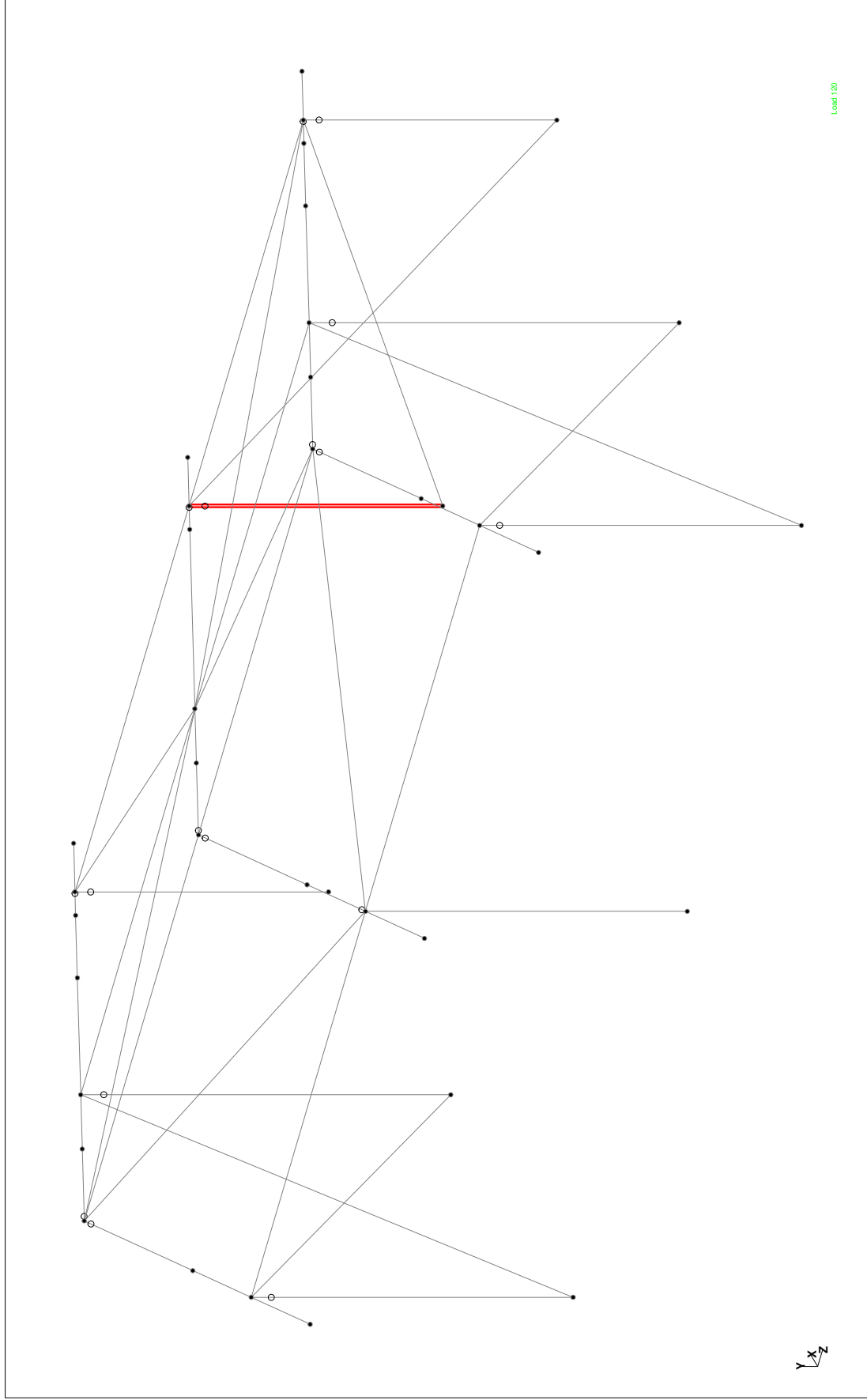
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kniklengte zwakke as $L=2,89m$



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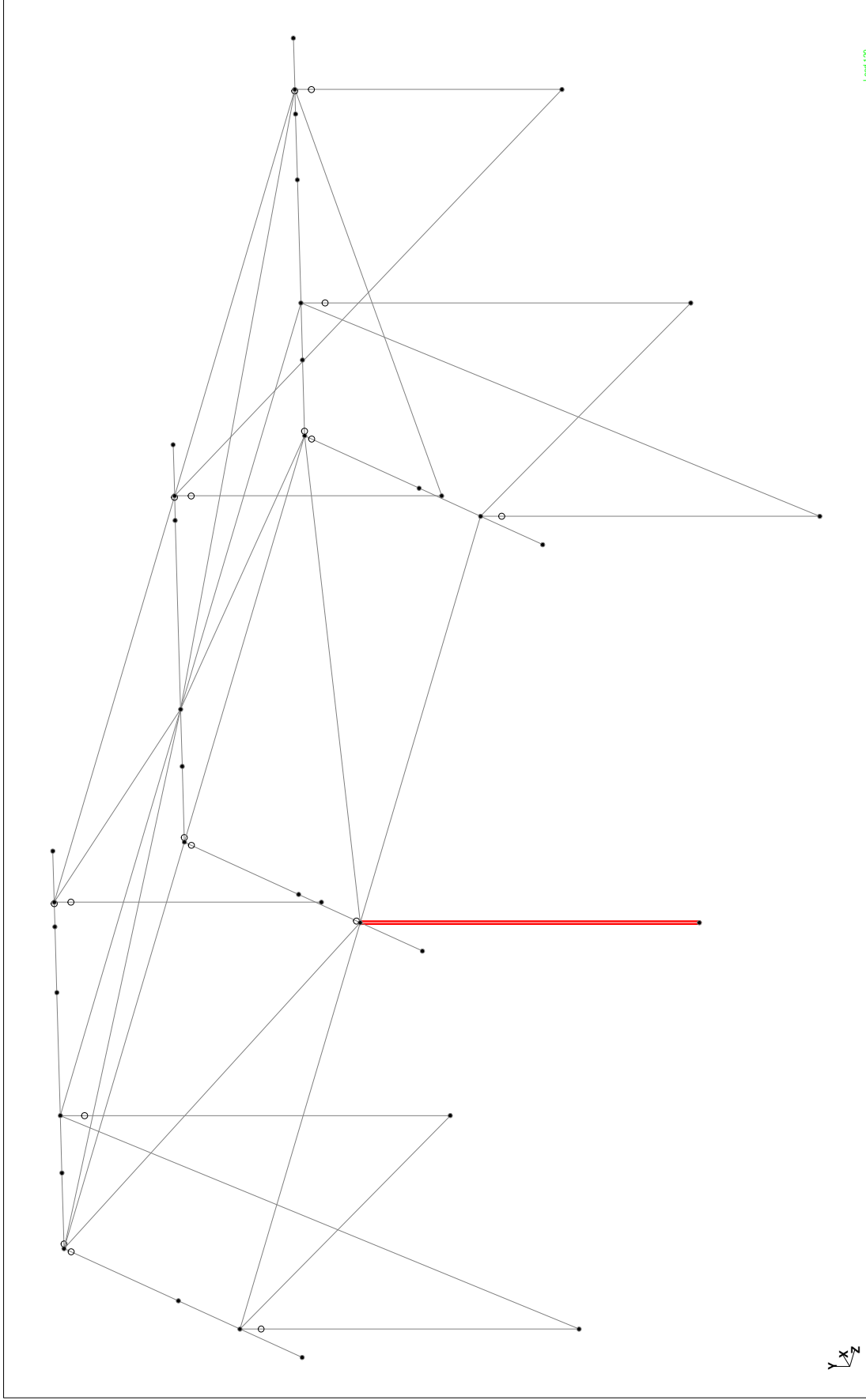
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kniklengte sterke as L=8.59m

Load L20



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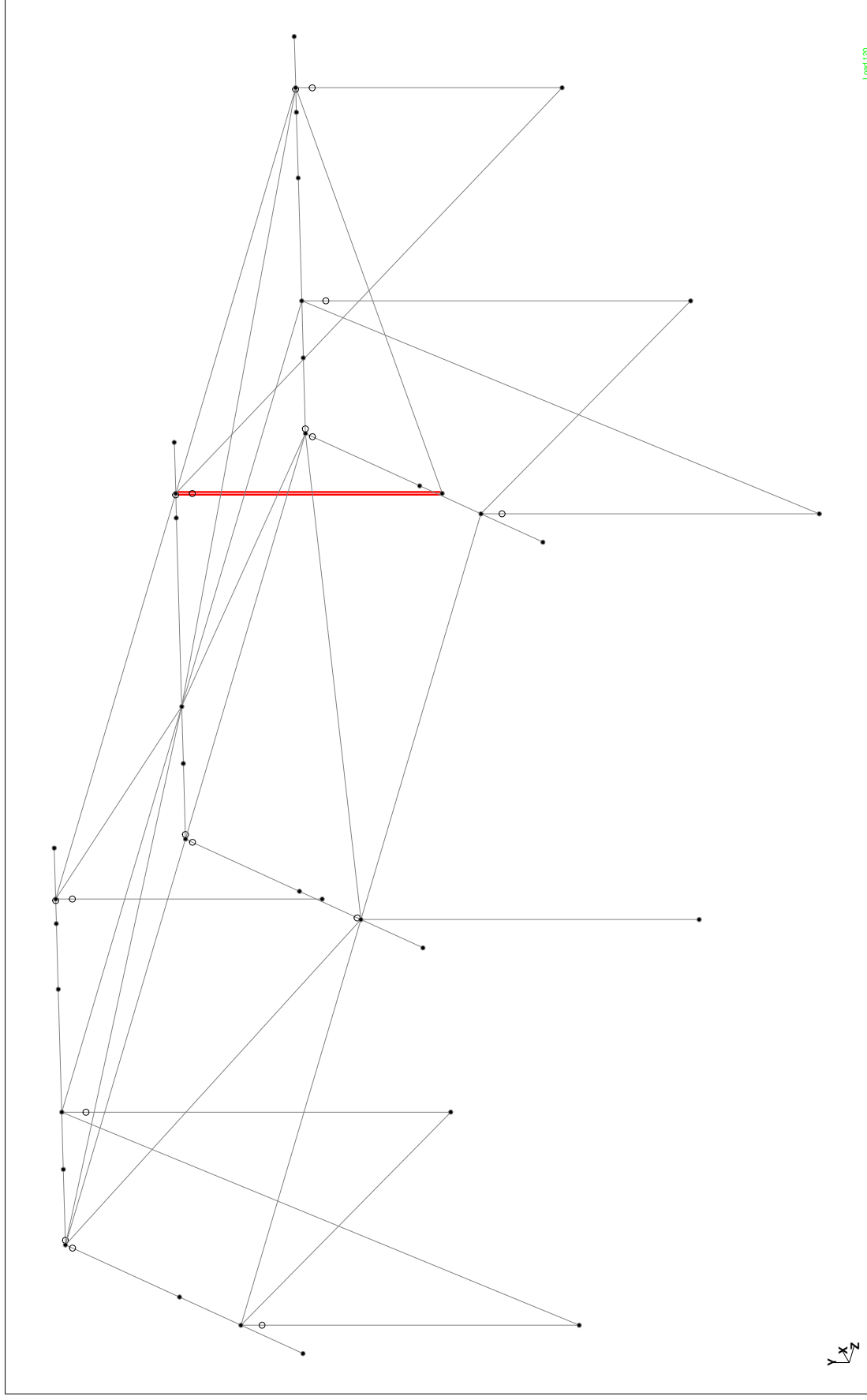
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Load 120

kniklengte sterke as L=7.79m



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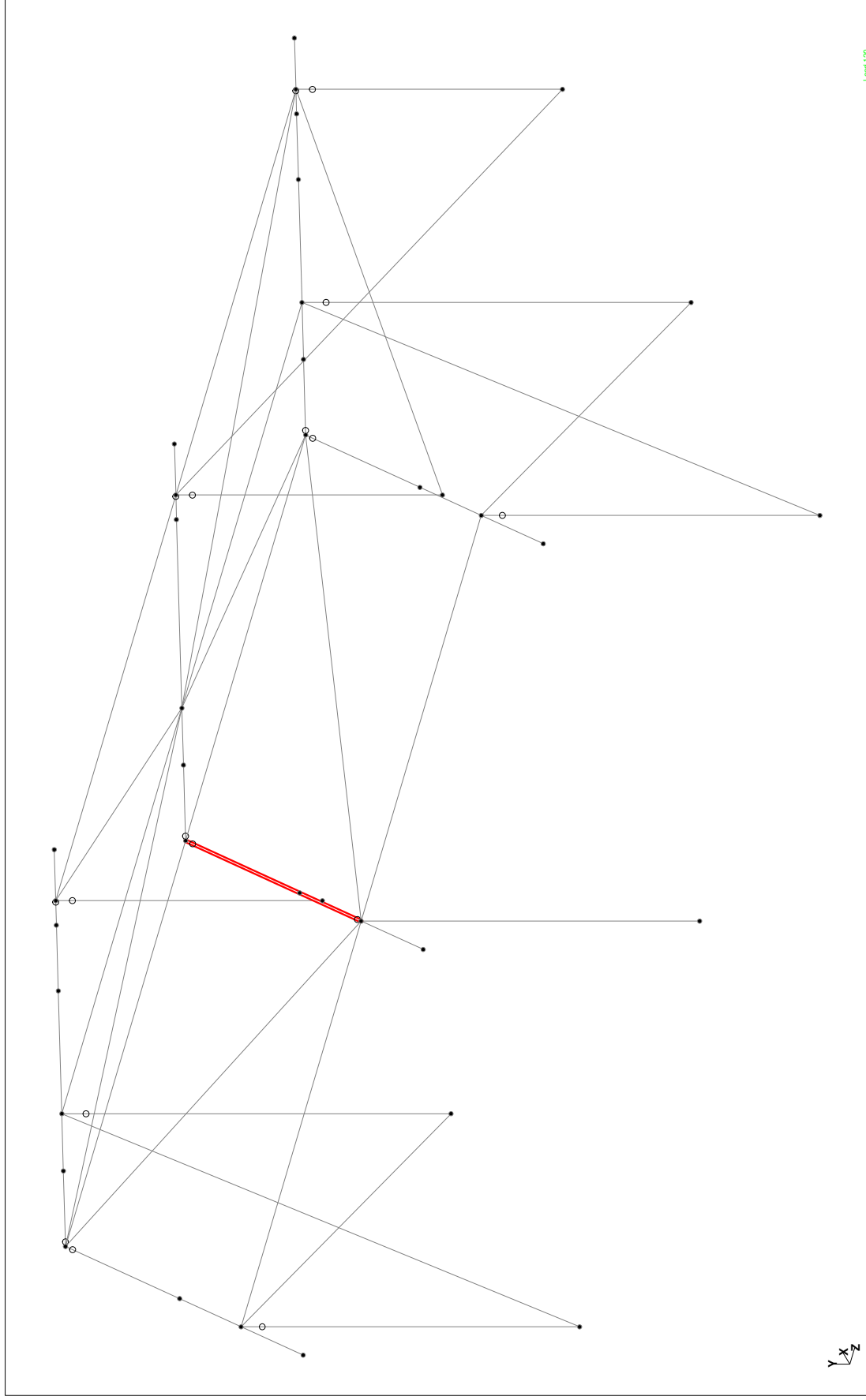
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kniklengte sterkte as L=3.05m

Load 120



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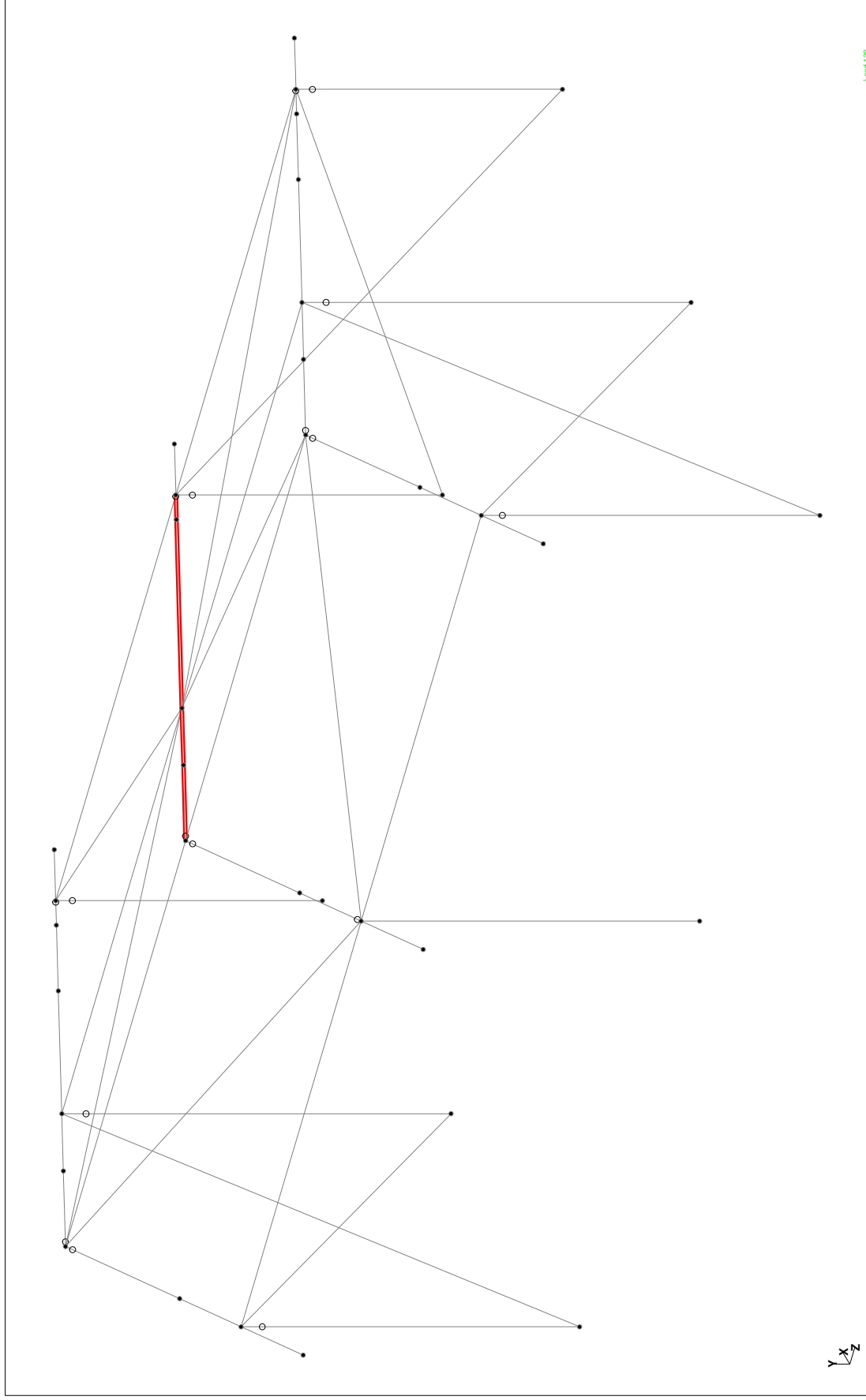
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kniklengte sterkte as L=10.81m

Load L20



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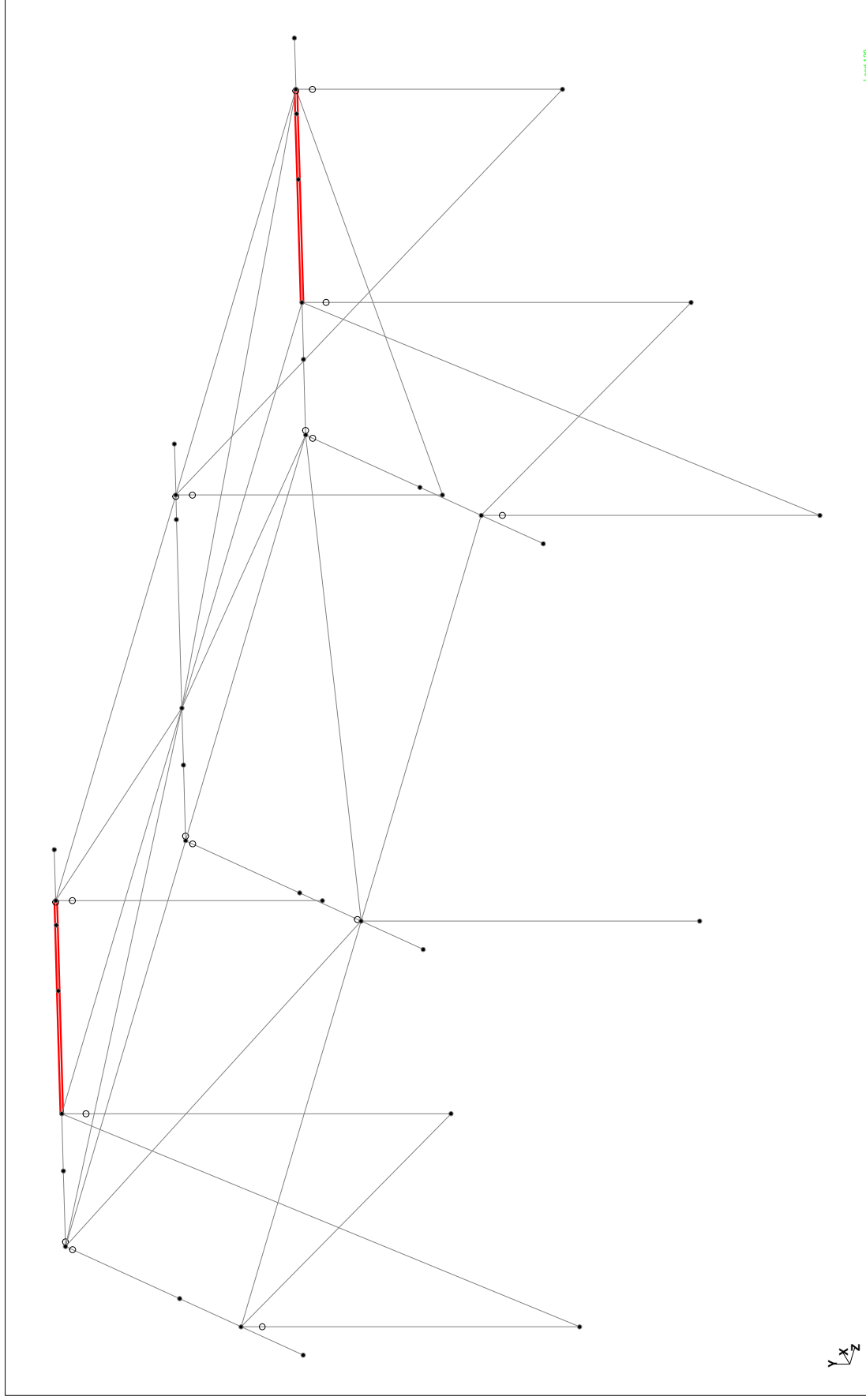
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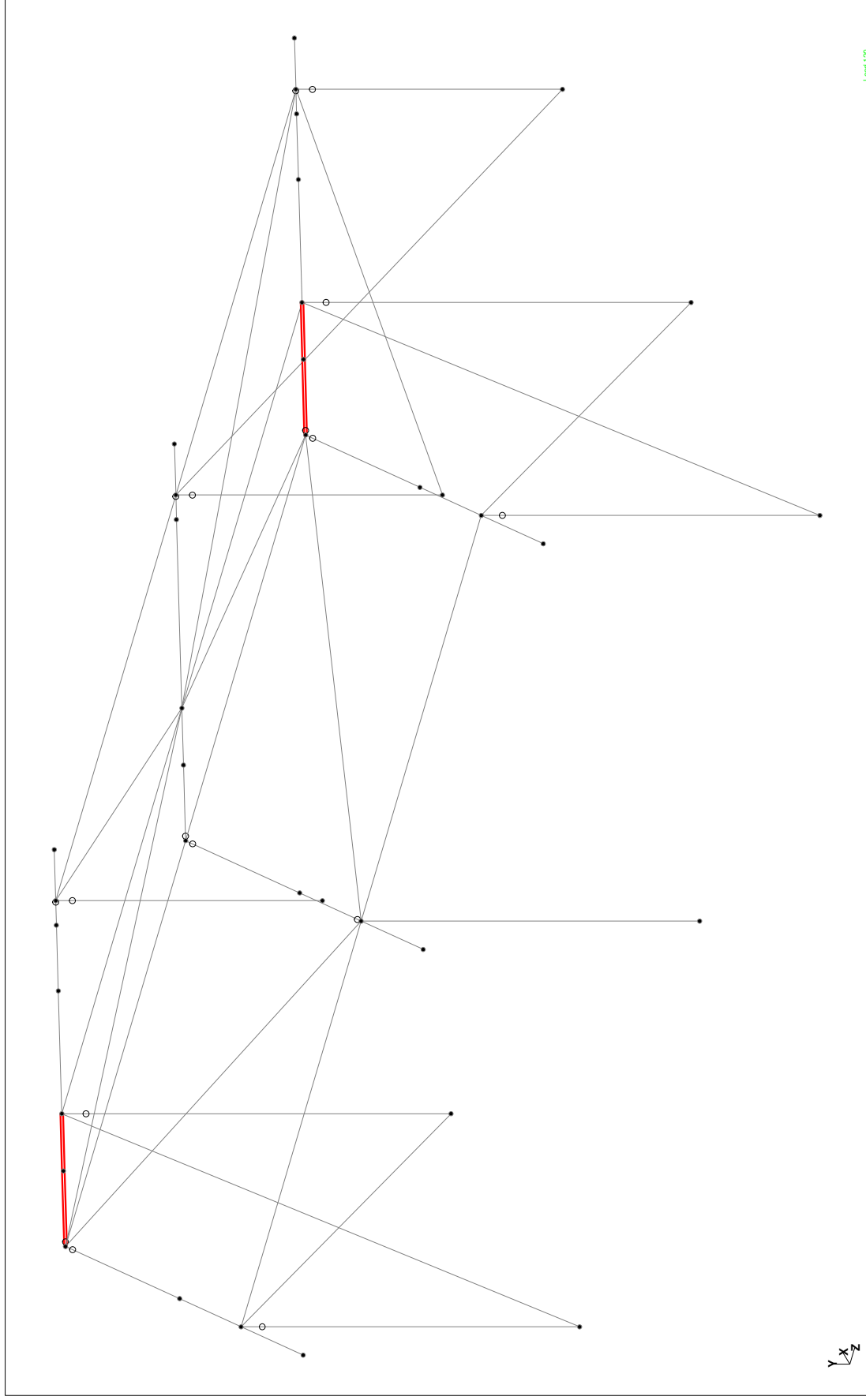
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Load 120

kniklengte sterkte as L=3.99m





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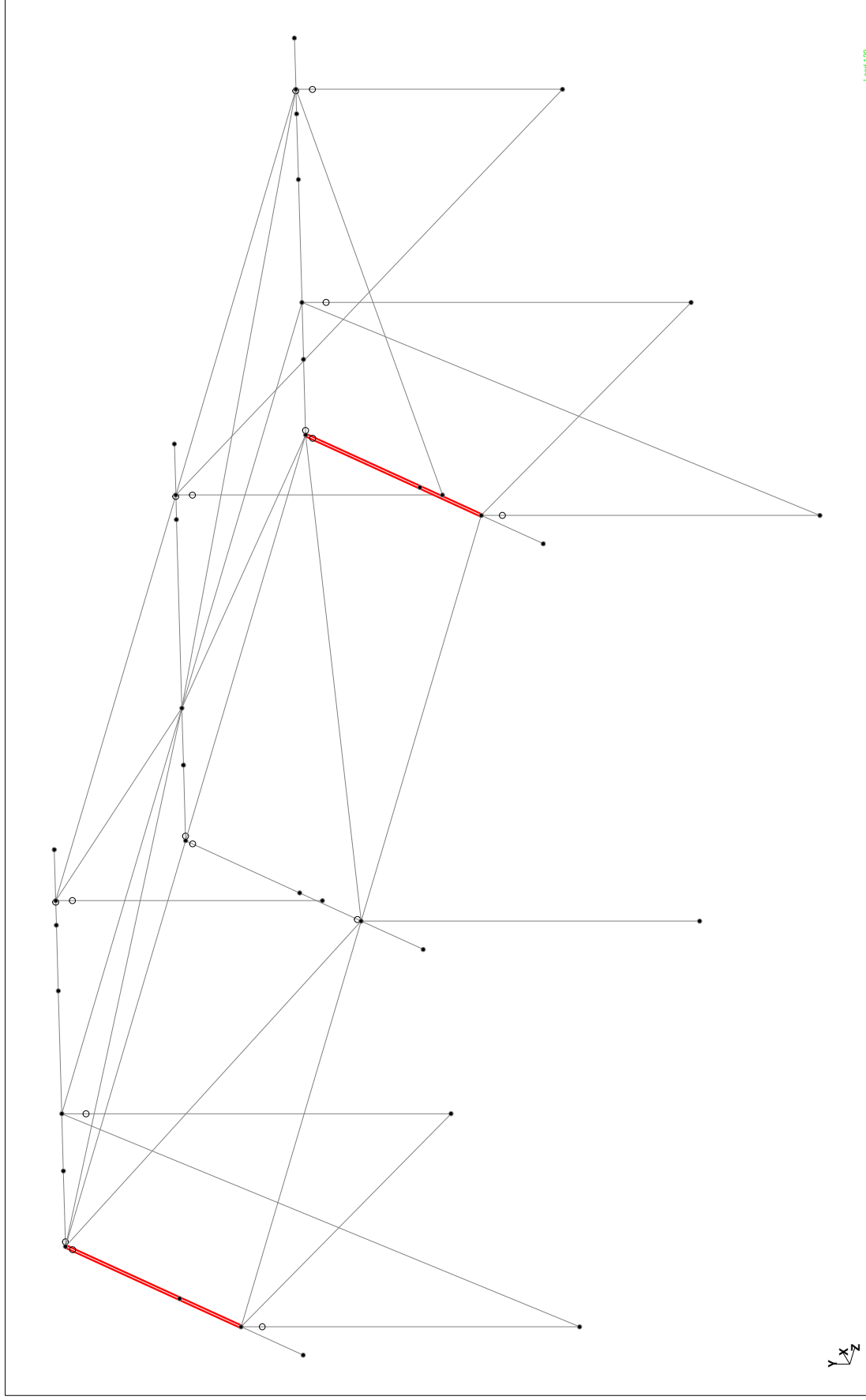
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kniklengte sterke as L=2.0m

Load 1.20



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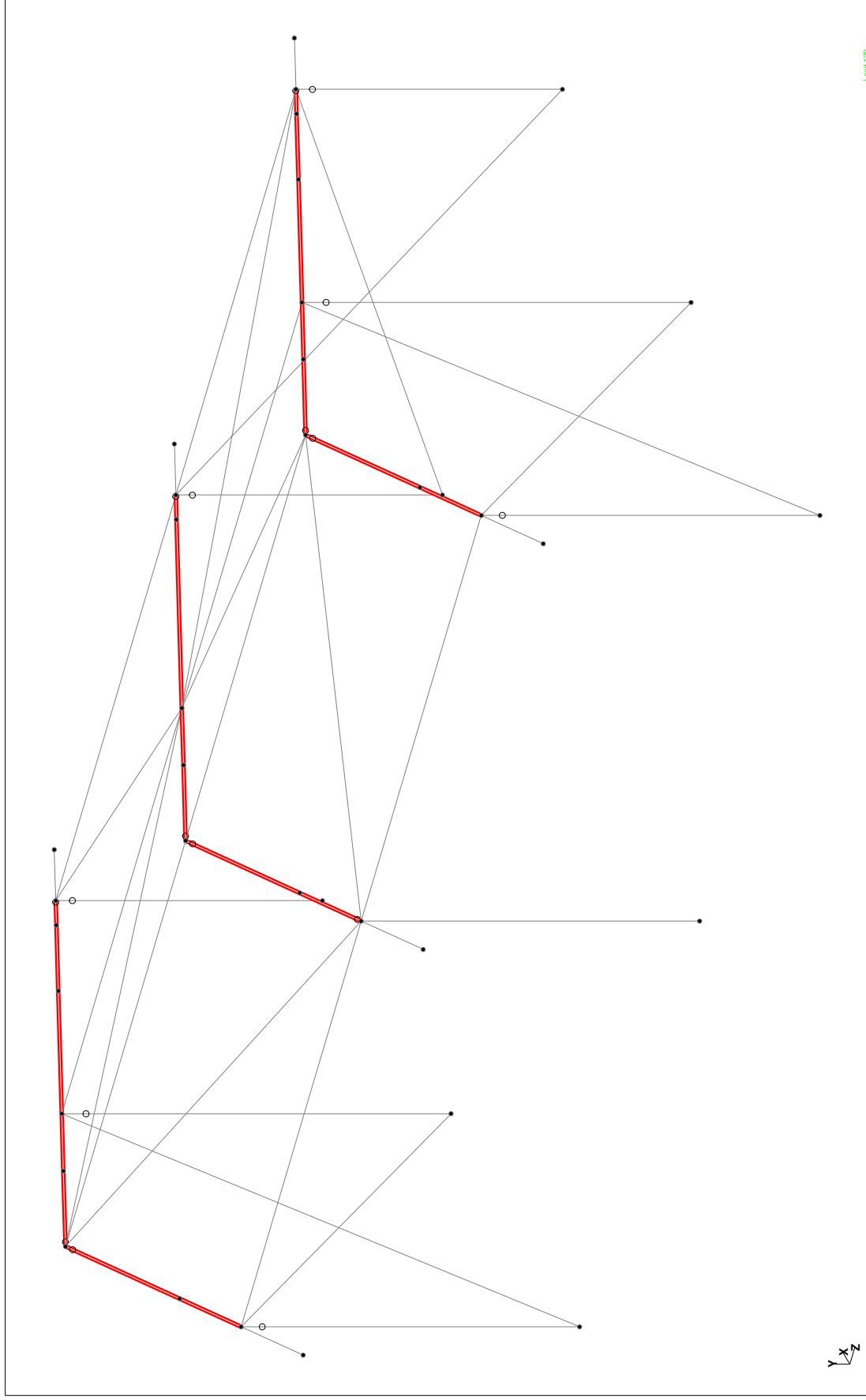
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File 9111-011.std

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Kiplengte L=2.0m

Load L20



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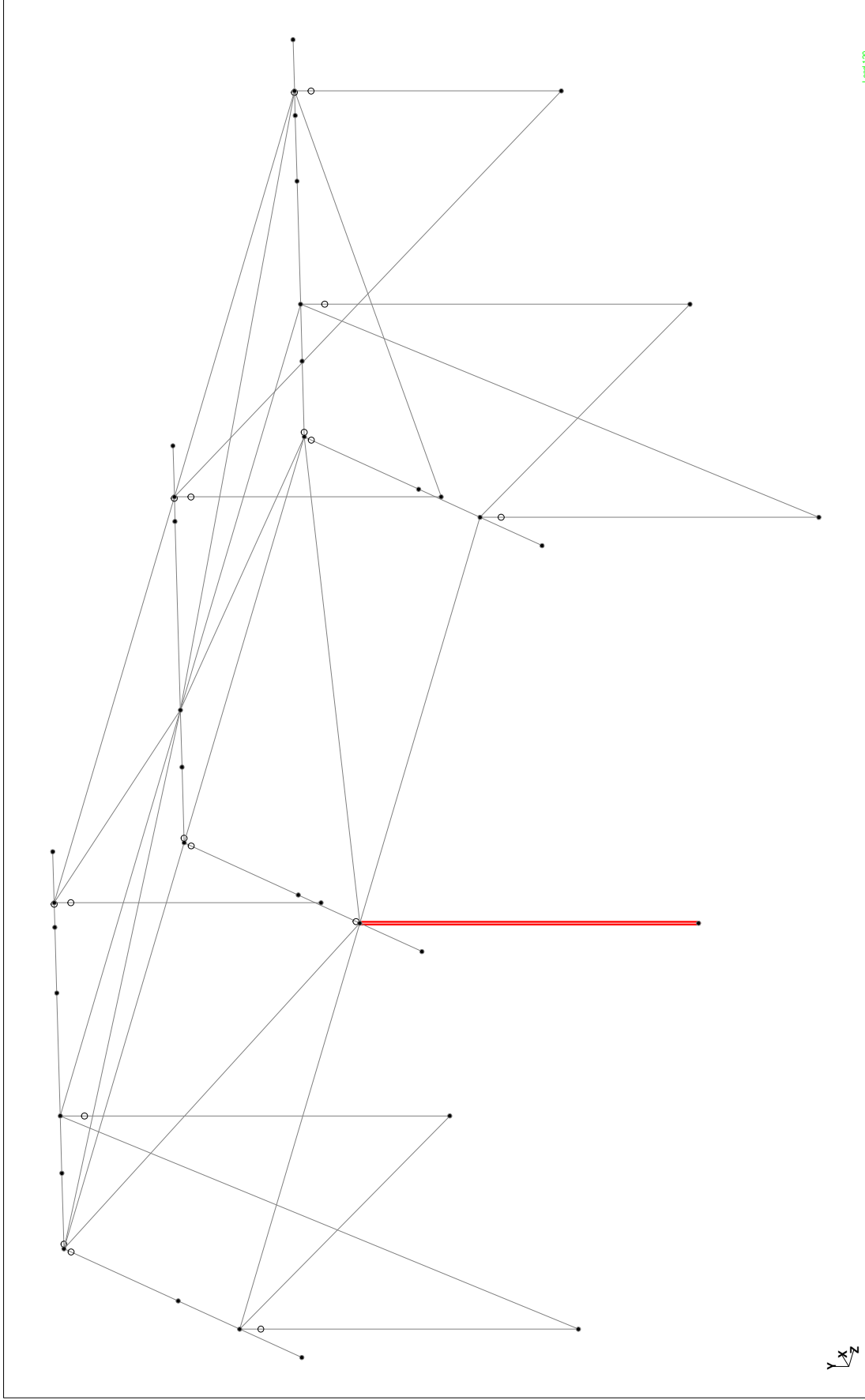
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Kiplengte L=3.66m

Load L20



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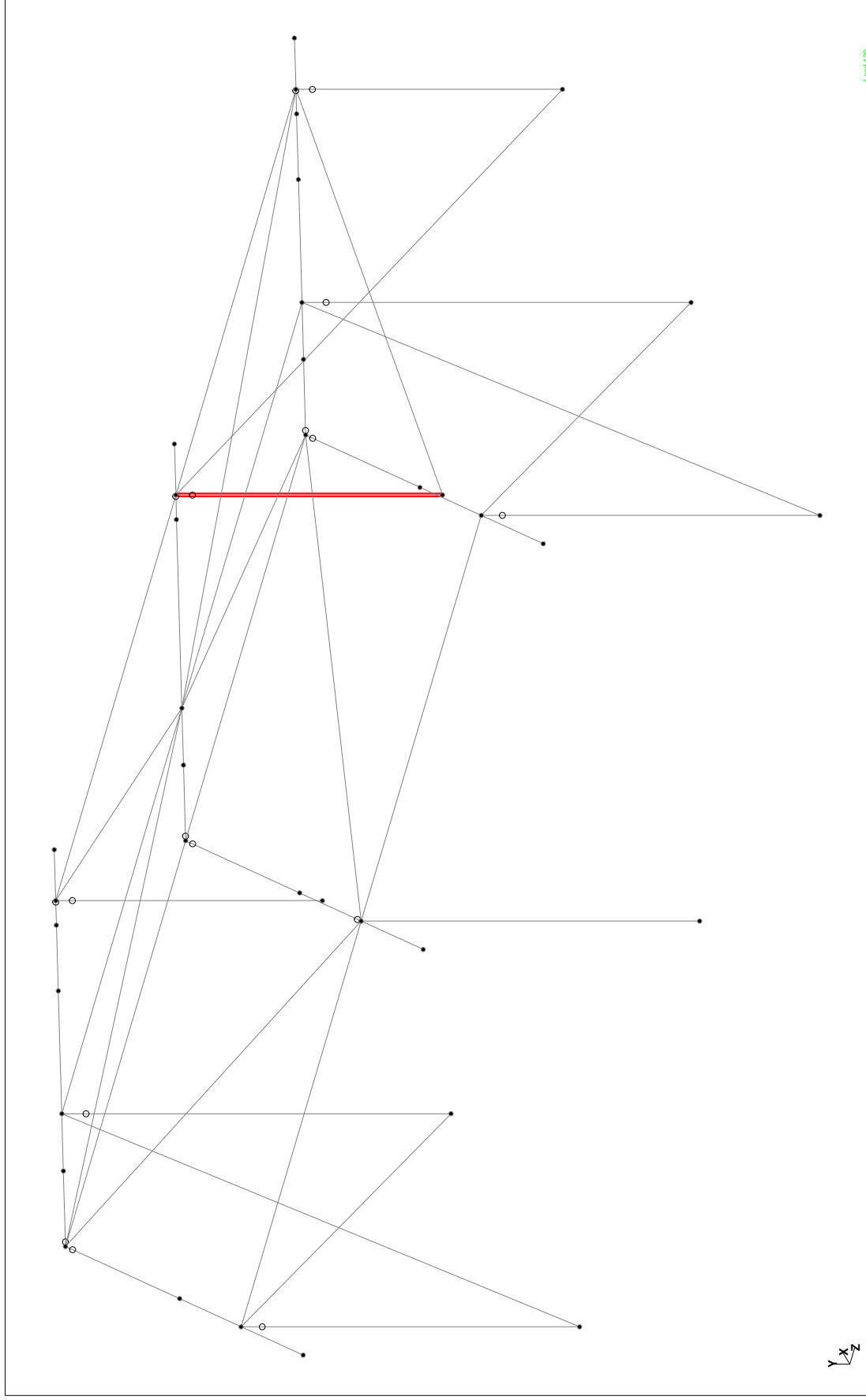
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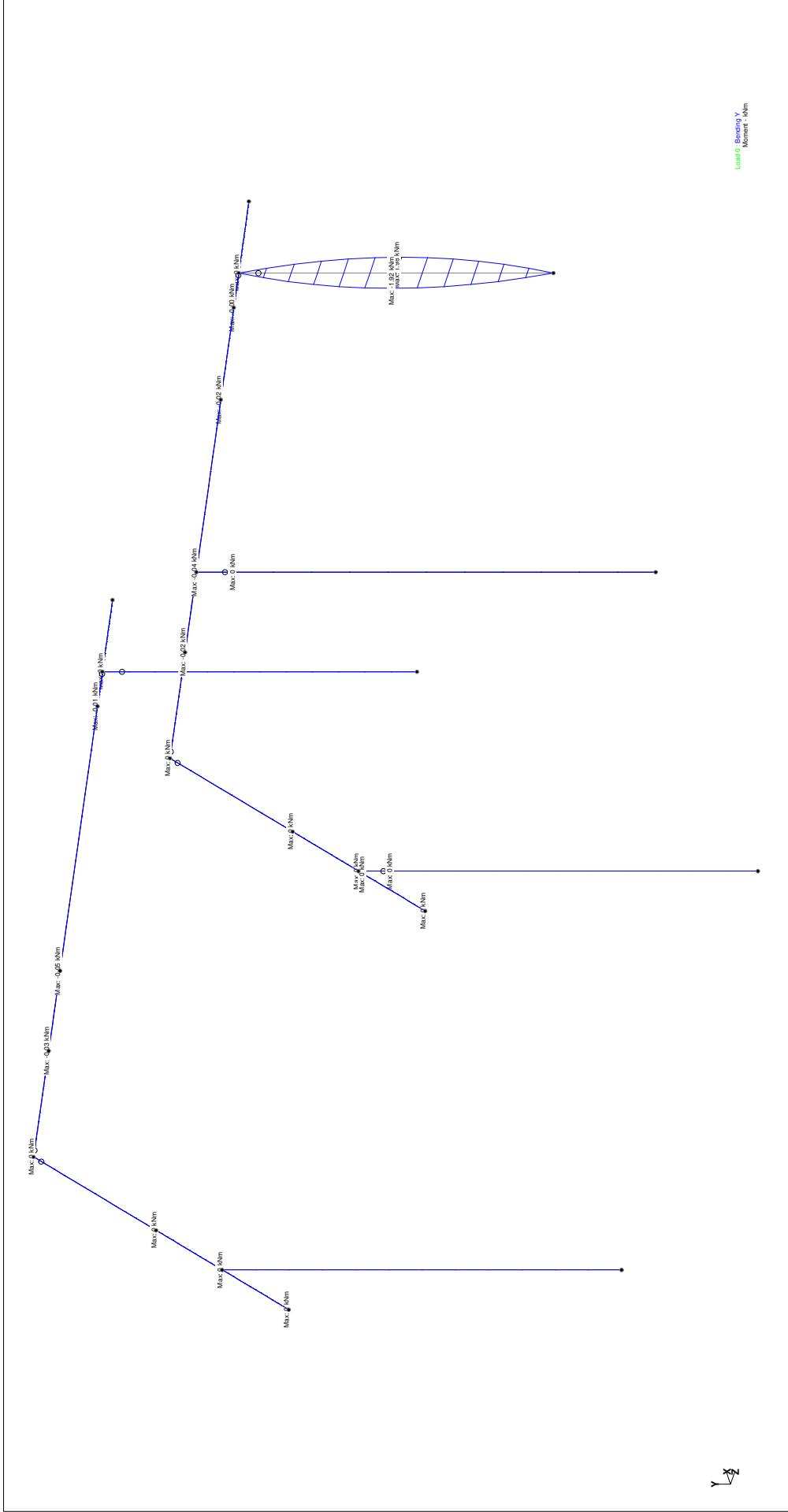
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Kiplengte L=2.89m

Load L20



onthullende momentenlijnen Mx



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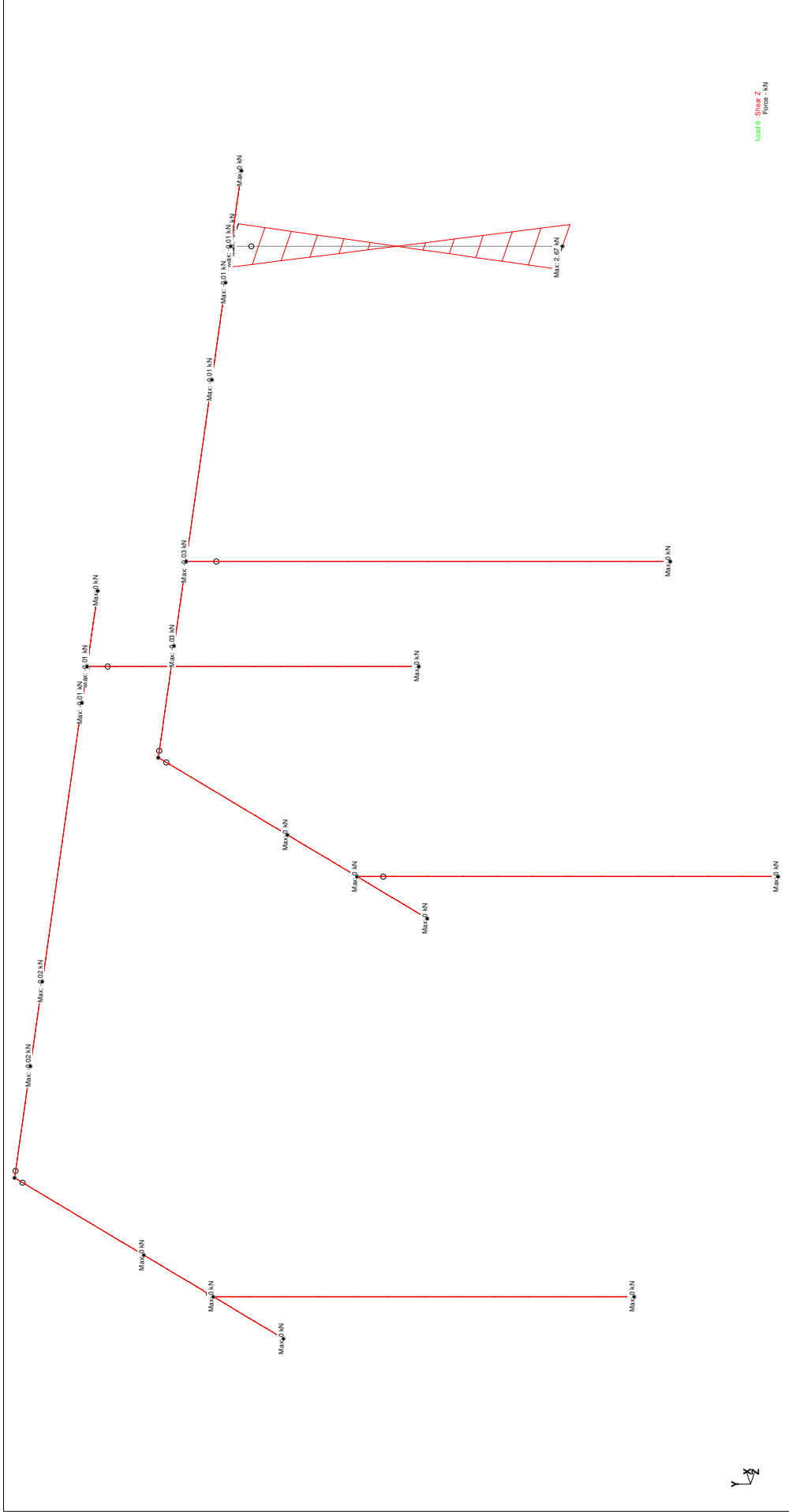
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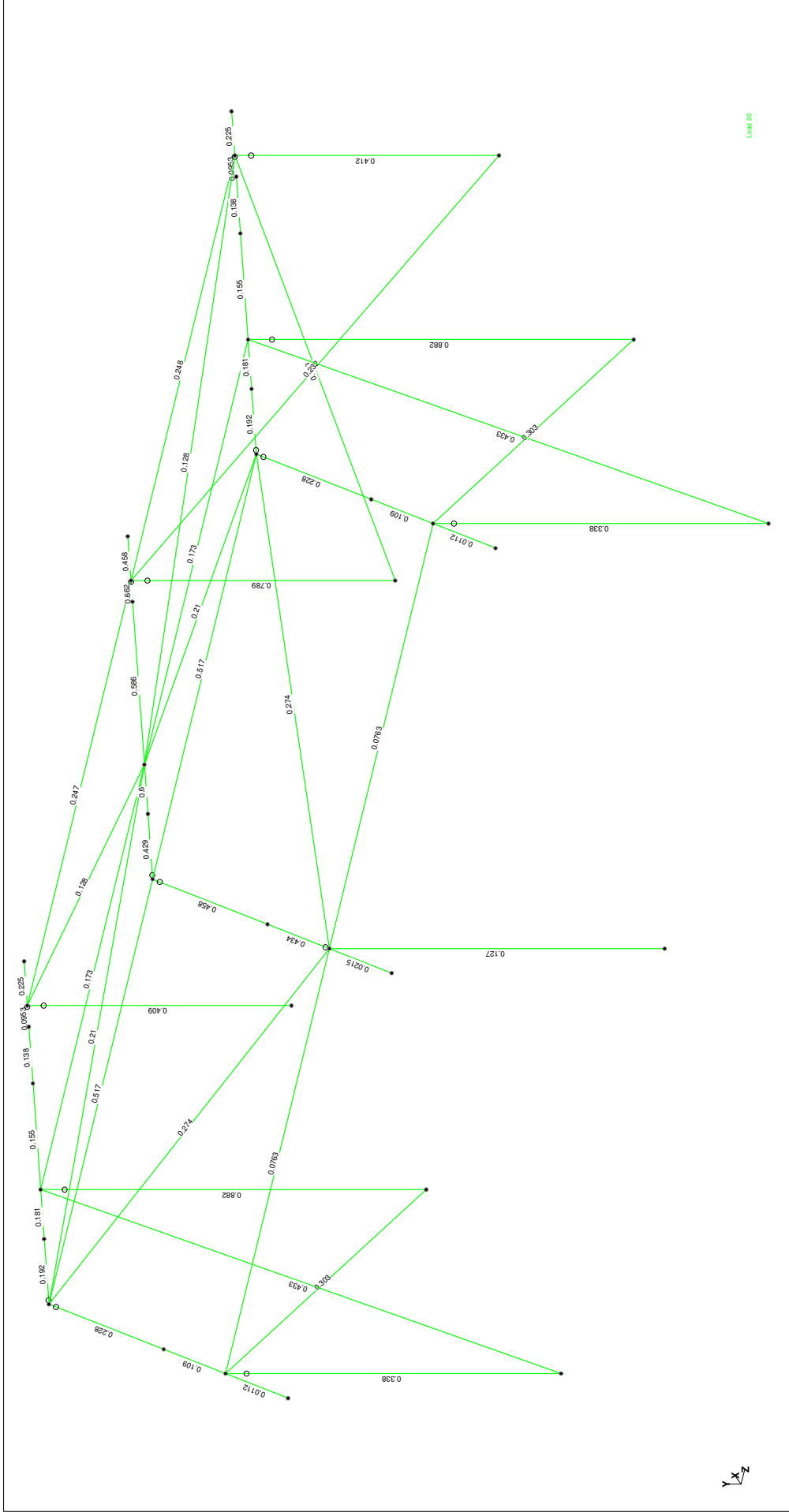
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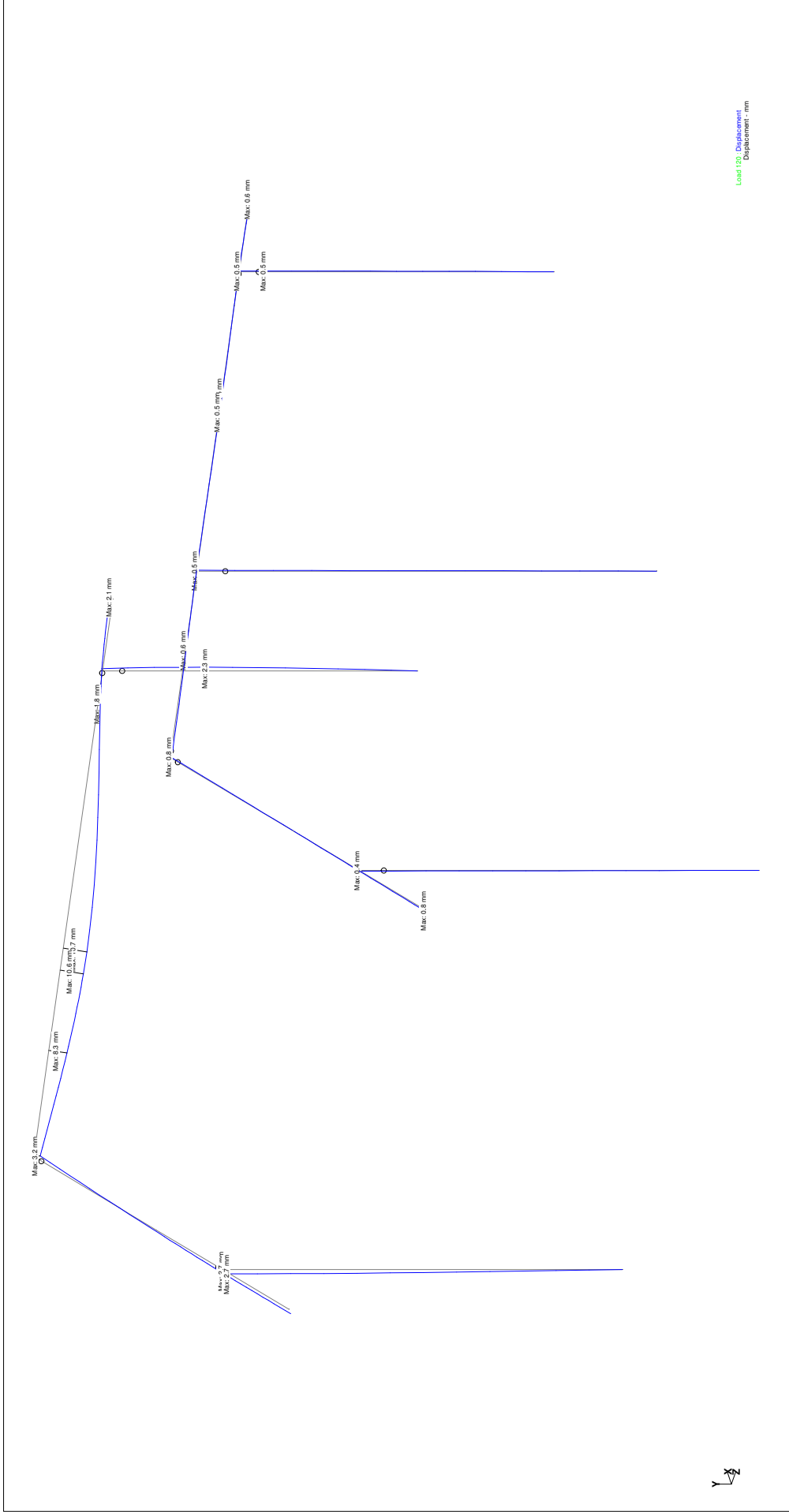
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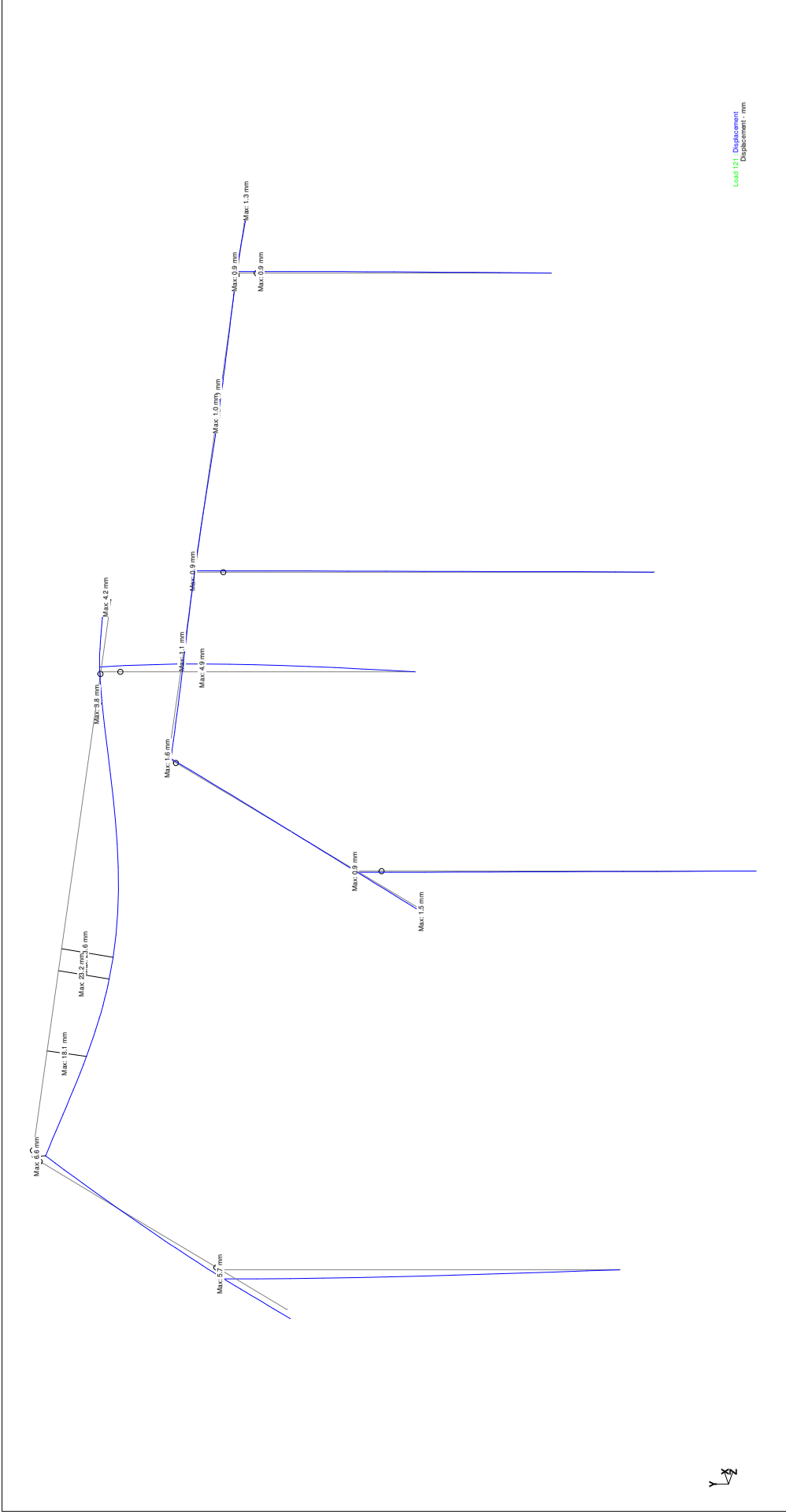
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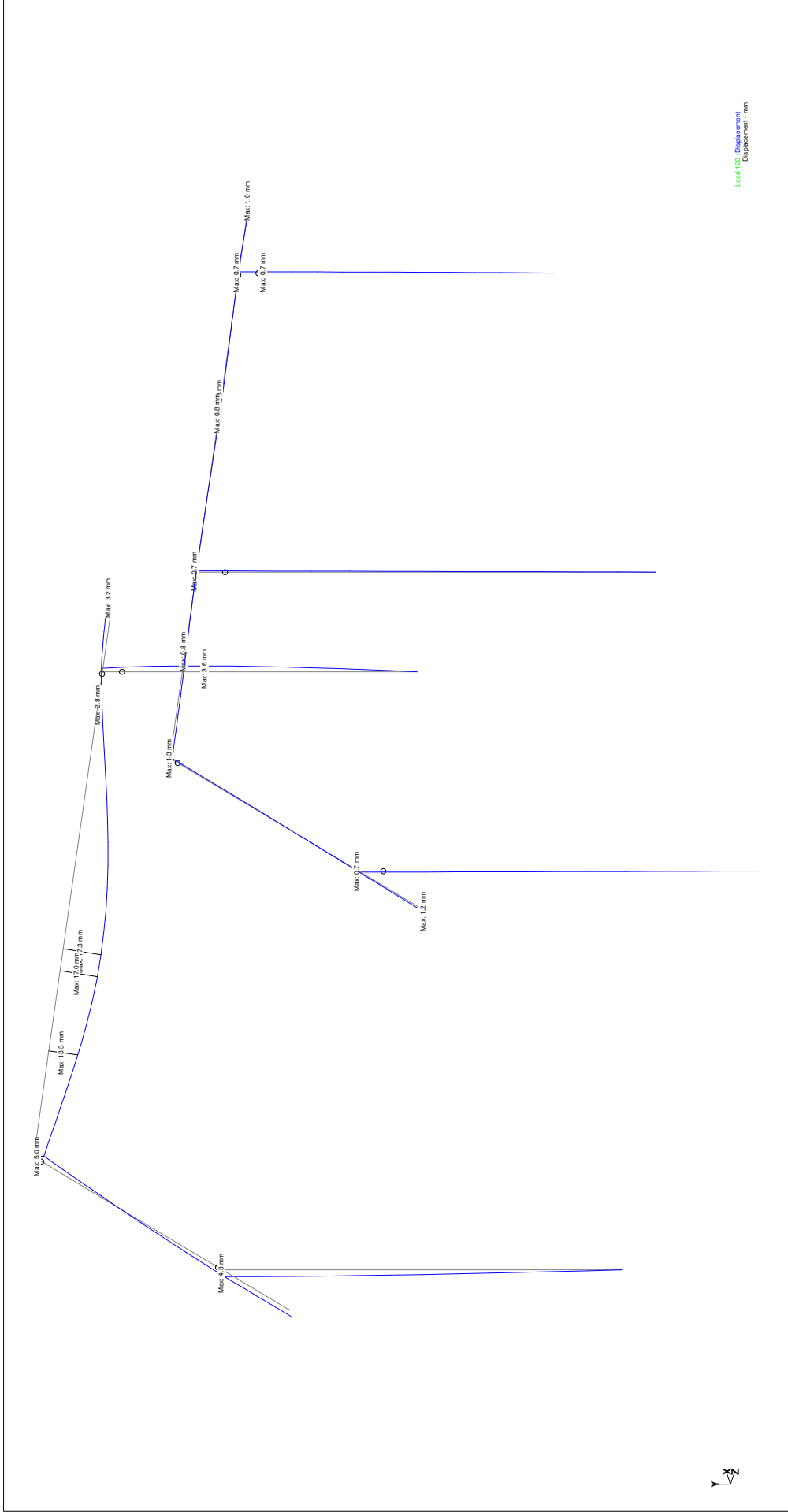


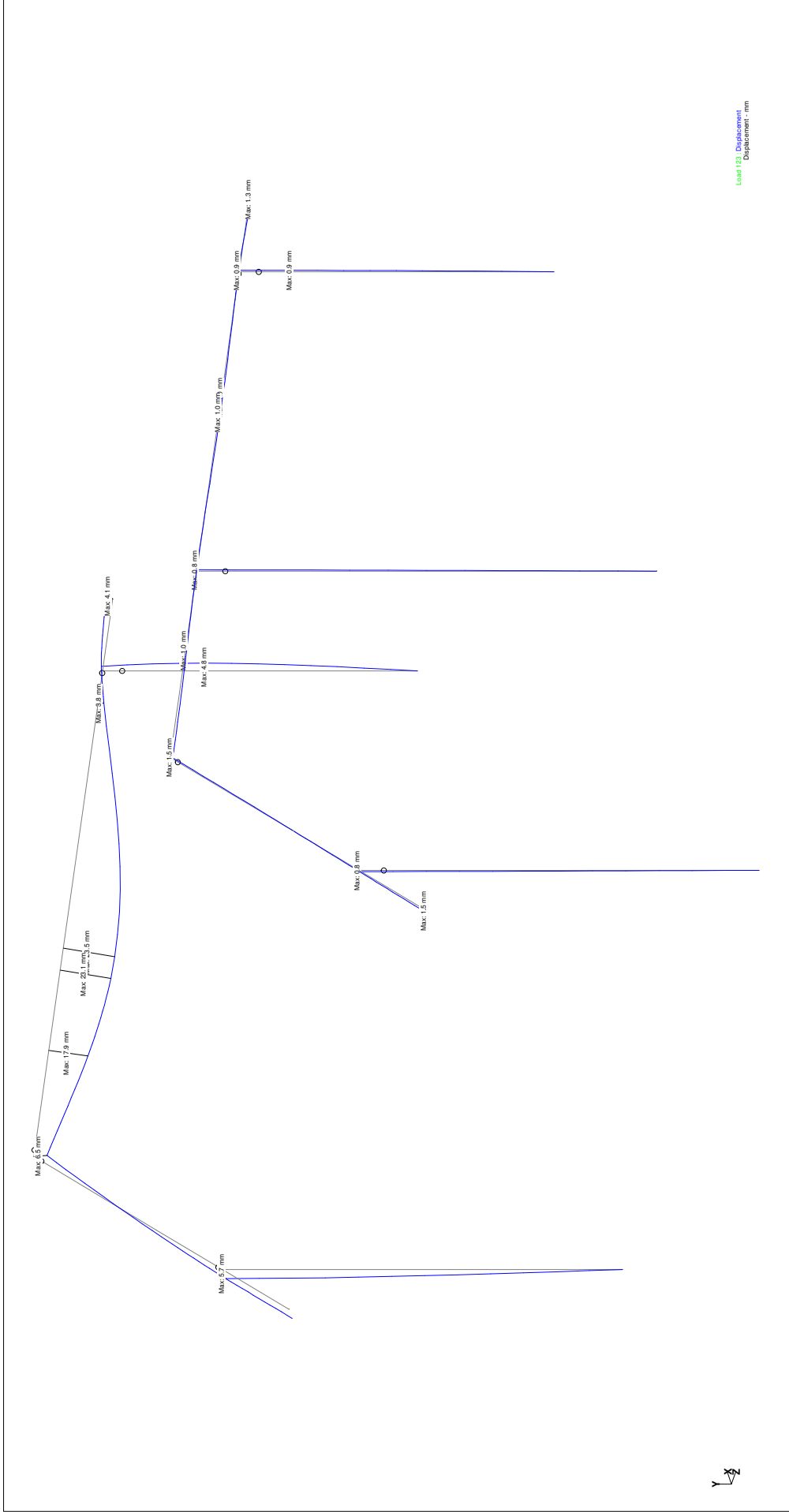


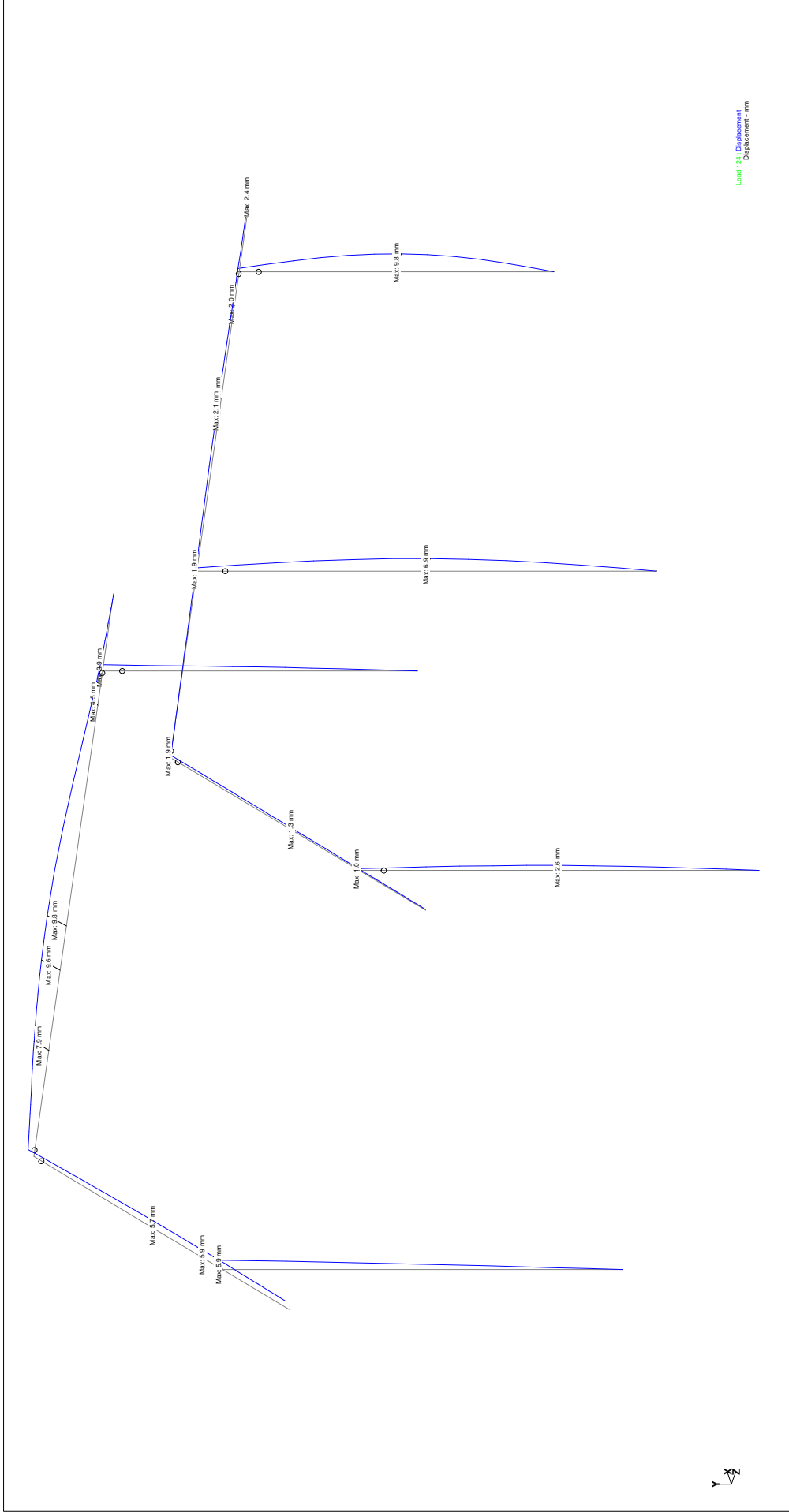
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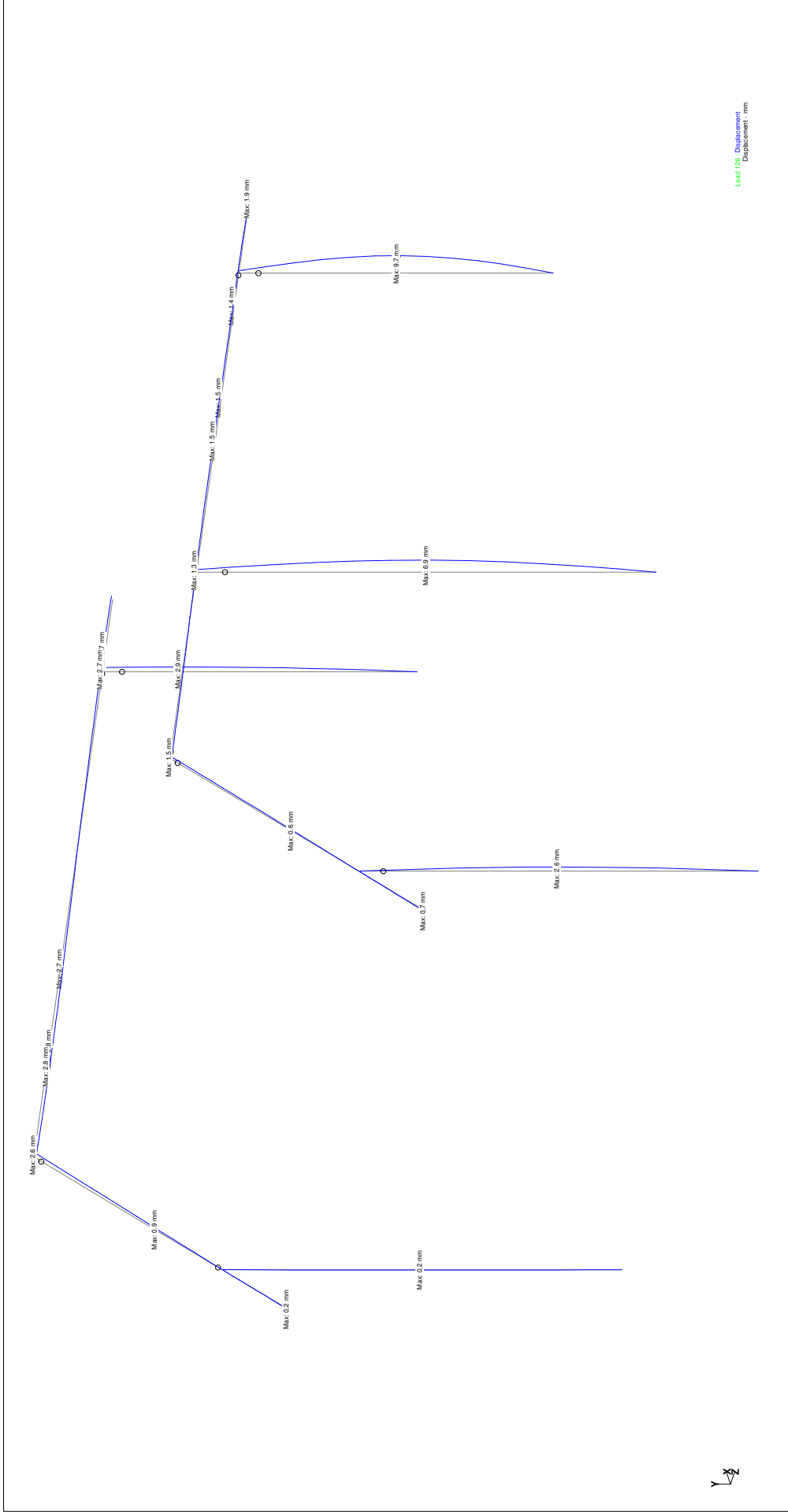


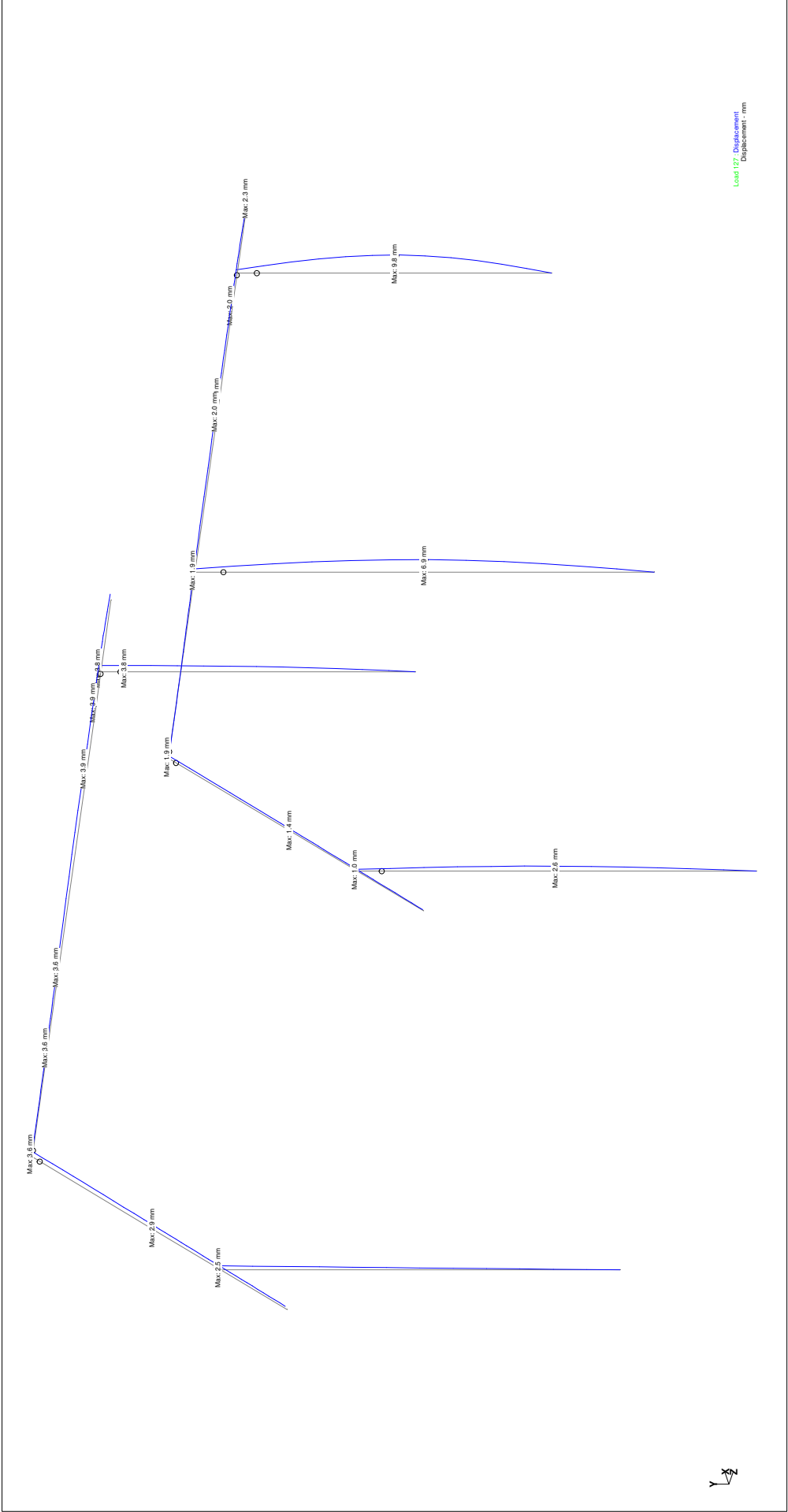


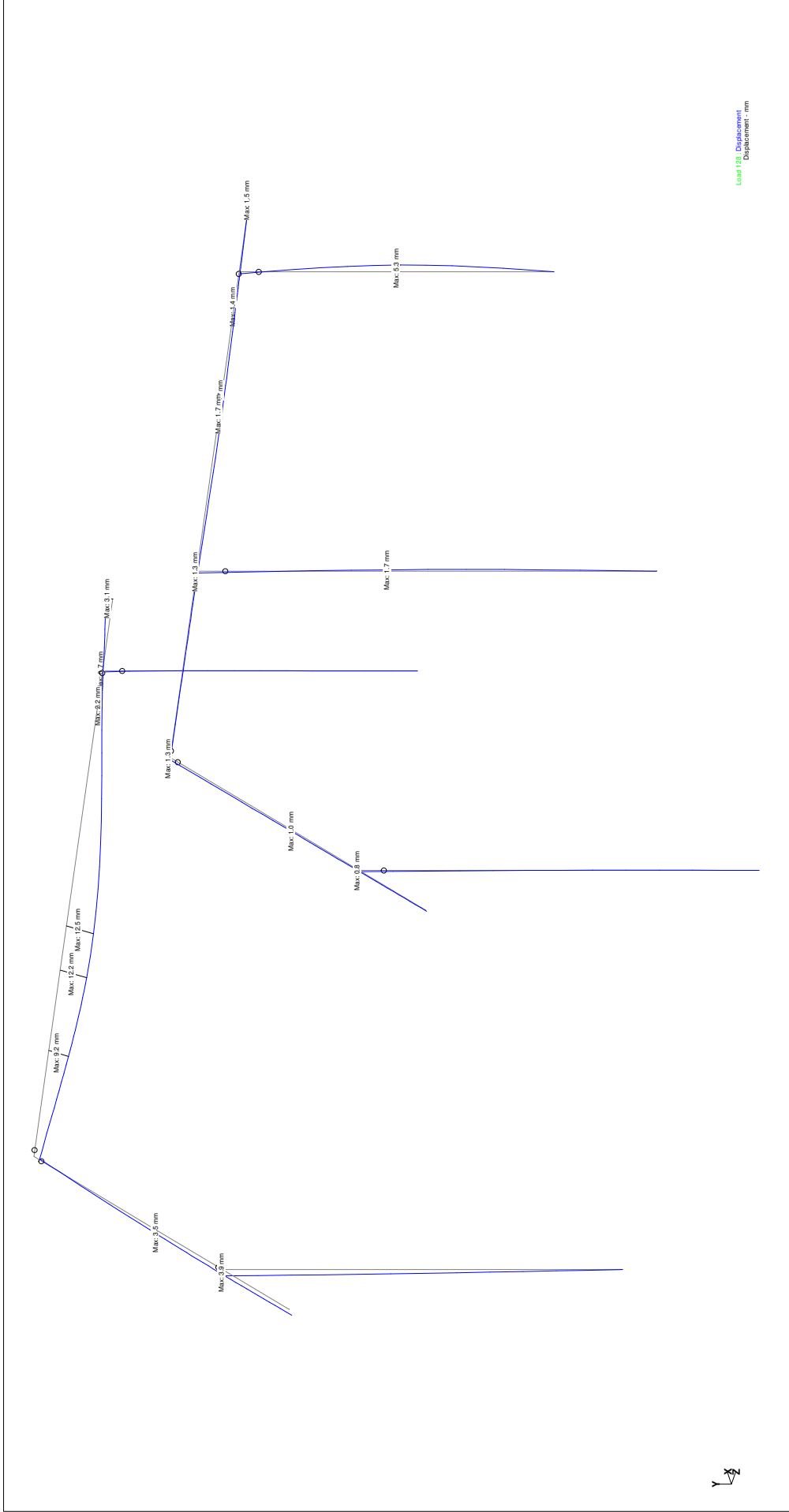


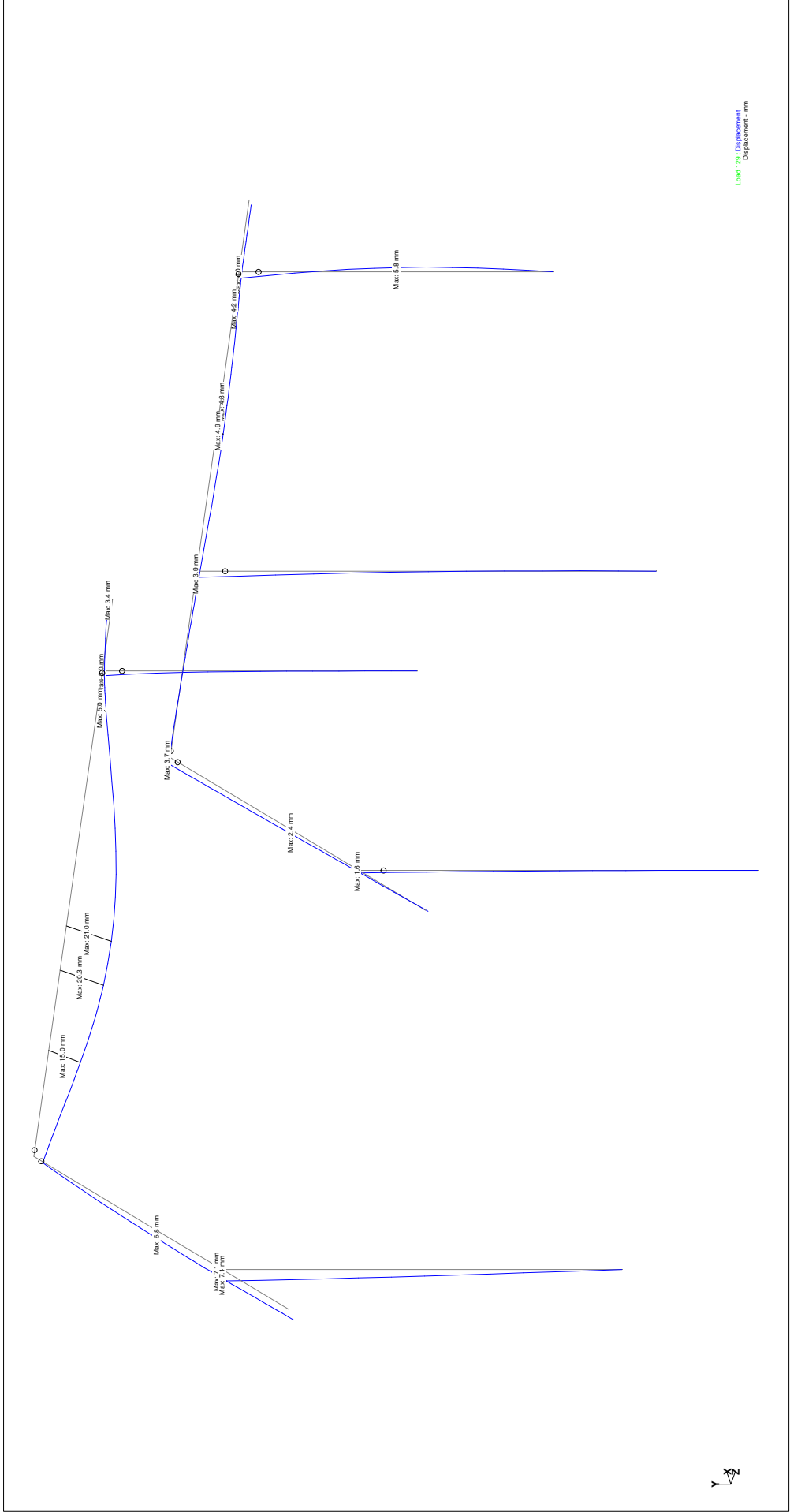


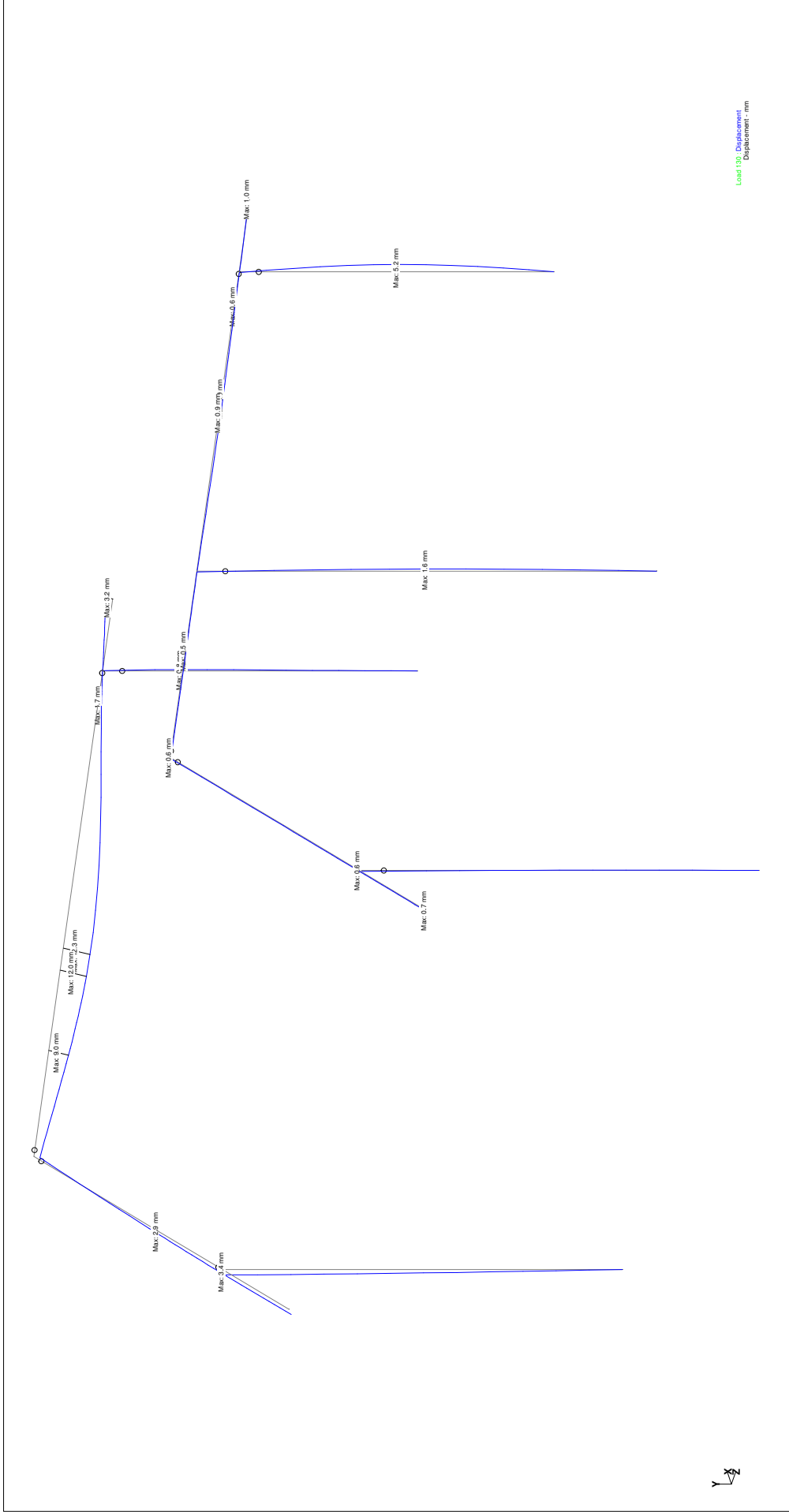


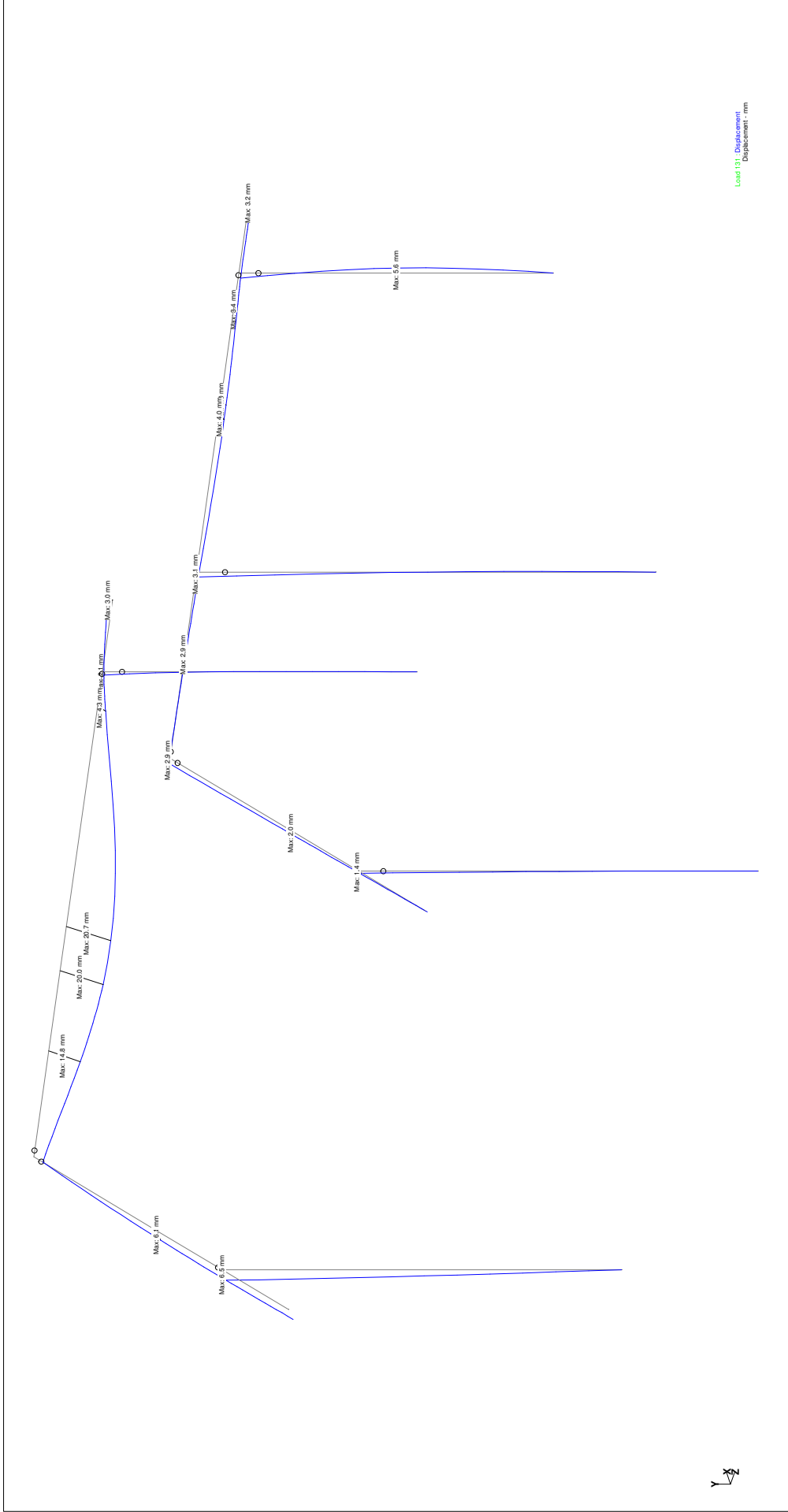


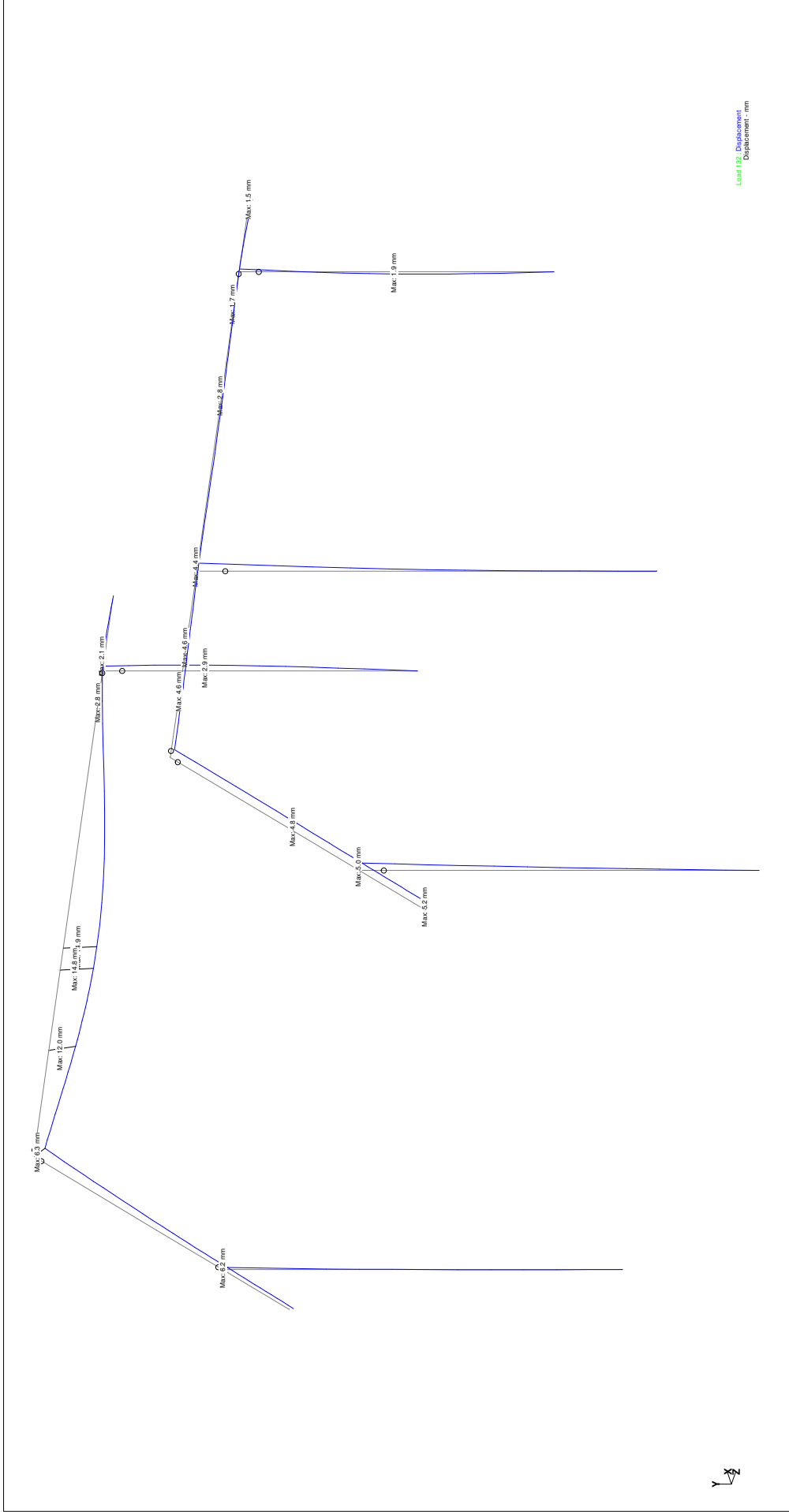


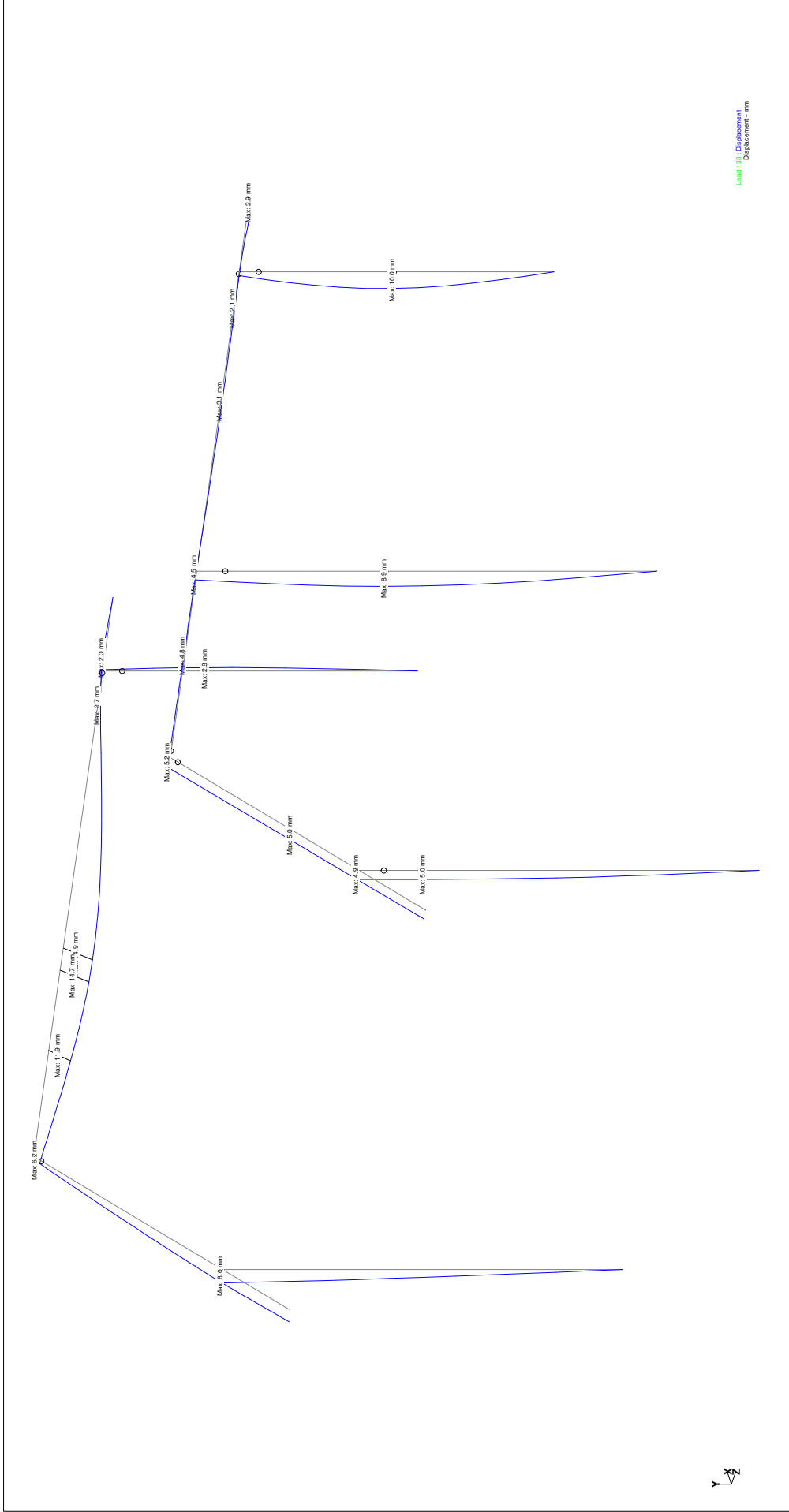












10.2 - numerieke computer in- en uitvoer

 KLOEZE bv ENGINEERING Software licensed to Engineering	Job No 9111-011	Sheet No 1	Rev
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Job Title Nieuwbouw schuur	Ref		
	By AdJ	Date 07-Jul-15	Chd PC
Client Fam. Venekamp / van Lingen	File 9111-011.std	Date/Time 08-Jul-2015 14:01	

Job Information

	Engineer	Checked	Approved
Name:	AdJ	PC	PC
Date:	07-Jul-15	08-Jul-15	08-Jul-15

Structure Type SPACE FRAME

Number of Nodes	37	Highest Node	44
Number of Elements	54	Highest Beam	68

Number of Basic Load Cases	56
Number of Combination Load Cases	0

Included in this printout are data for:

View	staafnummers tbv staafcontroles
------	---------------------------------

Included in this printout are results for load cases:

Type	L/C	Name
Primary	1	EG
Primary	2	BB DAK + WAND
Primary	3	SNEEUW1
Primary	4	SNEEUW2
Primary	5	SNEEUW3
Primary	6	WIND X1
Primary	7	WIND X2
Primary	8	WIND X3
Primary	9	WIND X4
Primary	10	WIND -X1
Primary	11	WIND -X2
Primary	12	WIND -X3
Primary	13	WIND -X4
Primary	14	WIND Z
Primary	15	WIND -Z
Primary	16	OVERDRUK WIND X
Primary	17	ONDERDRUK WIND -X
Primary	18	ONDERDRUK WIND Z
Primary	20	UGT1
Primary	21	UGT2
Primary	22	UGT3
Primary	23	UGT4
Primary	24	UGT5
Primary	25	UGT6
Primary	26	UGT7
Primary	27	UGT8
Primary	28	UGT9
Primary	29	UGT10
Primary	30	UGT11
Primary	31	UGT12
Primary	32	UGT13
Primary	33	UGT14
Primary	34	UGT15
Primary	35	UGT16
Primary	36	UGT17
Primary	37	UGT18
Primary	38	UGT19
Primary	39	UGT20
Primary	40	UGT21
Primary	41	UGT22
Primary	42	UGT23
Primary	43	UGT24
Primary	120	BGT1
Primary	121	BGT2
Primary	122	BGT3
Primary	123	BGT4
Primary	124	BGT5
Primary	125	BGT6
Primary	126	BGT7
Primary	127	BGT8
Primary	128	BGT9
Primary	129	BGT10
Primary	130	BGT11
Primary	131	BGT12
Primary	132	BGT13
Primary	133	BGT14

Section Properties

Prop	Section	Area (cm ²)	I _{yy} (cm ⁴)	I _{zz} (cm ⁴)	J (cm ⁴)	Material
1	IPE160	20.100	68.000	869.000	2.851	STEEL
2	PSS0X6	0.000	0.000	0.000	0.000	MATERIAL1
3	IPE160	20.100	68.000	869.000	2.851	STEEL
4	HE180A	45.300	925.000	2.51E+3	11.451	MATERIAL1
5	IPE160	20.100	68.000	869.000	2.851	STEEL
6	L50X5	4.800	17.811	4.692	0.406	MATERIAL1
7	KK70X3	7.880	58.460	58.460	90.229	STEEL
8	KK70X3	7.880	58.460	58.460	90.229	STEEL

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	Part Staalconstructie		
Job Title Nieuwbouw schuur	Ref		
	By AdJ	Date 07-Jul-15	Chd PC
Client Fam. Venekamp / van Lingen	File 9111-011.std	Date/Time 08-Jul-2015 14:01	

Materials

Mat	Name	E (kN/mm ²)	ν	Density (kg/m ³)	α (/°C)
1	STEEL	205.000	0.300	7.83E+3	12E-6
2	STAINLESSSTEEL	197.930	0.300	7.83E+3	18E-6
3	ALUMINUM	68.948	0.330	2.71E+3	23E-6
4	MATERIAL1	205.000	0.300	7.85E+3	12E-12
5	CONCRETE	21.718	0.170	2.4E+3	10E-6

Supports

Node	X (kN/mm)	Y (kN/mm)	Z (kN/mm)	rX (kN m/deg)	rY (kN m/deg)	rZ (kN m/deg)
25	Fixed	Fixed	Fixed	-	0.001	-
26	Fixed	Fixed	Fixed	-	0.001	-
27	Fixed	Fixed	Fixed	-	0.001	-
28	Fixed	Fixed	Fixed	-	0.001	-
29	Fixed	Fixed	Fixed	-	0.001	-

Releases

Beam ends not shown in this table are fixed in all directions.

Beam	Node	x	y	z	rx	ry	rz
25	4	Fixed	Fixed	Fixed	Spring	Spring	Spring
26	2	Fixed	Fixed	Fixed	Spring	Spring	Spring
27	21	Fixed	Fixed	Fixed	Fixed	Pin	Pin
28	13	Fixed	Fixed	Fixed	Fixed	Pin	Pin
44	2	Fixed	Fixed	Fixed	Spring	Spring	Spring
48	4	Fixed	Fixed	Fixed	Spring	Spring	Spring
55	23	Fixed	Fixed	Fixed	Fixed	Pin	Spring
56	17	Fixed	Fixed	Fixed	Spring	Spring	Spring
58	16	Fixed	Fixed	Fixed	Spring	Spring	Spring
62	17	Fixed	Fixed	Fixed	Spring	Spring	Spring
64	16	Fixed	Fixed	Fixed	Spring	Spring	Spring

Primary Load Cases

Number	Name	Type
1	EG	None
2	BB DAK + WAND	None
3	SNEEUW1	None
4	SNEEUW2	None
5	SNEEUW3	None
6	WIND X1	None
7	WIND X2	None
8	WIND X3	None
9	WIND X4	None
10	WIND -X1	None
11	WIND -X2	None
12	WIND -X3	None
13	WIND -X4	None
14	WIND Z	None
15	WIND -Z	None
16	OVERDRUK WIND X	None
17	ONDERDRUK WIND -X	None
18	ONDERDRUK WIND Z	None
20	UGT1	None
21	UGT2	None
22	UGT3	None
23	UGT4	None
24	UGT5	None
25	UGT6	None
26	UGT7	None
27	UGT8	None
28	UGT9	None
29	UGT10	None
30	UGT11	None
31	UGT12	None
32	UGT13	None
33	UGT14	None
34	UGT15	None
35	UGT16	None
36	UGT17	None
37	UGT18	None
38	UGT19	None
39	UGT20	None
40	UGT21	None
41	UGT22	None
42	UGT23	None
43	UGT24	None
120	BGT1	None
121	BGT2	None
122	BGT3	None
123	BGT4	None
124	BGT5	None
125	BGT6	None

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Primary Load Cases Cont...

Number	Name	Type
126	BGT7	None
127	BGT8	None
128	BGT9	None
129	BGT10	None
130	BGT11	None
131	BGT12	None
132	BGT13	None
133	BGT14	None

1 EG : Selfweight

Direction	Factor	Assigned Geometry
Y	-1.020	ALL

2 BB DAK + WAND : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	GY	-1.270	-	-	-	-
8	UNI kN/m	GY	-0.640	-	-	-	-
15	UNI kN/m	GY	-0.640	-	-	-	-
16	UNI kN/m	GY	-1.270	-	-	-	-
25	UNI kN/m	GY	-0.690	-	-	-	-
26	UNI kN/m	GY	-0.690	-	-	-	-
27	UNI kN/m	GY	-0.690	-	-	-	-
28	UNI kN/m	GY	-0.350	-	-	-	-
44	UNI kN/m	GY	-0.640	-	-	-	-
45	UNI kN/m	GY	-0.640	-	-	-	-
48	UNI kN/m	GY	-1.270	-	-	-	-
49	UNI kN/m	GY	-1.270	-	-	-	-
50	UNI kN/m	GY	-0.640	-	-	-	-
55	UNI kN/m	GY	-1.270	-	-	-	-
56	UNI kN/m	GY	-0.640	-	-	-	-
58	UNI kN/m	GY	-1.270	-	-	-	-
59	UNI kN/m	GY	-0.640	-	-	-	-
61	UNI kN/m	GY	-1.270	-	-	-	-
62	UNI kN/m	GY	-0.640	-	-	-	-
64	UNI kN/m	GY	-1.270	-	-	-	-
65	UNI kN/m	GY	-0.640	-	-	-	-

3 SNEEUW1 : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	GY	-2.000	-	-	-	-
8	UNI kN/m	GY	-0.380	-	-	-	-
15	UNI kN/m	GY	-1.000	-	-	-	-
16	UNI kN/m	GY	-0.750	-	-	-	-
44	UNI kN/m	GY	-1.000	-	-	-	-
45	UNI kN/m	GY	-1.000	-	-	-	-
48	UNI kN/m	GY	-2.000	-	-	-	-
49	UNI kN/m	GY	-2.000	-	-	-	-
50	UNI kN/m	GY	-0.380	-	-	-	-
55	UNI kN/m	GY	-0.750	-	-	-	-
56	UNI kN/m	GY	-0.380	-	-	-	-
58	UNI kN/m	GY	-0.750	-	-	-	-
59	UNI kN/m	GY	-1.000	-	-	-	-
61	UNI kN/m	GY	-2.000	-	-	-	-
62	UNI kN/m	GY	-1.000	-	-	-	-
64	UNI kN/m	GY	-2.000	-	-	-	-
65	UNI kN/m	GY	-1.000	-	-	-	-

4 SNEEUW2 : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	GY	-1.000	-	-	-	-
8	UNI kN/m	GY	-0.380	-	-	-	-
15	UNI kN/m	GY	-0.500	-	-	-	-
16	UNI kN/m	GY	-0.750	-	-	-	-
44	UNI kN/m	GY	-0.500	-	-	-	-
45	UNI kN/m	GY	-0.500	-	-	-	-
48	UNI kN/m	GY	-1.000	-	-	-	-
49	UNI kN/m	GY	-1.000	-	-	-	-
50	UNI kN/m	GY	-0.380	-	-	-	-
55	UNI kN/m	GY	-0.750	-	-	-	-
56	UNI kN/m	GY	-0.380	-	-	-	-
58	UNI kN/m	GY	-0.750	-	-	-	-
59	UNI kN/m	GY	-0.500	-	-	-	-
61	UNI kN/m	GY	-1.000	-	-	-	-
62	UNI kN/m	GY	-0.500	-	-	-	-
64	UNI kN/m	GY	-1.000	-	-	-	-
65	UNI kN/m	GY	-0.500	-	-	-	-



5 SNEEUW3 : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	GY	-2.000	-	-	-	-
8	UNI kN/m	GY	-0.190	-	-	-	-
15	UNI kN/m	GY	-1.000	-	-	-	-
16	UNI kN/m	GY	-0.380	-	-	-	-
44	UNI kN/m	GY	-1.000	-	-	-	-
45	UNI kN/m	GY	-1.000	-	-	-	-
48	UNI kN/m	GY	-2.000	-	-	-	-
49	UNI kN/m	GY	-2.000	-	-	-	-
50	UNI kN/m	GY	-0.190	-	-	-	-
55	UNI kN/m	GY	-0.380	-	-	-	-
56	UNI kN/m	GY	-0.190	-	-	-	-
58	UNI kN/m	GY	-0.380	-	-	-	-
59	UNI kN/m	GY	-1.000	-	-	-	-
61	UNI kN/m	GY	-2.000	-	-	-	-
62	UNI kN/m	GY	-1.000	-	-	-	-
64	UNI kN/m	GY	-2.000	-	-	-	-
65	UNI kN/m	GY	-1.000	-	-	-	-

6 WIND X1 : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	Y	-0.060	-	-	-	-
15	UNI kN/m	Y	-0.030	-	-	-	-
25	UNI kN/m	GX	0.990	-	-	-	-
26	UNI kN/m	GZ	0.700	-	-	-	-
	UNI kN/m	GX	0.500	-	-	-	-
27	UNI kN/m	GZ	1.390	-	-	-	-
28	UNI kN/m	GZ	1.110	-	-	-	-
44	UNI kN/m	Y	0.470	-	-	-	-
45	UNI kN/m	Y	0.470	-	-	-	-
48	UNI kN/m	Y	0.930	-	-	-	-
49	UNI kN/m	Y	0.930	-	-	-	-
59	UNI kN/m	Y	0.470	-	-	-	-
61	UNI kN/m	Y	0.930	-	-	-	-
62	UNI kN/m	Y	0.960	-	-	-	-
64	UNI kN/m	Y	1.920	-	-	-	-
65	UNI kN/m	Y	0.470	-	-	-	-

7 WIND X2 : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	Y	-0.060	-	-	-	-
8	UNI kN/m	Y	-0.810	-	-	-	-
15	UNI kN/m	Y	-0.030	-	-	-	-
16	UNI kN/m	Y	-1.620	-	-	-	-
25	UNI kN/m	GX	0.990	-	-	-	-
26	UNI kN/m	GZ	0.700	-	-	-	-
	UNI kN/m	GX	0.500	-	-	-	-
27	UNI kN/m	GZ	1.390	-	-	-	-
28	UNI kN/m	GZ	1.110	-	-	-	-
44	UNI kN/m	Y	0.470	-	-	-	-
45	UNI kN/m	Y	0.470	-	-	-	-
48	UNI kN/m	Y	0.930	-	-	-	-
49	UNI kN/m	Y	0.930	-	-	-	-
50	UNI kN/m	Y	-0.810	-	-	-	-
55	UNI kN/m	Y	-1.620	-	-	-	-
56	UNI kN/m	Y	-0.700	-	-	-	-
58	UNI kN/m	Y	-1.390	-	-	-	-
59	UNI kN/m	Y	0.470	-	-	-	-
61	UNI kN/m	Y	0.930	-	-	-	-
62	UNI kN/m	Y	0.960	-	-	-	-
64	UNI kN/m	Y	1.920	-	-	-	-
65	UNI kN/m	Y	0.470	-	-	-	-

8 WIND X3 : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	Y	-0.990	-	-	-	-
15	UNI kN/m	Y	-0.500	-	-	-	-
25	UNI kN/m	GX	0.990	-	-	-	-
26	UNI kN/m	GZ	0.700	-	-	-	-
	UNI kN/m	GX	0.500	-	-	-	-
27	UNI kN/m	GZ	1.390	-	-	-	-
28	UNI kN/m	GZ	1.110	-	-	-	-

**9 WIND X4 : Beam Loads**

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	Y	-0.990	-	-	-	-
8	UNI kN/m	Y	-0.810	-	-	-	-
15	UNI kN/m	Y	-0.500	-	-	-	-
16	UNI kN/m	Y	-1.620	-	-	-	-
25	UNI kN/m	GX	0.990	-	-	-	-
26	UNI kN/m	GZ	0.700	-	-	-	-
	UNI kN/m	GX	0.500	-	-	-	-
27	UNI kN/m	GZ	1.390	-	-	-	-
28	UNI kN/m	GZ	1.110	-	-	-	-
50	UNI kN/m	Y	-0.810	-	-	-	-
55	UNI kN/m	Y	-1.620	-	-	-	-
56	UNI kN/m	Y	-0.700	-	-	-	-
58	UNI kN/m	Y	-1.390	-	-	-	-

10 WIND -X1 : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	Y	3.200	-	-	-	-
8	UNI kN/m	Y	0.240	-	-	-	-
15	UNI kN/m	Y	1.680	-	-	-	-
16	UNI kN/m	Y	0.470	-	-	-	-
25	UNI kN/m	GX	-1.580	-	-	-	-
26	UNI kN/m	GZ	1.110	-	-	-	-
	UNI kN/m	GX	-0.790	-	-	-	-
27	UNI kN/m	GZ	1.390	-	-	-	-
28	UNI kN/m	GZ	0.700	-	-	-	-
44	UNI kN/m	Y	0.890	-	-	-	-
45	UNI kN/m	Y	0.320	-	-	-	-
48	UNI kN/m	Y	1.620	-	-	-	-
49	UNI kN/m	Y	0.630	-	-	-	-
50	UNI kN/m	Y	0.240	-	-	-	-
55	UNI kN/m	Y	0.470	-	-	-	-
56	UNI kN/m	Y	0.350	-	-	-	-
58	UNI kN/m	Y	0.700	-	-	-	-
59	UNI kN/m	Y	0.320	-	-	-	-
61	UNI kN/m	Y	0.630	-	-	-	-
62	UNI kN/m	Y	0.320	-	-	-	-
64	UNI kN/m	Y	0.630	-	-	-	-
65	UNI kN/m	Y	0.320	-	-	-	-

11 WIND -X2 : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	Y	0.720	-	-	-	-
8	UNI kN/m	Y	0.240	-	-	-	-
15	UNI kN/m	Y	0.360	-	-	-	-
16	UNI kN/m	Y	0.470	-	-	-	-
25	UNI kN/m	GX	-1.580	-	-	-	-
26	UNI kN/m	GZ	1.110	-	-	-	-
	UNI kN/m	GX	-0.790	-	-	-	-
27	UNI kN/m	GZ	1.390	-	-	-	-
28	UNI kN/m	GZ	0.700	-	-	-	-
44	UNI kN/m	Y	-0.430	-	-	-	-
45	UNI kN/m	Y	-0.320	-	-	-	-
48	UNI kN/m	Y	-0.860	-	-	-	-
49	UNI kN/m	Y	-0.630	-	-	-	-
50	UNI kN/m	Y	0.240	-	-	-	-
55	UNI kN/m	Y	0.470	-	-	-	-
56	UNI kN/m	Y	0.350	-	-	-	-
58	UNI kN/m	Y	0.700	-	-	-	-
59	UNI kN/m	Y	-0.320	-	-	-	-
61	UNI kN/m	Y	-0.630	-	-	-	-
62	UNI kN/m	Y	-0.320	-	-	-	-
64	UNI kN/m	Y	-0.630	-	-	-	-
65	UNI kN/m	Y	-0.320	-	-	-	-



12 WIND -X3 : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	Y	3.200	-	-	-	-
15	UNI kN/m	Y	1.680	-	-	-	-
25	UNI kN/m	GX	-1.580	-	-	-	-
26	UNI kN/m	GZ	1.110	-	-	-	-
	UNI kN/m	GX	-0.790	-	-	-	-
27	UNI kN/m	GZ	1.390	-	-	-	-
28	UNI kN/m	GZ	0.700	-	-	-	-
44	UNI kN/m	Y	0.890	-	-	-	-
45	UNI kN/m	Y	0.320	-	-	-	-
48	UNI kN/m	Y	1.620	-	-	-	-
49	UNI kN/m	Y	0.630	-	-	-	-
59	UNI kN/m	Y	0.320	-	-	-	-
61	UNI kN/m	Y	0.630	-	-	-	-
62	UNI kN/m	Y	0.320	-	-	-	-
64	UNI kN/m	Y	0.630	-	-	-	-
65	UNI kN/m	Y	0.320	-	-	-	-

13 WIND -X4 : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	Y	0.720	-	-	-	-
15	UNI kN/m	Y	0.360	-	-	-	-
25	UNI kN/m	GX	-1.580	-	-	-	-
26	UNI kN/m	GZ	1.110	-	-	-	-
	UNI kN/m	GX	-0.790	-	-	-	-
27	UNI kN/m	GZ	1.390	-	-	-	-
28	UNI kN/m	GZ	0.700	-	-	-	-
44	UNI kN/m	Y	-0.430	-	-	-	-
45	UNI kN/m	Y	-0.320	-	-	-	-
48	UNI kN/m	Y	-0.860	-	-	-	-
49	UNI kN/m	Y	-0.630	-	-	-	-
59	UNI kN/m	Y	-0.320	-	-	-	-
61	UNI kN/m	Y	-0.630	-	-	-	-
62	UNI kN/m	Y	-0.320	-	-	-	-
64	UNI kN/m	Y	-0.630	-	-	-	-
65	UNI kN/m	Y	-0.320	-	-	-	-

14 WIND Z : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	Y	-0.590	-	-	-	-
8	UNI kN/m	Y	0.560	-	-	-	-
15	UNI kN/m	Y	-0.020	-	-	-	-
16	UNI kN/m	Y	1.390	-	-	-	-
25	UNI kN/m	GX	1.850	-	-	-	-
26	UNI kN/m	GZ	0.370	-	-	-	-
	UNI kN/m	GX	0.580	-	-	-	-
27	UNI kN/m	GZ	0.740	-	-	-	-
28	UNI kN/m	GZ	0.370	-	-	-	-
44	UNI kN/m	Y	0.560	-	-	-	-
45	UNI kN/m	Y	0.560	-	-	-	-
48	UNI kN/m	Y	1.260	-	-	-	-
49	UNI kN/m	Y	1.260	-	-	-	-
50	UNI kN/m	Y	0.560	-	-	-	-
55	UNI kN/m	Y	1.390	-	-	-	-
56	UNI kN/m	Y	0.560	-	-	-	-
58	UNI kN/m	Y	1.390	-	-	-	-
59	UNI kN/m	Y	0.560	-	-	-	-
61	UNI kN/m	Y	1.260	-	-	-	-
62	UNI kN/m	Y	0.560	-	-	-	-
64	UNI kN/m	Y	1.260	-	-	-	-
65	UNI kN/m	Y	0.560	-	-	-	-



15 WIND -Z : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	Y	-0.590	-	-	-	-
8	UNI kN/m	Y	1.110	-	-	-	-
15	UNI kN/m	Y	-0.240	-	-	-	-
16	UNI kN/m	Y	1.390	-	-	-	-
25	UNI kN/m	GX	1.850	-	-	-	-
26	UNI kN/m	GZ	-0.600	-	-	-	-
	UNI kN/m	GX	1.210	-	-	-	-
27	UNI kN/m	GZ	-1.180	-	-	-	-
28	UNI kN/m	GZ	-0.600	-	-	-	-
44	UNI kN/m	Y	0.970	-	-	-	-
45	UNI kN/m	Y	1.010	-	-	-	-
48	UNI kN/m	Y	1.260	-	-	-	-
49	UNI kN/m	Y	1.260	-	-	-	-
50	UNI kN/m	Y	1.110	-	-	-	-
55	UNI kN/m	Y	1.390	-	-	-	-
56	UNI kN/m	Y	1.110	-	-	-	-
58	UNI kN/m	Y	1.390	-	-	-	-
59	UNI kN/m	Y	0.970	-	-	-	-
61	UNI kN/m	Y	1.260	-	-	-	-
62	UNI kN/m	Y	1.010	-	-	-	-
64	UNI kN/m	Y	1.260	-	-	-	-
65	UNI kN/m	Y	1.010	-	-	-	-

16 OVERDRUK WIND X : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	Y	1.670	-	-	-	-
8	UNI kN/m	Y	0.840	-	-	-	-
15	UNI kN/m	Y	0.840	-	-	-	-
16	UNI kN/m	Y	1.670	-	-	-	-
25	UNI kN/m	GX	1.670	-	-	-	-
26	UNI kN/m	GZ	0.630	-	-	-	-
	UNI kN/m	GX	0.840	-	-	-	-
27	UNI kN/m	GZ	1.250	-	-	-	-
28	UNI kN/m	GZ	0.630	-	-	-	-
44	UNI kN/m	Y	0.840	-	-	-	-
45	UNI kN/m	Y	0.840	-	-	-	-
48	UNI kN/m	Y	1.670	-	-	-	-
49	UNI kN/m	Y	1.670	-	-	-	-
50	UNI kN/m	Y	0.840	-	-	-	-
55	UNI kN/m	Y	1.670	-	-	-	-
56	UNI kN/m	Y	0.840	-	-	-	-
58	UNI kN/m	Y	1.670	-	-	-	-
59	UNI kN/m	Y	0.840	-	-	-	-
61	UNI kN/m	Y	1.670	-	-	-	-
62	UNI kN/m	Y	0.840	-	-	-	-
64	UNI kN/m	Y	1.670	-	-	-	-
65	UNI kN/m	Y	0.840	-	-	-	-

17 ONDERDRUK WIND -X : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	Y	-1.040	-	-	-	-
8	UNI kN/m	Y	-0.520	-	-	-	-
15	UNI kN/m	Y	-0.520	-	-	-	-
16	UNI kN/m	Y	-1.040	-	-	-	-
25	UNI kN/m	GX	-1.040	-	-	-	-
26	UNI kN/m	GZ	-0.390	-	-	-	-
	UNI kN/m	GX	-0.520	-	-	-	-
27	UNI kN/m	GZ	-0.780	-	-	-	-
28	UNI kN/m	GZ	-0.390	-	-	-	-
44	UNI kN/m	Y	-0.520	-	-	-	-
45	UNI kN/m	Y	-0.520	-	-	-	-
48	UNI kN/m	Y	-1.040	-	-	-	-
49	UNI kN/m	Y	-1.040	-	-	-	-
50	UNI kN/m	Y	-0.520	-	-	-	-
55	UNI kN/m	Y	-1.040	-	-	-	-
56	UNI kN/m	Y	-0.520	-	-	-	-
58	UNI kN/m	Y	-1.040	-	-	-	-
59	UNI kN/m	Y	-0.520	-	-	-	-
61	UNI kN/m	Y	-1.040	-	-	-	-
62	UNI kN/m	Y	-0.520	-	-	-	-
64	UNI kN/m	Y	-1.040	-	-	-	-
65	UNI kN/m	Y	-0.520	-	-	-	-

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18 ONDERDRUK WIND Z : Beam Loads

Beam	Type	Direction	Fa	Da (m)	Fb	Db	Ecc. (m)
5	UNI kN/m	Y	-1.830	-	-	-	-
8	UNI kN/m	Y	-0.910	-	-	-	-
15	UNI kN/m	Y	-0.910	-	-	-	-
16	UNI kN/m	Y	-1.830	-	-	-	-
25	UNI kN/m	GX	-1.830	-	-	-	-
26	UNI kN/m	GZ	-0.690	-	-	-	-
	UNI kN/m	GX	-0.910	-	-	-	-
27	UNI kN/m	GZ	-1.370	-	-	-	-
28	UNI kN/m	GZ	-0.690	-	-	-	-
44	UNI kN/m	Y	-0.910	-	-	-	-
45	UNI kN/m	Y	-0.910	-	-	-	-
48	UNI kN/m	Y	-1.830	-	-	-	-
49	UNI kN/m	Y	-1.830	-	-	-	-
50	UNI kN/m	Y	-0.910	-	-	-	-
55	UNI kN/m	Y	-1.830	-	-	-	-
56	UNI kN/m	Y	-0.910	-	-	-	-
58	UNI kN/m	Y	-1.830	-	-	-	-
59	UNI kN/m	Y	-0.910	-	-	-	-
61	UNI kN/m	Y	-1.830	-	-	-	-
62	UNI kN/m	Y	-0.910	-	-	-	-
64	UNI kN/m	Y	-1.830	-	-	-	-
65	UNI kN/m	Y	-0.910	-	-	-	-

20 UGT1 : Repeat Loads

Ref	Name	Factor
1	EG	1.220
2	BB DAK + WAND	1.220

21 UGT2 : Repeat Loads

Ref	Name	Factor
1	EG	1.080
2	BB DAK + WAND	1.080
3	SNEEUW1	1.350

22 UGT3 : Repeat Loads

Ref	Name	Factor
1	EG	1.080
2	BB DAK + WAND	1.080
4	SNEEUW2	1.350

23 UGT4 : Repeat Loads

Ref	Name	Factor
1	EG	1.080
2	BB DAK + WAND	1.080
5	SNEEUW3	1.350

24 UGT5 : Repeat Loads

Ref	Name	Factor
1	EG	1.080
2	BB DAK + WAND	1.080
6	WIND X1	1.350
16	OVERDRUK WIND X	1.350

25 UGT6 : Repeat Loads

Ref	Name	Factor
1	EG	1.080
2	BB DAK + WAND	1.080
7	WIND X2	1.350
16	OVERDRUK WIND X	1.350

26 UGT7 : Repeat Loads

Ref	Name	Factor
1	EG	1.080
2	BB DAK + WAND	1.080
8	WIND X3	1.350
16	OVERDRUK WIND X	1.350



27 UGT8 : Repeat Loads

Ref	Name	Factor
1	EG	1.080
2	BB DAK + WAND	1.080
9	WIND X4	1.350
16	ONDERDRUK WIND X	1.350

28 UGT9 : Repeat Loads

Ref	Name	Factor
1	EG	1.080
2	BB DAK + WAND	1.080
10	WIND -X1	1.350
17	ONDERDRUK WIND -X	1.350

29 UGT10 : Repeat Loads

Ref	Name	Factor
1	EG	1.080
2	BB DAK + WAND	1.080
11	WIND -X2	1.350
17	ONDERDRUK WIND -X	1.350

30 UGT11 : Repeat Loads

Ref	Name	Factor
1	EG	1.080
2	BB DAK + WAND	1.080
12	WIND -X3	1.350
17	ONDERDRUK WIND -X	1.350

31 UGT12 : Repeat Loads

Ref	Name	Factor
1	EG	1.080
2	BB DAK + WAND	1.080
13	WIND -X4	1.350
17	ONDERDRUK WIND -X	1.350

32 UGT13 : Repeat Loads

Ref	Name	Factor
1	EG	1.080
2	BB DAK + WAND	1.080
14	WIND Z	1.350
18	ONDERDRUK WIND Z	1.350

33 UGT14 : Repeat Loads

Ref	Name	Factor
1	EG	1.080
2	BB DAK + WAND	1.080
15	WIND -Z	1.350
18	ONDERDRUK WIND Z	1.350

34 UGT15 : Repeat Loads

Ref	Name	Factor
1	EG	0.900
2	BB DAK + WAND	0.900
6	WIND X1	1.350
16	ONDERDRUK WIND X	1.350

35 UGT16 : Repeat Loads

Ref	Name	Factor
1	EG	0.900
2	BB DAK + WAND	0.900
7	WIND X2	1.350
16	ONDERDRUK WIND X	1.350

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36 UGT17 : Repeat Loads

Ref	Name	Factor
1	EG	0.900
2	BB DAK + WAND	0.900
8	WIND X3	1.350
16	OVERDRUK WIND X	1.350

37 UGT18 : Repeat Loads

Ref	Name	Factor
1	EG	0.900
2	BB DAK + WAND	0.900
9	WIND X4	1.350
16	OVERDRUK WIND X	1.350

38 UGT19 : Repeat Loads

Ref	Name	Factor
1	EG	0.900
2	BB DAK + WAND	0.900
10	WIND -X1	1.350
17	ONDERDRUK WIND -X	1.350

39 UGT20 : Repeat Loads

Ref	Name	Factor
1	EG	0.900
2	BB DAK + WAND	0.900
11	WIND -X2	1.350
17	ONDERDRUK WIND -X	1.350

40 UGT21 : Repeat Loads

Ref	Name	Factor
1	EG	0.900
2	BB DAK + WAND	0.900
12	WIND -X3	1.350
17	ONDERDRUK WIND -X	1.350

41 UGT22 : Repeat Loads

Ref	Name	Factor
1	EG	0.900
2	BB DAK + WAND	0.900
13	WIND -X4	1.350
17	ONDERDRUK WIND -X	1.350

42 UGT23 : Repeat Loads

Ref	Name	Factor
1	EG	0.900
2	BB DAK + WAND	0.900
14	WIND Z	1.350
18	ONDERDRUK WIND Z	1.350

43 UGT24 : Repeat Loads

Ref	Name	Factor
1	EG	0.900
2	BB DAK + WAND	0.900
15	WIND -Z	1.350
18	ONDERDRUK WIND Z	1.350

120 BGT1 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000

121 BGT2 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000
3	SNEEUW1	1.000



122 BGT3 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000
4	SNEEUW2	1.000

123 BGT4 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000
5	SNEEUW3	1.000

124 BGT5 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000
6	WIND X1	1.000
16	OVERDRUK WIND X	1.000

125 BGT6 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000
7	WIND X2	1.000
16	OVERDRUK WIND X	1.000

126 BGT7 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000
8	WIND X3	1.000
16	OVERDRUK WIND X	1.000

127 BGT8 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000
9	WIND X4	1.000
16	OVERDRUK WIND X	1.000

128 BGT9 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000
10	WIND -X1	1.000
17	ONDERDRUK WIND -X	1.000

129 BGT10 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000
11	WIND -X2	1.000
17	ONDERDRUK WIND -X	1.000

130 BGT11 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000
12	WIND -X3	1.000
17	ONDERDRUK WIND -X	1.000

131 BGT12 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000
13	WIND -X4	1.000
17	ONDERDRUK WIND -X	1.000

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132 BGT13 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000
14	WIND Z	1.000
18	ONDERDRUK WIND Z	1.000

133 BGT14 : Repeat Loads

Ref	Name	Factor
1	EG	1.000
2	BB DAK + WAND	1.000
15	WIND -Z	1.000
18	ONDERDRUK WIND Z	1.000



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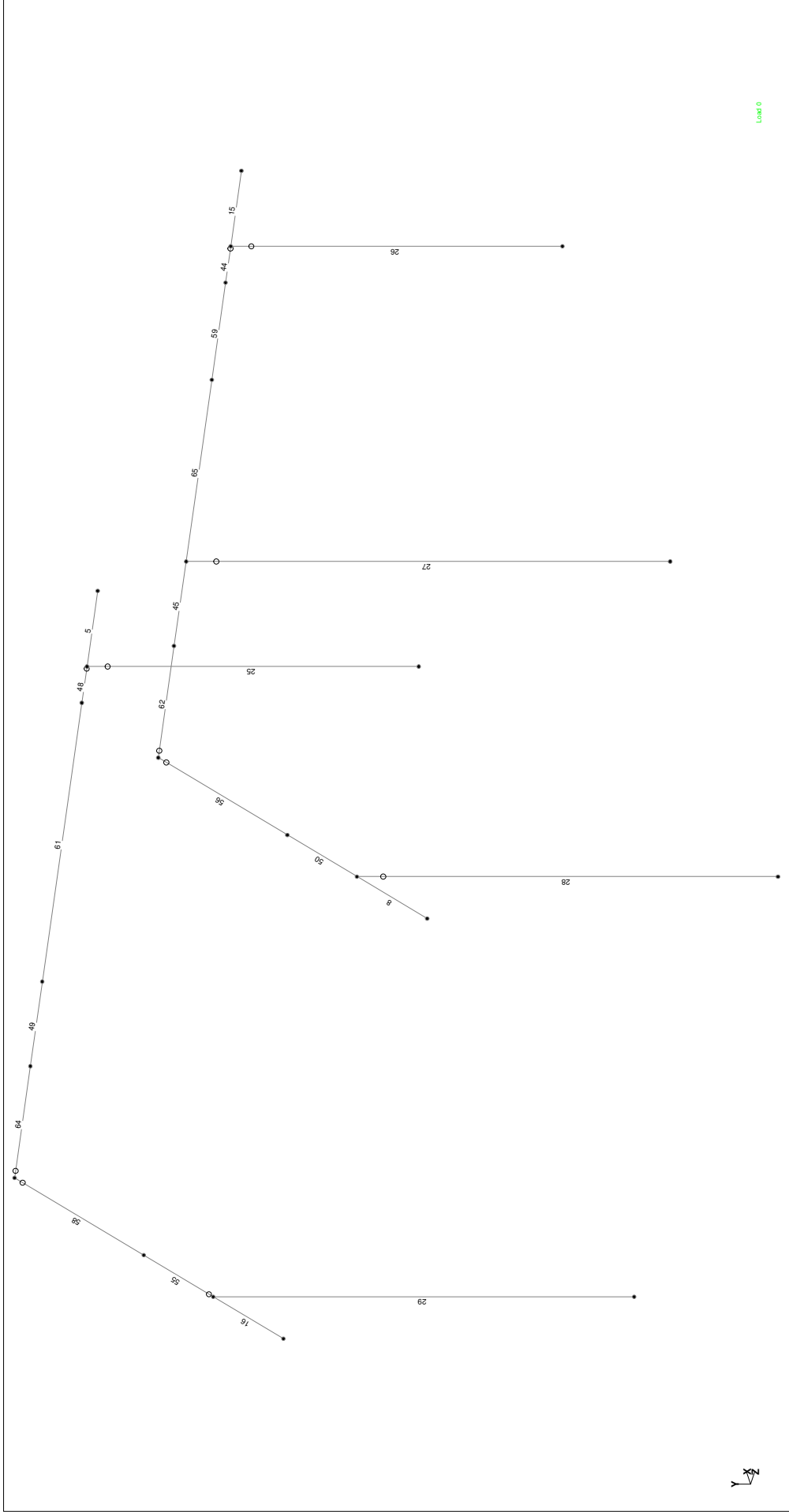
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Steel Design (Track 2) Beam 5 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
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```
=====
      5 ST   KK70X3      (DUTCH SECTIONS)
                        PASS      EC-6.2.9.1      0.458      32
=====
                        0.47 T      0.00      -2.12      0.96
=====
```

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 95.78
Gross Area = 7.88 Net Area = 7.88

	z-axis	y-axis
Moment of inertia	58.460	58.460
Plastic modulus	19.684	19.684
Elastic modulus	16.703	16.703
Shear Area	3.940	3.940
Radius of gyration	2.724	2.724
Effective Length	95.776	95.776

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 185.18
Axial force/Squash load : 0.003
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	35.2	35.2
Compression Capacity	177.7	177.7
Tension Capacity	185.2	185.2
Moment Capacity	4.6	4.6
Reduced Moment Capacity	4.6	4.6
Shear Capacity	53.5	53.5

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 4.6
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 0.958

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.007	21	-1.4	3.7	0.0	-1.8	0.0
EC-6.2.9.1	0.458	32	-0.5	4.4	0.0	-2.1	0.0
EC-6.2.5	0.317	12	0.0	-3.1	0.0	1.5	0.0
EC-6.2.6-(Y)	0.083	32	-0.5	4.4	0.0	-2.1	0.0
EC-6.3.2 LTb	0.317	12	0.0	-3.1	0.0	1.5	0.0

Torsion and deflections have not been considered in the design.

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Steel Design (Track 2) Beam 8 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					
8 ST	IPE160	(DUTCH SECTIONS)			
		PASS	EC-6.2.9.1	0.011	30
		0.43 T	0.00	-0.33	0.71
=====					

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 70.71
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	70.711	70.711

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.001
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	10.8	38.4
Compression Capacity	472.4	435.7
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 28.9
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 0.707

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.001	21	-0.7	0.7	0.0	-0.2	0.0
EC-6.2.9.1	0.011	30	-0.4	0.9	0.0	-0.3	0.0
EC-6.2.5	0.010	15	0.0	-0.8	0.0	0.3	0.0
EC-6.2.6-(Y)	0.007	30	-0.4	0.9	0.0	-0.3	0.0
EC-6.3.2 LTB	0.011	30	-0.4	0.9	0.0	-0.3	0.0

Torsion and deflections have not been considered in the design.

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Steel Design (Track 2) Beam 15 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
--------	-------	---------------	----------------------	--------------	----------------------

```

=====
15 ST   KK70X3      (DUTCH SECTIONS)
                        PASS      EC-6.2.9.1      0.225      33
                        0.25 T      0.00      -1.04      0.96
=====

```

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 95.78
Gross Area = 7.88 Net Area = 7.88

	z-axis	y-axis
Moment of inertia	58.460	58.460
Plastic modulus	19.684	19.684
Elastic modulus	16.703	16.703
Shear Area	3.940	3.940
Radius of gyration	2.724	2.724
Effective Length	95.776	95.776

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 185.18
Axial force/Squash load : 0.001
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	35.2	35.2
Compression Capacity	177.7	177.7
Tension Capacity	185.2	185.2
Moment Capacity	4.6	4.6
Reduced Moment Capacity	4.6	4.6
Shear Capacity	53.5	53.5

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 4.6
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 0.958

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.004	21	-0.7	1.9	0.0	-0.9	0.0
EC-6.2.9.1	0.225	33	-0.2	2.2	0.0	-1.0	0.0
EC-6.2.5	0.167	10	0.0	-1.6	0.0	0.8	0.0
EC-6.2.6-(Y)	0.041	33	-0.2	2.2	0.0	-1.0	0.0
EC-6.3.2 LTb	0.167	10	0.0	-1.6	0.0	0.8	0.0

Torsion and deflections have not been considered in the design.

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Steel Design (Track 2) Beam 16 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					
16 ST	IPE160	(DUTCH SECTIONS)			
	PASS	EC-6.3.2 LTB		0.022	30
	0.77 T	0.00		-0.62	0.71
=====					

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 70.71
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	70.711	70.711

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.002
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	10.8	38.4
Compression Capacity	472.4	435.7
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 28.9
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 0.707

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.003	21	-1.3	1.3	0.0	-0.5	0.0
EC-6.2.9.1	0.021	30	-0.8	1.8	0.0	-0.6	0.0
EC-6.2.5	0.016	18	0.0	1.3	0.0	-0.5	0.0
EC-6.2.6-(Y)	0.013	30	-0.8	1.8	0.0	-0.6	0.0
EC-6.3.2 LTB	0.022	30	-0.8	1.8	0.0	-0.6	0.0

Torsion and deflections have not been considered in the design.

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Steel Design (Track 2) Beam 25 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
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25 ST	IPE160	(DUTCH SECTIONS)			
	PASS	EC-6.3.3-662		0.789	21
	21.14 C	0.00		-11.82	2.97

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm²
Design Strength (py) = 235 N/mm²

SECTION PROPERTIES (units - cm)

Member Length = 297.00
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	779.000	289.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.045
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	118.5	157.1
Compression Capacity	232.6	134.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 17.8
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.890

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.025	35	-11.9	-7.6	0.0	6.8	0.0
EC-6.3.1.1	0.177	21	23.9	-4.0	0.0	0.0	0.0
EC-6.2.9.1	0.406	21	21.1	4.0	0.0	-11.8	0.0
EC-6.3.3-661	0.517	21	21.1	4.0	0.0	-11.8	0.0
EC-6.3.3-662	0.789	21	21.1	4.0	0.0	-11.8	0.0
EC-6.2.5	0.091	127	0.1	0.2	0.0	2.6	0.0
EC-6.2.6-(Y)	0.067	31	19.1	8.7	0.0	-10.3	0.0
EC-6.3.2 LTB	0.662	21	21.1	4.0	0.0	-11.8	0.0

Torsion and deflections have not been considered in the design.

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Steel Design (Track 2) Beam 26 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					
26 ST	IPE160	(DUTCH SECTIONS)			
	PASS	EC-6.3.3-662		0.412	27
	0.38 C	1.98		1.75	1.49
=====					

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 297.00
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	297.000	297.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.001
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	45.2	161.5
Compression Capacity	439.3	128.8
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 17.6
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.970

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.007	34	-3.3	-2.9	2.7	0.8	0.0
EC-6.3.1.1	0.109	32	14.0	0.4	-0.6	0.0	0.0
EC-6.2.9.1	0.328	25	-1.2	0.1	0.0	1.8	2.0
EC-6.3.3-661	0.280	27	0.4	0.2	0.0	1.8	2.0
EC-6.3.3-662	0.412	27	0.4	0.2	0.0	1.8	2.0
EC-6.2.5	0.243	36	0.0	-1.1	1.3	1.3	1.5
EC-6.2.6-(Z)	0.024	24	-0.1	-2.4	2.7	0.0	0.0
EC-6.2.6-(Y)	0.024	30	2.6	3.1	1.4	-1.5	0.0
EC-6.3.2 LTB	0.102	25	-1.2	0.1	0.0	1.8	2.0

Torsion and deflections have not been considered in the design.

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Steel Design (Track 2) Beam 27 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
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27 ST	IPE160	(DUTCH SECTIONS)			
	PASS	EC-6.3.3-662		0.882	25
	19.38 C	0.00		8.37	2.17

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 433.49
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	433.489	433.489

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.041
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	65.9	235.7
Compression Capacity	400.0	65.5
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 13.7
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 4.335

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.004	10	-2.0	-3.0	0.0	0.0	0.0
EC-6.3.1.1	0.326	25	21.4	-7.7	0.0	0.0	0.0
EC-6.2.9.1	0.287	24	15.0	0.0	0.0	8.4	0.0
EC-6.3.3-661	0.644	25	19.4	0.0	0.0	8.4	0.0
EC-6.3.3-662	0.882	25	19.4	0.0	0.0	8.4	0.0
EC-6.2.6-(Y)	0.059	24	17.0	-7.7	0.0	0.0	0.0
EC-6.3.2 LTB	0.612	24	15.0	0.0	0.0	8.4	0.0

Torsion and deflections have not been considered in the design.

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Steel Design (Track 2) Beam 28 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					
28 ST	IPE160	(DUTCH SECTIONS)			
	PASS	EC-6.3.3-662		0.338	33
	11.59 C	0.00		-3.09	1.88
=====					

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 377.00
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	377.000	377.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.025
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	57.3	205.0
Compression Capacity	418.5	84.6
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 15.1
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 3.770

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.004	16	-1.9	-1.2	0.0	0.0	0.0
EC-6.3.1.1	0.282	29	23.9	-0.8	0.0	0.0	0.0
EC-6.2.9.1	0.143	24	0.6	0.0	0.0	4.2	0.0
EC-6.3.3-661	0.272	27	3.2	0.0	0.0	4.2	0.0
EC-6.3.3-662	0.338	33	11.6	0.0	0.0	-3.1	0.0
EC-6.2.5	0.107	24	0.1	2.2	0.0	3.1	0.0
EC-6.2.6-(Y)	0.034	24	1.6	-4.4	0.0	0.0	0.0
EC-6.3.2 LTB	0.277	24	0.6	0.0	0.0	4.2	0.0

Torsion and deflections have not been considered in the design.

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Steel Design (Track 2) Beam 29 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					
29 ST	HE180A	(DUTCH SECTIONS)			
	PASS	EC-6.3.3-662		0.127	21
	8.32 C	0.00		-7.43	3.77
=====					

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 377.00
Gross Area = 45.30 Net Area = 45.30

	z-axis	y-axis
Moment of inertia	2510.000	925.000
Plastic modulus	325.000	156.000
Elastic modulus	293.567	102.778
Shear Area	22.799	14.520
Radius of gyration	7.444	4.519
Effective Length	859.000	366.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 1064.55
Axial force/Squash load : 0.008
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	115.4	81.0
Compression Capacity	492.5	663.2
Tension Capacity	1064.6	1064.6
Moment Capacity	76.4	36.7
Reduced Moment Capacity	76.4	36.7
Shear Capacity	309.3	197.0

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 65.0
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 3.660

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.006	16	-6.8	1.1	0.0	0.0	0.0
EC-6.3.1.1	0.020	21	9.8	-2.0	0.0	0.0	0.0
EC-6.2.9.1	0.107	35	-3.8	-2.2	0.0	8.2	0.0
EC-6.3.3-661	0.086	21	8.3	2.0	0.0	-7.4	0.0
EC-6.3.3-662	0.127	21	8.3	2.0	0.0	-7.4	0.0
EC-6.2.5	0.053	125	0.0	-1.1	0.0	4.1	0.0
EC-6.2.6-(Y)	0.011	35	-2.6	2.2	0.0	0.0	0.0
EC-6.3.2 LTB	0.126	35	-3.8	-2.2	0.0	8.2	0.0

Torsion and deflections have not been considered in the design.

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Steel Design (Track 2) Beam 44 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
44 ST	IPE160	(DUTCH SECTIONS) PASS	EC-6.3.3-662	0.095	21
		1.74 C	0.00	1.91	0.00

MATERIAL DATA

Grade of steel = S 235
 Modulus of elasticity = 205 kN/mm2
 Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 46.00
 Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	399.000	200.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
 Squash Load : 472.35
 Axial force/Squash load : 0.004
 GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	60.7	108.7
Compression Capacity	411.7	236.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 21.7
 co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.000

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.009	34	-4.4	-1.8	0.0	-0.5	0.0
EC-6.3.1.1	0.028	33	6.6	1.4	0.0	0.4	0.0
EC-6.2.9.1	0.066	21	1.7	3.8	0.0	1.9	0.0
EC-6.3.3-661	0.062	21	1.7	3.8	0.0	1.9	0.0
EC-6.3.3-662	0.095	21	1.7	3.8	0.0	1.9	0.0
EC-6.2.6-(Y)	0.031	29	4.6	4.0	0.0	1.3	0.0
EC-6.3.2 LTB	0.088	21	1.7	3.8	0.0	1.9	0.0

Torsion and deflections have not been considered in the design.

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Steel Design (Track 2) Beam 45 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					
45 ST	IPE160	(DUTCH SECTIONS)			
	PASS	EC-6.3.3-662		0.181	21
	6.02 C	0.02		3.36	0.00
=====					

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 107.00
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	249.000	200.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.013
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	37.9	108.7
Compression Capacity	449.6	236.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 21.7
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.000

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.3.1.1	0.036	25	8.5	-2.1	0.0	-1.6	0.0
EC-6.2.9.1	0.115	21	6.0	4.6	0.0	3.4	0.0
EC-6.3.3-661	0.091	21	6.0	4.6	0.0	3.4	0.0
EC-6.3.3-662	0.181	21	6.0	4.6	0.0	3.4	0.0
EC-6.2.6-(Y)	0.035	21	6.0	4.6	0.0	3.4	0.0
EC-6.3.2 LTB	0.155	21	6.0	4.6	0.0	3.4	0.0

Torsion and deflections have not been considered in the design.

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Steel Design (Track 2) Beam 48 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					
48 ST	IPE160	(DUTCH SECTIONS)			
		PASS	EC-6.3.3-662	0.662	21
		9.47 C	0.00	13.60	0.00
=====					

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 46.00
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	1081.000	200.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.020
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	164.4	108.7
Compression Capacity	134.2	236.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 21.7
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.000

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.025	35	-12.0	-7.3	0.0	-4.3	0.0
EC-6.3.1.1	0.105	31	14.1	12.9	0.0	11.1	0.0
EC-6.2.9.1	0.467	21	9.5	14.4	0.0	13.6	0.0
EC-6.3.3-661	0.608	21	9.5	14.4	0.0	13.6	0.0
EC-6.3.3-662	0.662	21	9.5	14.4	0.0	13.6	0.0
EC-6.2.5	0.079	10	0.1	-2.7	0.0	-2.3	0.0
EC-6.2.6-(Y)	0.110	21	9.5	14.4	0.0	13.6	0.0
EC-6.3.2 LTB	0.626	21	9.5	14.4	0.0	13.6	0.0

Torsion and deflections have not been considered in the design.

 KLOEZE bv ENGINEERING Software licensed to Engineering	Job No 9111-011	Sheet No 26	Rev
	Part Staalconstructie		
Job Title Nieuwbouw schuur	Ref		
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Steel Design (Track 2) Beam 49 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					
49 ST	IPE160	(DUTCH SECTIONS)			
		PASS	EC-6.3.3-661	0.600	21
		10.42 C	0.00	-12.12	0.00
=====					

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 107.00
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	1081.000	200.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.022
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	164.4	108.7
Compression Capacity	134.2	236.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 21.7
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.000

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.006	36	-3.0	1.4	0.0	0.8	0.0
EC-6.3.1.1	0.090	31	12.0	-2.8	0.0	-10.2	0.0
EC-6.2.9.1	0.416	21	10.4	-2.3	0.0	-12.1	0.0
EC-6.3.3-661	0.600	21	10.4	-2.3	0.0	-12.1	0.0
EC-6.3.3-662	0.598	21	10.4	-2.3	0.0	-12.1	0.0
EC-6.2.5	0.071	12	0.1	0.2	0.0	2.1	0.0
EC-6.2.6-(Y)	0.053	29	11.0	6.9	0.0	4.9	0.0
EC-6.3.2 LTB	0.558	21	10.4	-2.3	0.0	-12.1	0.0

Torsion and deflections have not been considered in the design.

 KLOEZE bv ENGINEERING Software licensed to Engineering	Job No 9111-011	Sheet No 27	Rev
	Part Staalconstructie		
Job Title Nieuwbouw schuur	Ref		
	By AdJ	Date 07-Jul-15	Chd PC
Client Fam. Venekamp / van Lingen	File 9111-011.std	Date/Time 08-Jul-2015 14:01	

Steel Design (Track 2) Beam 50 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
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50 ST	IPE160	(DUTCH SECTIONS)			
	PASS	EC-6.3.3-662		0.109	39
	14.02 C	0.00		-1.10	0.70

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm²
Design Strength (py) = 235 N/mm²

SECTION PROPERTIES (units - cm)

Member Length = 70.00
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	200.000	200.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.030
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	30.4	108.7
Compression Capacity	459.0	236.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 21.7
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.000

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.003	34	-1.5	-0.1	0.0	0.1	0.0
EC-6.3.1.1	0.062	29	14.8	-0.7	0.0	0.2	0.0
EC-6.2.9.1	0.038	39	14.0	1.6	0.0	-1.1	0.0
EC-6.3.3-661	0.063	39	14.0	1.6	0.0	-1.1	0.0
EC-6.3.3-662	0.109	39	14.0	1.6	0.0	-1.1	0.0
EC-6.2.5	0.005	126	0.0	0.4	0.0	-0.2	0.0
EC-6.2.6-(Y)	0.014	21	9.1	1.9	0.0	0.2	0.0
EC-6.3.2 LTB	0.051	39	14.0	1.6	0.0	-1.1	0.0

Torsion and deflections have not been considered in the design.

 KLOEZE bv ENGINEERING Software licensed to Engineering	Job No 9111-011	Sheet No 28	Rev
	Part Staalconstructie		
Job Title Nieuwbouw schuur	Ref		
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Steel Design (Track 2) Beam 55 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
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=====
      55 ST   IPE160      (DUTCH SECTIONS)
                        PASS      EC-6.3.3-662      0.434      21
=====
                        17.78 C      0.00      7.89      0.00
=====
```

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 70.00
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	305.000	200.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.038
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	46.4	108.7
Compression Capacity	437.5	236.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 21.7
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.000

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.016	34	-7.4	2.0	0.0	4.8	0.0
EC-6.3.1.1	0.075	31	17.8	0.6	0.0	4.5	0.0
EC-6.2.9.1	0.274	35	-5.2	-2.0	0.0	-8.0	0.0
EC-6.3.3-661	0.375	21	17.8	2.8	0.0	7.9	0.0
EC-6.3.3-662	0.434	21	17.8	2.8	0.0	7.9	0.0
EC-6.2.5	0.050	27	0.0	0.6	0.0	-1.4	0.0
EC-6.2.6-(Y)	0.022	34	-6.8	-2.9	0.0	-6.5	0.0
EC-6.3.2 LTB	0.367	35	-5.2	-2.0	0.0	-8.0	0.0

Torsion and deflections have not been considered in the design.

 KLOEZE bv ENGINEERING Software licensed to Engineering	Job No 9111-011	Sheet No 29	Rev
	Part Staalconstructie		
Job Title Nieuwbouw schuur	Ref		
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Steel Design (Track 2) Beam 56 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
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56 ST	IPE160	(DUTCH SECTIONS)			
	PASS	EC-6.3.3-662		0.228	39
	13.36 C	0.00		-3.77	1.30

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm²
Design Strength (py) = 235 N/mm²

SECTION PROPERTIES (units - cm)

Member Length = 130.09
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	200.000	200.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.028
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	30.4	108.7
Compression Capacity	459.0	236.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 21.7
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.000

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.004	24	-2.1	-1.0	0.0	1.0	0.0
EC-6.3.1.1	0.061	29	14.3	-1.4	0.0	1.0	0.0
EC-6.2.9.1	0.129	39	13.4	2.5	0.0	-3.8	0.0
EC-6.3.3-661	0.148	39	13.4	2.5	0.0	-3.8	0.0
EC-6.3.3-662	0.228	39	13.4	2.5	0.0	-3.8	0.0
EC-6.2.5	0.025	127	0.0	0.2	0.0	-0.7	0.0
EC-6.2.6-(Y)	0.021	41	12.3	2.7	0.0	-3.3	0.0
EC-6.3.2 LTB	0.174	39	13.4	2.5	0.0	-3.8	0.0

Torsion and deflections have not been considered in the design.

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Steel Design (Track 2) Beam 58 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					
58 ST	IPE160	(DUTCH SECTIONS)			
	PASS	EC-6.3.3-662		0.458	29
	15.57 C	0.00		-8.62	1.30
=====					

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 130.09
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	305.000	200.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.033
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	46.4	108.7
Compression Capacity	437.5	236.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 21.7
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.000

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.018	34	-8.6	0.2	0.0	3.4	0.0
EC-6.3.1.1	0.072	31	17.1	-1.1	0.0	4.7	0.0
EC-6.2.9.1	0.296	29	15.6	3.9	0.0	-8.6	0.0
EC-6.3.3-661	0.355	29	15.6	3.9	0.0	-8.6	0.0
EC-6.3.3-662	0.458	29	15.6	3.9	0.0	-8.6	0.0
EC-6.2.5	0.030	127	0.0	0.2	0.0	-0.9	0.0
EC-6.2.6-(Y)	0.034	41	14.8	4.4	0.0	-8.0	0.0
EC-6.3.2 LTB	0.397	29	15.6	3.9	0.0	-8.6	0.0

Torsion and deflections have not been considered in the design.

 KLOEZE bv ENGINEERING Software licensed to Engineering	Job No 9111-011	Sheet No 31	Rev
	Part Staalconstructie		
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Steel Design (Track 2) Beam 59 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					
59 ST	IPE160	(DUTCH SECTIONS)			
	PASS	EC-6.3.3-662		0.138	29
	4.15 C	-0.01		2.60	1.23
=====					

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 123.00
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	399.000	200.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.009
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	60.7	108.7
Compression Capacity	411.7	236.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 21.7
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.000

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.010	24	-4.7	0.3	0.0	-0.9	0.0
EC-6.3.1.1	0.027	33	6.5	1.1	0.0	-0.2	0.0
EC-6.2.9.1	0.089	29	4.2	-0.7	0.0	2.6	0.0
EC-6.3.3-661	0.102	29	4.2	-0.7	0.0	2.6	0.0
EC-6.3.3-662	0.138	29	4.2	-0.7	0.0	2.6	0.0
EC-6.2.5	0.003	1	0.0	0.0	0.0	0.1	0.0
EC-6.2.6-(Y)	0.023	29	4.5	3.1	0.0	-0.3	0.0
EC-6.3.2 LTB	0.120	29	4.2	-0.7	0.0	2.6	0.0

Torsion and deflections have not been considered in the design.

 KLOEZE bv ENGINEERING Software licensed to Engineering	Job No 9111-011	Sheet No 32	Rev
	Part Staalconstructie		
Job Title Nieuwbouw schuur	Ref		
	By AdJ	Date 07-Jul-15	Chd PC
Client Fam. Venekamp / van Lingen	File 9111-011.std	Date/Time 08-Jul-2015 14:01	

Steel Design (Track 2) Beam 61 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
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=====
        61 ST   IPE160      (DUTCH SECTIONS)
                        PASS   EC-6.3.3-662      0.586      21
=====
                        4.11 C      0.00      -12.39      3.24
=====

```

MATERIAL DATA

Grade of steel = S 235
 Modulus of elasticity = 205 kN/mm2
 Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 353.07
 Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	1081.000	200.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
 Squash Load : 472.35
 Axial force/Squash load : 0.009
 GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	164.4	108.7
Compression Capacity	134.2	236.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 21.7
 co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.000

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.029	35	-13.6	-1.0	0.0	-6.9	0.0
EC-6.3.1.1	0.103	31	13.9	11.0	0.0	5.6	0.0
EC-6.2.9.1	0.425	21	4.1	-0.3	0.0	-12.4	0.0
EC-6.3.3-661	0.542	29	12.1	0.0	0.0	-10.8	0.0
EC-6.3.3-662	0.586	21	4.1	-0.3	0.0	-12.4	0.0
EC-6.2.5	0.067	10	0.1	0.0	0.0	2.0	0.0
EC-6.2.6-(Y)	0.096	21	8.8	12.6	0.0	7.4	0.0
EC-6.3.2 LTB	0.570	21	4.1	-0.3	0.0	-12.4	0.0

Torsion and deflections have not been considered in the design.

 KLOEZE bv ENGINEERING Software licensed to Engineering	Job No 9111-011	Sheet No 33	Rev
	Part Staalconstructie		
Job Title Nieuwbouw schuur	Ref		
	By AdJ	Date 07-Jul-15	Chd PC
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Steel Design (Track 2) Beam 62 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
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62 ST	IPE160	(DUTCH SECTIONS)			
		PASS	EC-6.3.3-662	0.192	39
		4.67 C	0.00	-3.77	1.42

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm²
Design Strength (py) = 235 N/mm²

SECTION PROPERTIES (units - cm)

Member Length = 141.50
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	249.000	200.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.010
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	37.9	108.7
Compression Capacity	449.6	236.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 21.7
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.000

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.3.1.1	0.034	25	8.2	-1.1	0.0	0.2	0.0
EC-6.2.9.1	0.129	39	4.7	3.5	0.0	-3.8	0.0
EC-6.3.3-661	0.110	39	4.7	3.5	0.0	-3.8	0.0
EC-6.3.3-662	0.192	39	4.7	3.5	0.0	-3.8	0.0
EC-6.2.6-(Y)	0.026	39	4.7	3.5	0.0	-3.8	0.0
EC-6.3.2 LTB	0.174	39	4.7	3.5	0.0	-3.8	0.0

Torsion and deflections have not been considered in the design.

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	Part Staalconstructie		
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Steel Design (Track 2) Beam 64 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					
64 ST	IPE160	(DUTCH SECTIONS)			
	PASS	EC-6.3.3-662		0.429	29
	10.22 C	0.00		-8.62	1.42
=====					

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 141.50
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	1081.000	200.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.022
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	164.4	108.7
Compression Capacity	134.2	236.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 21.7
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.000

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.008	26	-3.6	-2.2	0.0	2.3	0.0
EC-6.3.1.1	0.085	31	11.5	-6.8	0.0	-5.1	0.0
EC-6.2.9.1	0.296	29	10.2	12.2	0.0	-8.6	0.0
EC-6.3.3-661	0.245	29	10.2	12.2	0.0	-8.6	0.0
EC-6.3.3-662	0.429	29	10.2	12.2	0.0	-8.6	0.0
EC-6.2.5	0.050	12	0.1	0.9	0.0	1.5	0.0
EC-6.2.6-(Y)	0.093	23	6.6	12.2	0.0	-5.9	0.0
EC-6.3.2 LTB	0.397	29	10.2	12.2	0.0	-8.6	0.0

Torsion and deflections have not been considered in the design.

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Steel Design (Track 2) Beam 65 Check 1

ALL UNITS ARE - KN METE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					
65 ST	IPE160	(DUTCH SECTIONS)			
	PASS	EC-6.3.2 LTB		0.155	21
	1.28 T	-0.02		-3.36	2.30
=====					

MATERIAL DATA

Grade of steel = S 235
Modulus of elasticity = 205 kN/mm2
Design Strength (py) = 235 N/mm2

SECTION PROPERTIES (units - cm)

Member Length = 230.07
Gross Area = 20.10 Net Area = 20.10

	z-axis	y-axis
Moment of inertia	869.000	68.000
Plastic modulus	124.000	26.000
Elastic modulus	108.625	16.585
Shear Area	8.090	9.666
Radius of gyration	6.575	1.839
Effective Length	399.000	200.000

DESIGN DATA (units - kN,m) EUROCODE NO.3 /2005

Section Class : CLASS 1
Squash Load : 472.35
Axial force/Squash load : 0.003
GM0 : 1.00 GM1 : 1.00 GM2 : 1.25

	z-axis	y-axis
Slenderness ratio (KL/r)	60.7	108.7
Compression Capacity	411.7	236.9
Tension Capacity	472.4	472.4
Moment Capacity	29.1	6.1
Reduced Moment Capacity	29.1	6.1
Shear Capacity	109.8	131.1

BUCKLING CALCULATIONS (units - kN,m)

Lateral Torsional Buckling Moment MB = 21.7
co-efficients C1 & K : C1 =1.132 K =1.0, Effective Length= 2.000

CRITICAL LOADS FOR EACH CLAUSE CHECK (units- kN,m):

CLAUSE	RATIO	LOAD	FX	VY	VZ	MZ	MY
EC-6.2.3 (T)	0.011	24	-5.4	-1.9	0.0	1.0	0.0
EC-6.3.1.1	0.026	33	6.1	0.2	0.0	-1.0	0.0
EC-6.2.9.1	0.115	21	-1.3	4.5	0.0	-3.4	0.0
EC-6.3.3-661	0.117	39	4.1	0.0	0.0	-2.7	0.0
EC-6.3.3-662	0.143	29	4.0	-0.1	0.0	-2.7	0.0
EC-6.2.5	0.046	23	0.0	-0.9	0.0	-1.3	0.0
EC-6.2.6-(Y)	0.034	21	-1.3	4.5	0.0	-3.4	0.0
EC-6.3.2 LTB	0.155	21	-1.3	4.5	0.0	-3.4	0.0

Torsion and deflections have not been considered in the design.

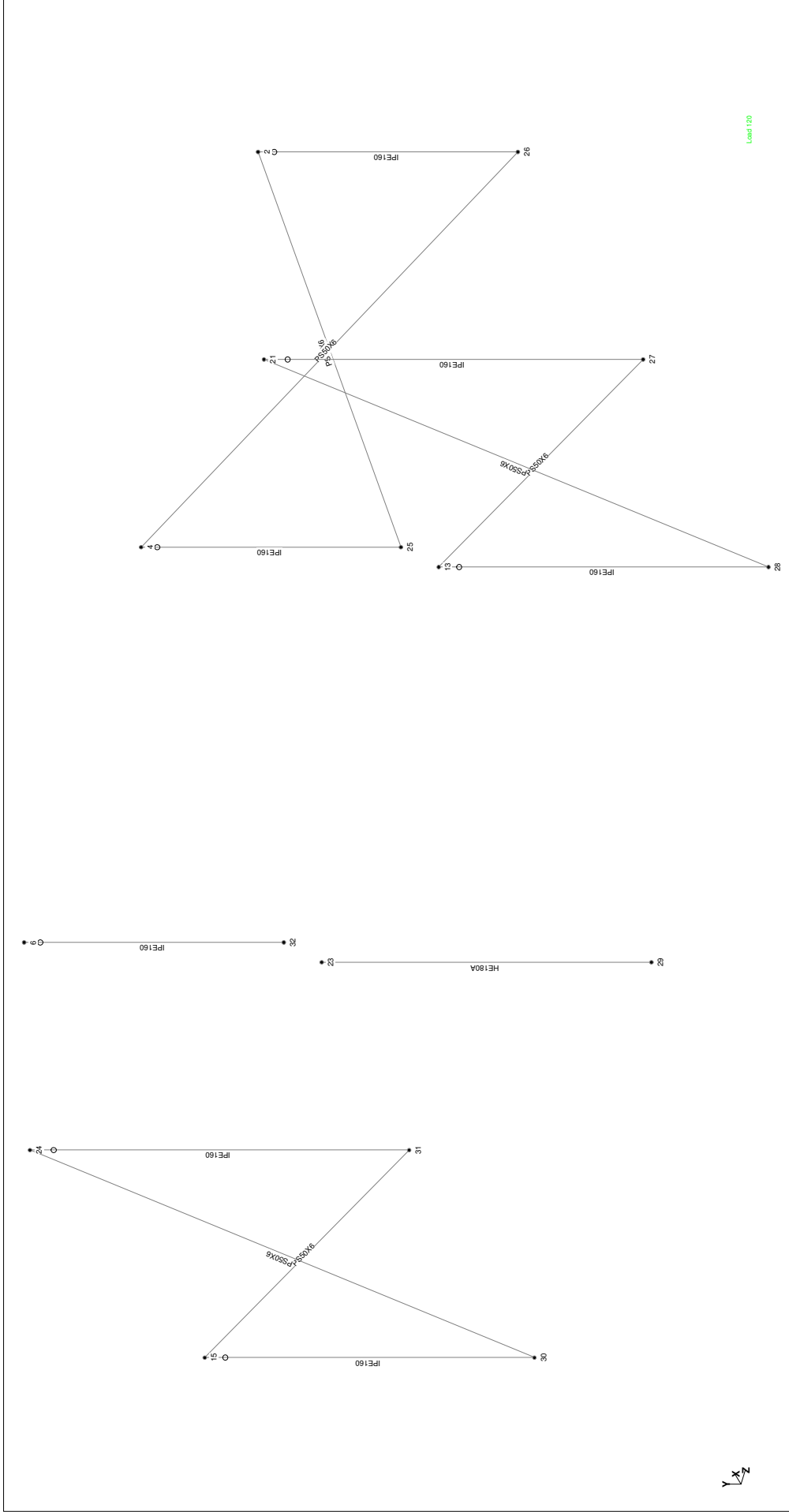
 KLOEZE bv ENGINEERING Software licensed to Engineering	Job No 9111-011	Sheet No 36	Rev
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Beam Maximum Forces by Section Property

Section		Axial	Shear		Torsion	Bending	
		Max Fx (kN)	Max Fy (kN)	Max Fz (kN)	Max Mx (kNm)	Max My (kNm)	Max Mz (kNm)
IPE160	Max +ve	23.86	7.72	0.00	0.00	0.00	8.37
	Max -ve	-1.98	-7.72	-0.00	-0.00	-0.00	-8.09
PS50X6	Max +ve	0.04	0.06	0.00	0.00	0.00	0.00
	Max -ve	-21.90	-0.06	0.00	0.00	0.00	0.00
IPE160	Max +ve	14.77	4.58	2.67	0.00	1.98	3.77
	Max -ve	-5.37	-4.51	-2.67	-0.00	-1.98	-2.72
HE180A	Max +ve	9.77	2.17	0.00	0.00	0.00	7.43
	Max -ve	-6.84	-1.97	-0.00	-0.00	-0.00	-8.19
IPE160	Max +ve	23.86	14.40	0.02	0.00	0.05	13.60
	Max -ve	-13.60	-12.21	-0.02	-0.00	-0.05	-12.39
L50X5	Max +ve	0.03	0.13	0.00	0.00	0.00	0.00
	Max -ve	-22.15	-0.13	0.00	0.00	0.00	0.00
KK70X3	Max +ve	22.26	0.19	0.00	0.00	0.00	0.00
	Max -ve	-7.71	-0.19	0.00	0.00	0.00	0.00
KK70X3	Max +ve	0.00	3.06	0.00	0.00	0.00	2.12
	Max -ve	-1.36	-4.42	-0.00	-0.00	-0.00	-1.47

Utilization Ratio

Beam	Analysis Property	Design Property	Actual Ratio	Allowable Ratio	Ratio (Act./Allow.)	Clause	L/C	Ax (cm ²)	Iz (cm ⁴)	Iy (cm ⁴)	Ix (cm ⁴)
1	PS50X6	PS50X6	0.303	1.000	0.303	EC-6.2.3 (T)	29	3.000	6.250	0.090	0.333
2	PS50X6	PS50X6	0.433	1.000	0.433	EC-6.2.3 (T)	35	3.000	6.250	0.090	0.333
3	PS50X6	PS50X6	0.303	1.000	0.303	EC-6.2.3 (T)	29	3.000	6.250	0.090	0.333
4	KK70X3	KK70X3	0.517	1.000	0.517	EC-6.3.1.1	21	7.880	58.460	58.460	91.920
5	KK70X3	KK70X3	0.458	1.000	0.458	EC-6.2.9.1	32	7.880	58.460	58.460	91.920
6	IPE160	IPE160	0.011	1.000	0.011	EC-6.2.9.1	30	20.100	869.000	68.000	3.600
7	KK70X3	KK70X3	0.517	1.000	0.517	EC-6.3.1.1	21	7.880	58.460	58.460	91.920
8	IPE160	IPE160	0.011	1.000	0.011	EC-6.2.9.1	30	20.100	869.000	68.000	3.600
9	KK70X3	KK70X3	0.225	1.000	0.225	EC-6.2.9.1	32	7.880	58.460	58.460	91.920
10	PS50X6	PS50X6	0.433	1.000	0.433	EC-6.2.3 (T)	35	3.000	6.250	0.090	0.333
11	PS50X6	PS50X6	0.232	1.000	0.232	EC-6.2.3 (T)	33	3.000	6.250	0.090	0.333
12	PS50X6	PS50X6	0.689	1.000	0.689	EC-6.3.1.1	28	3.000	6.250	0.090	0.333
15	KK70X3	KK70X3	0.225	1.000	0.225	EC-6.2.9.1	33	7.880	58.460	58.460	91.920
16	IPE160	IPE160	0.022	1.000	0.022	EC-6.3.2 LTB	30	20.100	869.000	68.000	3.600
21	KK70X3	KK70X3	0.248	1.000	0.248	EC-6.3.1.1	32	7.880	58.460	58.460	91.920
22	KK70X3	KK70X3	0.247	1.000	0.247	EC-6.3.1.1	32	7.880	58.460	58.460	91.920
23	KK70X3	KK70X3	0.173	1.000	0.173	EC-6.3.1.1	33	7.880	58.460	58.460	91.920
24	KK70X3	KK70X3	0.173	1.000	0.173	EC-6.3.1.1	32	7.880	58.460	58.460	91.920
25	IPE160	IPE160	0.789	1.000	0.789	EC-6.3.3-662	21	20.100	869.000	68.000	3.600
26	IPE160	IPE160	0.412	1.000	0.412	EC-6.3.3-662	27	20.100	869.000	68.000	3.600
27	IPE160	IPE160	0.882	1.000	0.882	EC-6.3.3-662	25	20.100	869.000	68.000	3.600
28	IPE160	IPE160	0.338	1.000	0.338	EC-6.3.3-662	33	20.100	869.000	68.000	3.600
29	HE180A	HE180A	0.127	1.000	0.127	EC-6.3.3-662	21	45.300	2.51E+3	925.000	14.800
30	IPE160	IPE160	0.338	1.000	0.338	EC-6.3.3-662	32	20.100	869.000	68.000	3.600
31	IPE160	IPE160	0.882	1.000	0.882	EC-6.3.3-662	25	20.100	869.000	68.000	3.600
32	IPE160	IPE160	0.409	1.000	0.409	EC-6.3.3-662	27	20.100	869.000	68.000	3.600
35	L50X5	L50X5	0.128	1.000	0.128	EC-6.2.3 (T)	33	4.800	4.516	17.986	0.400
36	L50X5	L50X5	0.274	1.000	0.274	EC-6.2.3 (T)	29	4.800	4.516	17.986	0.400
37	L50X5	L50X5	0.274	1.000	0.274	EC-6.2.3 (T)	29	4.800	4.516	17.986	0.400
38	L50X5	L50X5	0.210	1.000	0.210	EC-6.2.3 (T)	25	4.800	4.516	17.986	0.400
42	L50X5	L50X5	0.128	1.000	0.128	EC-6.2.3 (T)	32	4.800	4.516	17.986	0.400
43	L50X5	L50X5	0.210	1.000	0.210	EC-6.2.3 (T)	25	4.800	4.516	17.986	0.400
44	IPE160	IPE160	0.095	1.000	0.095	EC-6.3.3-662	21	20.100	869.000	68.000	3.600
45	IPE160	IPE160	0.181	1.000	0.181	EC-6.3.3-662	21	20.100	869.000	68.000	3.600
46	IPE160	IPE160	0.095	1.000	0.095	EC-6.3.3-662	21	20.100	869.000	68.000	3.600
47	IPE160	IPE160	0.181	1.000	0.181	EC-6.3.3-662	21	20.100	869.000	68.000	3.600
48	IPE160	IPE160	0.662	1.000	0.662	EC-6.3.3-662	21	20.100	869.000	68.000	3.600
49	IPE160	IPE160	0.600	1.000	0.600	EC-6.3.3-661	21	20.100	869.000	68.000	3.600
50	IPE160	IPE160	0.109	1.000	0.109	EC-6.3.3-662	39	20.100	869.000	68.000	3.600
51	IPE160	IPE160	0.109	1.000	0.109	EC-6.3.3-662	39	20.100	869.000	68.000	3.600
55	IPE160	IPE160	0.434	1.000	0.434	EC-6.3.3-662	21	20.100	869.000	68.000	3.600
56	IPE160	IPE160	0.228	1.000	0.228	EC-6.3.3-662	39	20.100	869.000	68.000	3.600
57	IPE160	IPE160	0.228	1.000	0.228	EC-6.3.3-662	39	20.100	869.000	68.000	3.600
58	IPE160	IPE160	0.458	1.000	0.458	EC-6.3.3-662	29	20.100	869.000	68.000	3.600
59	IPE160	IPE160	0.138	1.000	0.138	EC-6.3.3-662	29	20.100	869.000	68.000	3.600
60	IPE160	IPE160	0.138	1.000	0.138	EC-6.3.3-662	29	20.100	869.000	68.000	3.600
61	IPE160	IPE160	0.586	1.000	0.586	EC-6.3.3-662	21	20.100	869.000	68.000	3.600
62	IPE160	IPE160	0.192	1.000	0.192	EC-6.3.3-662	39	20.100	869.000	68.000	3.600
63	IPE160	IPE160	0.192	1.000	0.192	EC-6.3.3-662	39	20.100	869.000	68.000	3.600
64	IPE160	IPE160	0.429	1.000	0.429	EC-6.3.3-662	29	20.100	869.000	68.000	3.600
65	IPE160	IPE160	0.155	1.000	0.155	EC-6.3.2 LTB	21	20.100	869.000	68.000	3.600
66	IPE160	IPE160	0.155	1.000	0.155	EC-6.3.2 LTB	21	20.100	869.000	68.000	3.600
67	KK70X3	KK70X3	0.076	1.000	0.076	EC-6.3.1.1	32	7.880	58.460	58.460	91.920
68	KK70X3	KK70X3	0.076	1.000	0.076	EC-6.3.1.1	33	7.880	58.460	58.460	91.920



Verklaring reactiekrachten :

De in de lijst aangegeven krachten zijn de minimale (-ve) en de maximale (+ve) **reactiekrachten**

in de richtingen (+) of tegengesteld (-) aan de richtingen van de pijlen zoals in het UDS icoon te zien links onder op sheet 37

Op deze pagina staan tevens de knooppuntnummers voor de reacties vermeld.

De maatgevende belastingcombinatie staat eronder.

Belastingcombinaties zie blz 8 ,deel 10.2 numerieke computerinvoer

Ontwerputgangspunten : 15 jr; CC1; EXC1

nr. 9111-011

dd : 08-07-15

Node	Env	Horizontal Fx kN	Vertical Fy kN	Horizontal Fz kN
25	+ve	3.20	23.93	0.00
		38 UGT19	21 UGT2	20 UGT1
25	-ve	-4.67	-9.86	-10.03
		26 UGT7	35 UGT16	32 UGT13
26	+ve	2.36	14.07	12.62
		39 UGT20	32 UGT13	33 UGT14
26	-ve	-2.55	-1.21	-2.35
		25 UGT6	34 UGT15	27 UGT8
27	+ve	10.76	21.43	7.46
		29 UGT10	25 UGT6	33 UGT14
27	-ve	-0.00	-2.33	-7.72
		34 UGT15	39 UGT20	24 UGT5
28	+ve	0.00	23.93	3.28
		-	29 UGT10	33 UGT14
28	-ve	-14.30	-13.66	-4.43
		35 UGT16	35 UGT16	24 UGT5
29	+ve	1.97	9.77	0.00
		21 UGT2	21 UGT2	33 UGT14
29	-ve	-2.17	-5.41	-0.00
		35 UGT16	34 UGT15	32 UGT13
30	+ve	0.00	23.93	4.43
		-	29 UGT10	24 UGT5
30	-ve	-14.30	-13.66	-3.28
		35 UGT16	35 UGT16	32 UGT13
31	+ve	10.76	21.43	7.72
		29 UGT10	25 UGT6	26 UGT7
31	-ve	-0.00	-2.33	-7.46
		25 UGT6	39 UGT20	32 UGT13
32	+ve	2.36	9.31	2.67
		39 UGT20	31 UGT12	25 UGT6
32	-ve	-2.55	-1.33	-2.59
		25 UGT6	34 UGT15	32 UGT13

INFORMATIEF
(representatief EG + BB)
BGT1

Horizontal Fx kN	Vertical Fy kN
0.00	10.17
-	120 BGT1
-1.47	0.00
120 BGT1	-
0.00	5.08
-	120 BGT1
-0.13	0.00
120 BGT1	-
2.14	7.93
120 BGT1	120 BGT1
0.00	0.00
-	-
0.00	6.51
-	120 BGT1
-1.67	0.00
120 BGT1	-
0.79	5.94
120 BGT1	120 BGT1
0.00	0.00
-	-
0.00	6.51
-	120 BGT1
-1.67	0.00
120 BGT1	-
2.14	7.93
120 BGT1	120 BGT1
0.00	0.00
-	-
0.00	4.95
-	120 BGT1
-0.13	0.00
120 BGT1	-